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A multi-order method for predicting stability of a multi-delay milling system considering helix angle and run-out effects

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- 14 Cutting force;
- Floquet theory; 15
- 16 Milling stability;

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Abstract In this paper, a multi-delay milling system considering helix angle and run-out effects is firstly established. An exponential cutting force model is used to model the interaction between a work-piece and a cutting tool, and a new approach is presented for accurately calibrating exponential cutting force coefficients and cutter run-out parameters. Furthermore, based on an implicit multi-step Adams formula and an improved precise time-integration algorithm, a novel stability prediction method is proposed to predict the stability of the system. The involved time delay term and periodic coefficient term are integrated as a comprehensive state term in the integral response which is approximated by the Adams formula. Then, a Floquet transition matrix with an arbitraryorder form is constructed by using a series of matrix multiplication, and the stability of the system is determined by the Floquet theory. Compared to classical semi-discretization methods and fulldiscretization methods, the developed method shows a good performance in convergence, efficiency, accuracy, and multi-order complexity. A series of cutting tests is further carried out to validate the practicability and effectiveness of the proposed method. The results show that the calibration process needs a time of less than 5 min, and the stability prediction method is effective.

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Milling operations are widely used in the aerospace industry

for machining various highly expensive components, such

as aero-engine blisks, impellers, blades, casings, and so on.

These components are mostly made of aluminum alloys, or

difficult-to-cut titanium and nickel alloys. In the milling pro-

cess, chatter is an undesirable phenomenon that inevitably

deteriorates workpiece quality and even causes damages to

CNC machine tools.¹ How to avoid chatter is a key issue to

1. Introduction

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29 ensure a stable cut with a high material removal rate. Chatter 30 stability prediction plays an important role in selecting machining parameters in order to achieve a chatter-free oper-31 ation. Generally, it utilizes stability lobes to classify machining 32 parameter combinations into stable and unstable regions in a 33 diagram,² namely the stability lobe diagram (SLD). An opti-34 mal cutting parameter combination chosen in a stable region 35 not only avoids chatter, but also improves machining produc-36 tivity. Therefore, it is particularly necessary and important to 37 seek an effective prediction method. 38

Apart from the trial and error method, some feasible meth-39 40 ods including analytical and numerical methods have been 41 proposed in the frequency domain and the discrete time domain. Altintas and Budak³ proposed the first analytical 42 solution in the frequency domain. Their method, known as 43 the single-frequency solution (SFS), can give a rapid and accu-44 45 rate computation of the SLD in a large radial immersion case. 46 In order to improve the prediction accuracy in a small radial 47 immersion case, a multi-frequency solution (MFS) was further proposed by Budak and Altintas⁴, which uses the higher har-48 49 monics of directional factors instead of the average ones used in the SFS. Alternately, based on the Floquet theory of delay-50 differential equations (DDEs), modeling in the discrete time 51 domain is also a good choice to achieve accurate stability pre-52 dictions. Bayly et al.⁵ solved discrete time equations by using 53 54 temporal finite elements analysis to determine stability boundaries. Butcher et al.⁶ proposed the Chebyshev collocation 55 method in the discrete time domain to predict the stability of 56 57 a time-periodic DDE. Both methods use one matrix to construct the Floquet transition matrix (FTM) in a similar way, 58 and they are very competitive for their rates of convergence. 59 However, they are only easy to use for single-delay cases and 60 61 not quite suitable for cases with varying or multiple time delays. 62

63 On the other hand, Insperger and Stépán⁷ investigated the 64 periodic motion of time-period DDEs using the semidiscretization (SD) method, in which only the delay term 65 and the periodic coefficient term are discretized. An updated 66 version of the SD method,⁸ known as the zeroth-order SD 67 (0th SD) method, was then applied to predict the stability of 68 69 milling processes, in which the delay term was discretized as a weighted sum of two neighboring discrete state values. 70 Furthermore, a first-order SD (1st SD) method⁹ was developed 71 to essentially increase the efficiency of the original SD method, 72 in which the delay term was then approximated by linear inter-73 polation of two neighboring discrete state values. Alterna-74 tively, Ding et al.¹⁰ proposed a first-order full-discretization 75 (1st FD) method with a faster computational efficiency. In 76 addition to discretizing the delay term and the periodic coeffi-77 cient term, a portion of the actual time-domain state term is 78 discretized in the FD method as well. Both SD and FD meth-79 ods use a series of matrix multiplication to construct the FTM 80 81 in another similar way, and they can be extended to predict the 82 stability of a milling system with varying or multiple time 83 delays. Insperger⁹ compared SD with FD methods in a same scheme and proved that the 1st FD method converges slower 84 than the same-order SD method. Later, second-order FD $(2nd FD)^{11}$ and high-order FD methods¹²⁻¹⁴ were further 85 86 developed to improve the convergence rate of FD methods. 87 However, the construction of the FTM becomes more compli-88 cated, especially for multi- or varying-delay systems. Recently, 89 Ding et al.¹⁵ developed an efficient numerical integration (NI) 90

method and Zhang et al.¹⁶ proposed a compact Simpson method for the stability analysis of milling processes, respectively based on an integration scheme and a differential scheme. It was found that these methods are also analogous to temporal finite elements analysis and the Chebyshev collocation method in constructing the FTM. Besides, Zhou et al.¹⁷ predicted the stability in end milling of aero-engine casings using an analytical method. Luo et al.¹⁸ presented a new time-domain model of mechanics and dynamics of the cutter exit process.

This paper proposes an efficient, accurate, and compact stability prediction for a multi-delay milling system. The delay term and the periodic coefficient term are integrated as a comprehensive state term in the integral response of time-period DDEs which is approximated by a multi-step implicit Adams formula, and the time-domain state term is not discretized. A compact and arbitrary-order FTM is constructed by using a series of matrix multiplication. An improved precise timeintegration algorithm is used to calculate the resulting exponential matrices rapidly. Furthermore, considering that different cutting force models and corresponding calibration accuracies of cutting force coefficients significantly affect the reliability of stability lobes^{19,20} but the cutting force models in most of the above works are linear, an exponential force model is employed and a new approach is also presented to accurately calibrate exponential cutting force coefficients (ECFCs) and cutter run-out parameters (CRPs) simultaneously.

2. Modeling of the milling dynamics

The milling cutter is modeled as a mass-spring-damper system 120 with two degrees of freedom (2-DOFs) respectively in the X121 direction (parallel to the tool feed) and the Y direction (per-122 pendicular to the tool feed). It is assumed to be flexible as 123 opposed to the rigid workpiece as shown in Fig. 1. $O_{\rm G}(t)$ is 124 the geometric center of the milling cutter at the current cutting 125 instant t. $O_{\rm G}(t-\tau)$ is the geometric center of the milling cutter 126 at the previous cutting instant $t - \tau$, where τ is the time delay. 127 $X_{\rm R}$ and $Y_{\rm R}$ are the orthogonal coordinate axes with their coor-128 dinate origins lying at $O_G(t)$. j - 1, j, and j + 1 represent the 129 previous, current, and next cutter teeth, respectively. k_x and 130

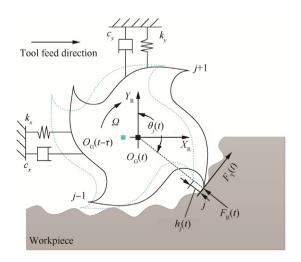


Fig. 1 Schematic of a 2-DOF milling process.

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