

CJA 891

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Chinese Society of Aeronautics and Astronautics & Beihang University

Chinese Journal of Aeronautics

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JOURNAL OF
AERONAUTICS

³ A multi-order method for predicting stability of a ⁴ multi-delay milling system considering helix angle and run-out effects

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9 Received 27 February 2017; revised 11 May 2017; accepted 20 May 2017

12 **KEYWORDS**

- 14 Cutting force;
- 15 Floquet theory;
- 16 Milling stability;
- 17 Multi-delay milling system;
- 18 Run-out

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Abstract In this paper, a multi-delay milling system considering helix angle and run-out effects is firstly established. An exponential cutting force model is used to model the interaction between a work-piece and a cutting tool, and a new approach is presented for accurately calibrating exponential cutting force coefficients and cutter run-out parameters. Furthermore, based on an implicit multi-step Adams formula and an improved precise time-integration algorithm, a novel stability prediction method is proposed to predict the stability of the system. The involved time delay term and periodic coefficient term are integrated as a comprehensive state term in the integral response which is approximated by the Adams formula. Then, a Floquet transition matrix with an arbitraryorder form is constructed by using a series of matrix multiplication, and the stability of the system is determined by the Floquet theory. Compared to classical semi-discretization methods and fulldiscretization methods, the developed method shows a good performance in convergence, efficiency, accuracy, and multi-order complexity. A series of cutting tests is further carried out to validate the practicability and effectiveness of the proposed method. The results show that the calibration process needs a time of less than 5 min, and the stability prediction method is effective.

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> Milling operations are widely used in the aerospace industry 21 for machining various highly expensive components, such 22 as aero-engine blisks, impellers, blades, casings, and so on. 23 These components are mostly made of aluminum alloys, or 24 difficult-to-cut titanium and nickel alloys. In the milling pro-
25 cess, chatter is an undesirable phenomenon that inevitably 26 deteriorates workpiece quality and even causes damages to 27 CNC machine tools.^{[1](#page--1-0)} How to avoid chatter is a key issue to 28

1. Introduction 20

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Peer review under responsibility of Editorial Committee of CJA.

ELSEVIER **Production and hosting by Elsevier**

<http://dx.doi.org/10.1016/j.cja.2017.08.005>

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Please cite this article in press as: JIANG S, SUN Y A multi-order method for predicting stability of a multi-delay milling system considering helix angle and run-out effects, Chin J Aeronaut (2017), <http://dx.doi.org/10.1016/j.cja.2017.08.005>

 ensure a stable cut with a high material removal rate. Chatter stability prediction plays an important role in selecting machining parameters in order to achieve a chatter-free oper- ation. Generally, it utilizes stability lobes to classify machining parameter combinations into stable and unstable regions in a diagram,^{[2](#page--1-0)} namely the stability lobe diagram (SLD). An opti- mal cutting parameter combination chosen in a stable region not only avoids chatter, but also improves machining produc- tivity. Therefore, it is particularly necessary and important to seek an effective prediction method.

 Apart from the trial and error method, some feasible meth- ods including analytical and numerical methods have been proposed in the frequency domain and the discrete time 42 domain. Altintas and Budak³ proposed the first analytical solution in the frequency domain. Their method, known as the single-frequency solution (SFS), can give a rapid and accu- rate computation of the SLD in a large radial immersion case. In order to improve the prediction accuracy in a small radial immersion case, a multi-frequency solution (MFS) was further 8 proposed by Budak and Altintas^4 , which uses the higher har- monics of directional factors instead of the average ones used in the SFS. Alternately, based on the Floquet theory of delay- differential equations (DDEs), modeling in the discrete time domain is also a good choice to achieve accurate stability pre- 53 dictions. Bayly et al.⁵ solved discrete time equations by using temporal finite elements analysis to determine stability bound-55 aries. Butcher et al.^{[6](#page--1-0)} proposed the Chebyshev collocation method in the discrete time domain to predict the stability of a time-periodic DDE. Both methods use one matrix to con- struct the Floquet transition matrix (FTM) in a similar way, and they are very competitive for their rates of convergence. However, they are only easy to use for single-delay cases and not quite suitable for cases with varying or multiple time 62 delays.

63 On the other hand, Insperger and Stépán⁷ investigated the periodic motion of time-period DDEs using the semi- discretization (SD) method, in which only the delay term and the periodic coefficient term are discretized. An updated 67 version of the SD method, $8 \text{ known as the zeroth-order SD}$ $8 \text{ known as the zeroth-order SD}$ (0th SD) method, was then applied to predict the stability of milling processes, in which the delay term was discretized as a weighted sum of two neighboring discrete state values. 71 Furthermore, a first-order SD (1st SD) method \degree was developed to essentially increase the efficiency of the original SD method, in which the delay term was then approximated by linear inter- polation of two neighboring discrete state values. Alterna- tively, Ding et al.[10](#page--1-0) proposed a first-order full-discretization (1st FD) method with a faster computational efficiency. In addition to discretizing the delay term and the periodic coeffi- cient term, a portion of the actual time-domain state term is discretized in the FD method as well. Both SD and FD meth- ods use a series of matrix multiplication to construct the FTM in another similar way, and they can be extended to predict the stability of a milling system with varying or multiple time 83 delays. Insperger^{[9](#page--1-0)} compared SD with FD methods in a same scheme and proved that the 1st FD method converges slower than the same-order SD method. Later, second-order FD 86 (2nd FD)^{[11](#page--1-0)} and high-order FD methods^{[12–14](#page--1-0)} were further developed to improve the convergence rate of FD methods. However, the construction of the FTM becomes more compli- cated, especially for multi- or varying-delay systems. Recently, 90 Ding et al. 15 15 15 developed an efficient numerical integration (NI) method and Zhang et al.^{[16](#page--1-0)} proposed a compact Simpson 91 method for the stability analysis of milling processes, respec- 92 tively based on an integration scheme and a differential 93 scheme. It was found that these methods are also analogous 94 to temporal finite elements analysis and the Chebyshev collo- 95 cation method in constructing the FTM. Besides, Zhou et al. 17 17 17 96 predicted the stability in end milling of aero-engine casings 97 using an analytical method. Luo et al. 18 presented a new 98 time-domain model of mechanics and dynamics of the cutter 99 exit process. 100

This paper proposes an efficient, accurate, and compact sta- 101 bility prediction for a multi-delay milling system. The delay 102 term and the periodic coefficient term are integrated as a comprehensive state term in the integral response of time-period 104 DDEs which is approximated by a multi-step implicit Adams 105 formula, and the time-domain state term is not discretized. A 106 compact and arbitrary-order FTM is constructed by using a 107 series of matrix multiplication. An improved precise time-
108 integration algorithm is used to calculate the resulting expo- 109 nential matrices rapidly. Furthermore, considering that differ-
110 ent cutting force models and corresponding calibration 111 accuracies of cutting force coefficients significantly affect the 112 reliability of stability lobes $19,20$ but the cutting force models 113 in most of the above works are linear, an exponential force 114 model is employed and a new approach is also presented to 115 accurately calibrate exponential cutting force coefficients 116 (ECFCs) and cutter run-out parameters (CRPs) 117 simultaneously. 118

2. Modeling of the milling dynamics 119

The milling cutter is modeled as a mass-spring-damper system 120 with two degrees of freedom $(2-DOFs)$ respectively in the $X = 121$ direction (parallel to the tool feed) and the Y direction (per-
122 pendicular to the tool feed). It is assumed to be flexible as 123 % opposed to the rigid workpiece as shown in Fig. 1. $O_G(t)$ is 124 the geometric center of the milling cutter at the current cutting 125 the geometric center of the milling cutter at the current cutting instant t. $O_G(t-\tau)$ is the geometric center of the milling cutter 126
at the previous cutting instant $t-\tau$ where τ is the time delay at the previous cutting instant $t - \tau$, where τ is the time delay. 127
 Y_2 and Y_3 are the orthogonal coordinate axes with their coordinate X_R and Y_R are the orthogonal coordinate axes with their coordinate origins lying at $O_G(t)$. $j - 1$, j , and $j + 1$ represent the 129
previous current and next cutter teeth respectively k and previous, current, and next cutter teeth, respectively. k_x and 130

Fig. 1 Schematic of a 2-DOF milling process.

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