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Erosion degradation characteristics of a linear electro-hydrostatic actuator under a high-frequency turbulent flow field

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KEYWORDS

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Abstract The paper proposes a performance degradation analysis model based on dynamic erosion wear for a novel Linear Electro-Hydrostatic Actuator (LEHA). Rather than the traditional statistical methods based on degradation data, the method proposed in this paper firstly analyzes the dominant progressive failure mode of the LEHA based on the working principle and working conditions of the LEHA. The Computational Fluid Dynamics (CFD) method, combining the turbulent theory and the micro erosion principle, is used to establish an erosion model of the rectification mechanism. The erosion rates for different port openings, under a time-varying flow field, are obtained. The piecewise linearization method is applied to update the concentration of contaminated particles within the LEHA, in order to gain insight into the erosion degradation process at various stages of degradation. The main contribution of the proposed model is the application of the dynamic concentration of contamination particles in erosion analysis of Electro-Hydraulic Servo Valves (EHSVs), throttle valves, spool valves, and needle valves. The effects of system parameters and working conditions on component wear are analyzed by simulations. The results of the proposed model match the expected degradation process.

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Integrated Electro-Hydrostatic Actuators (EHAs) have seen

increased application in More-Electric Aircraft (MEA), due

to their numerous advantages including high reliability, long lifetime, and high efficiency. $^{1-4}$ Traditional power-integrated

Rotary Electro-Hydrostatic Actuators (REHAs) are facing

many problems, such as severe heating, big inertia, low-

frequency response, and difficulty in redundancy configura-

tion. In order to solve these deficiencies, many researchers have

1. Introduction

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proposed direct-drive EHAs.⁵⁻⁹ Li et al. have presented a novel 33 LEHA for the pump control system based on a collaborative 34 rectification structure for linear pumps where the fundamental 35 subsystem consists of two Direct Drive Pump Cells 36 (DDPCs).¹⁰ Their prototype has verified feasibility of the pro-37 posed actuator and flexibility of the dual-control strategy. 38 Although the system has a number of advantages, its reliability 39 characteristics, such as degradation and life prediction, need to 40 be addressed and further improved. Applying the novel oper-41 ating principle, the LEHA has improved these performance 42 issues, but it has also introduced a problem due to the fact that 43 44 it cannot integrate filters. The novel LEHA is also an inte-45 grated closed system which can increase the power-to-weight 46 ratio. A linear resonance motor drives piston cylinder suction and discharges oil. The spool of a rectification slide valve is 47 rigidly connected with the driving cylinder rod, resulting in 48 49 the active rectification mechanism to be in a high-frequency 50 condition. Due to non-filter design, contaminated particles will 51 continuously cycle in an LEHA during its operation, which will precipitate further erosion and produce more contamina-52 tion particles. Consequently, compared to a conventional 53 hydraulic system with filters, the rectification mechanism in 54 an LEHA can fail more rapidly, which can lead to a dominant 55 progressive degradation process. 56

The rectification mechanism is commonly present in 57 hydraulic systems, and when coupled with oil contamination, 58 59 it can result in system failure. Some research results have indicated that contamination particles in oil wash out and wear the 60 edges of valve components.¹¹ The resulting leakage increase 61 caused by wear accounts for approximately 60% of cases of 62 component failure. According to the research by Zhang 63 et al., the wear resulting from particulate contaminants causes 64 65 an increase in the internal leakage, the output current hysteresis and null leakage, the input current threshold, and the pres-66 67 sure gain, as well as a decrease in the gain linearity of the electrohydraulic servo valve.¹² The Physics-of-Failure (PoF) 68 models of particle erosion wear introduced by Fang et al. show 69 that the erosion wear has significant impacts on the electrohy-70 draulic servo valve's service life and reliability.¹³ Furthermore, 71 the erosion of an LEHA is even more serious due to the par-72 73 ticular type of motion and active rectification under relatively severe conditions. This paper is focused on the performance 74 degradation of an LEHA induced by erosion wear. 75

Performance degradation analysis is extensively applied in 76 numerous engineering fields to evaluate safety of machine 77 parts and equipment.¹⁴ The associated theories can be divided 78 into three categories: (a) failure physics, (b) probability statis-79 tics, and (c) artificial intelligence. The first approach studies the 80 structural integrity of an object with respect to operating con-81 ditions and mechanical and physical properties of materials 82 used to make the object. Probability statistics models are 83 mainly suitable for analysis of degradation based on stress fati-84 85 gue, which requires significant amount of test data. Alter-86 nately, the artificial intelligence approach is dependent on 87 field performance degradation data. In the field of durability analysis and life prediction, numerous physical experiments 88 are performed in order to evaluate the life and reliability of 89 hydraulic components. Therefore, during the design stage, it 90 is essential to analyze the overall LEHA system based on the 91 physical nature of erosion. 92

A significant number of studies have been performed to analyze the effect of erosion on system performance degradation. Fitch and Hong investigated the effects of contaminated 95 oil on erosion in pumps and contaminant lock in servo valves, 96 and proposed a new method to predict service life.¹⁵ The 97 occurrence of contaminant lock is accidental whereas the ero-98 sion caused by contaminant particulates is a continuous pro-99 cess which takes place as long as the system is operational. 100 Vaughan et al. examined the effects of the particle size and 101 concentration, differential pressure across the metering land, 102 spool opening, spool surface, flow direction, as well as fluid 103 characteristics on erosion wear.¹⁶ Yang et al. adopted a 104 gamma process to describe the internal structure degradation 105 under erosion for electrohydraulic servo valves.¹ ⁷ Zhang 106 et al. presented a degradation assessment and life prediction 107 method for electrohydraulic servo valves based on the CFD 108 method and hydraulic simulation.¹² In addition, other 109 researchers have predicted structural wear by CFD tech-110 niques.¹⁸⁻²⁰ The mechanism of erosion for a ductile metal 111 material is a micro-cutting process, which was put forward 112 by Finnie, who also presented an analytical erosion model to 113 calculate erosion rates.²¹ Tilly proposed that erosion of ductile 114 materials could occur in two stages, where the first stage is 115 micro-cutting whereas the second stage is surface fragmenta-116 tion, and found that resulting estimates gave a good correla-117 tion with experimental data.²² Recent theoretical and 118 experimental studies explored the effects of particle properties, 119 impacting speed and angle, and material properties on the 120 severity of erosion. Among those studies, the Edwards model 121 has been widely accepted to be applicable to erosion for gas-122 solid, liquid-solid, or gas-liquid-solid flow, where particle 123 properties, impacting speed and angle, and material properties 124 are taken into account.²³ Therefore, the Edwards model is uti-125 lized in this study because of its extensive applicability and 126 high prediction accuracy. In addition, erosion due to the recti-127 fication mechanism in an LEHA under the influence of con-128 taminant particles in hydraulic oil falls within the model 129 framework. 130

This paper proposes a new method for analyzing performance degradation under dynamic erosion wear. The Edwards model is utilized to obtain erosion rates due to its broad applicability and high prediction accuracy. Furthermore, erosion rates of the rectification mechanism for different port openings and different degradation stages are estimated. In addition, in order to obtain the degradation curve under dynamic erosion wear, the concentration of contaminant particles is updated at different stages of degradation. Finally, the proposed degradation model is applied to simulate the wear degradation process in an LEHA under different flow conditions, and results are compared with results from traditional wear studies.

2. Problem description

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2.1. Working principle of the LEHA 144

The schematic representation of the proposed LEHA architec-145 ture is shown in Fig. 1, whereas Fig. 2 represents the hydraulic 146 circuit diagram and control loop of a traditional REHA. The 147 REHA utilizes a motor and a pump to convert electrical 148 energy to hydraulic energy, where the motor has reversible 149 rotation in order to control the flow direction of hydraulic 150 oil. Compared with the REHA, the proposed LEHA has the 151 following distinct characteristics: (1) a linear resonance motor 152

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