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# High-resolution simulation for rotorcraft aerodynamics in hovering and vertical descending flight using a hybrid method

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- Vorticity transport model 18
- 19

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Abstract A high-resolution simulation tool for rotorcraft aerodynamics is developed by coupling CFD with a Vorticity Transport Model (VTM). An Eulerian-based CFD module is used to model the blade near body flowfield, and a Lagrangian-based VTM module is employed for vortex tracking in the far wake. The coupling procedure is implemented by transmitting vortex sources to the VTM module and feeding boundary conditions back to the CFD module. The presented CFD/ VTM hybrid solver is firstly validated by hover cases of three different rotor configurations. Simulation results, including the blade surface pressure distribution, rotor downwash, and hover figure of merit, exhibit favorable correlations with available experimental data. Then, a rotor operated in vertical descending flight with a fixed collective pitch is investigated. It is shown that the CFD/VTM coupling method is suitable for rotor wake simulation. Wake instabilities (far wake breakdown in hover and toroidal wake pattern in the vortex ring state) are successfully demonstrated with a moderate computational cost.

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an accurate prediction of the rotor flowfield remains a chal-

lenging problem. The three-dimensional rotor wake is

unsteady and complex. In a hovering condition, highly ener-

getic tip vortices shed from the blade tip region, swirl down-

ward, and then undergo vortex breakdown in the far wake.

In descending flight, tip vortices constantly persist near the

rotor disk and interact with the blades, which may cause a high

level of fuselage vibration and remarkable induced power con-

sumption. Moreover, when a rotorcraft is operated over cer-

tain ranges of descent rate, convection of the wake would be

inhibited. It results in a doughnut-shaped ring around the

rotor disk, which is known as the Vortex Ring State<sup>1</sup> (VRS,

#### 1. Introduction 20

21 Rotorcraft plays an important role in aviation for its unique 22 ability in hovering and vertical descending flight. However,

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see Fig. 1). The VRS is regarded as the roughest flight regime of a rotorcraft. According to statistical data,<sup>2</sup> at least 32 helicopter accidents were attributed to this dangerous regime between 1982 and 1997.

Over the past few decades, studies about the unsteady char-39 acteristics of rotor wake in hovering and descending flight have 40 been focused on experiments<sup>3-11</sup> and qualitative analysis.<sup>12-15</sup> 41 Meanwhile, relatively sparse numerical simulations have been 42 paralleled. The aerodynamics near the blade surface, like com-43 pressible and viscous effects, are predicted well by conven-44 tional Eulerian-based CFD methods, but they are 45 computationally expensive, and inherent numerical dissipation 46 makes the rotor wake diffuse too early.<sup>16</sup> To date, conven-47 tional CFD methods are insufficient in far wake capturing of 48 the rotor. 49

Lagrangian-based models can address the problem of non-50 physical wake diffusion, and they are more computationally 51 52 efficient than CFD. In recent years, coupled Eulerian/Lagrangian simulation methods have shown promise in rotor wake 53 simulations and received much attention.<sup>17–20</sup> However, simple 54 Lagrangian models (e.g., prescribed wake models<sup>21</sup> and free 55 wake models<sup>22</sup>) rely heavily on empirical parameters such as 56 vortex core size and decay factor. Furthermore, they cannot 57 provide detailed information of the wake structure. Due to 58 the progress in wake modeling techniques, more advanced 59 Lagrangian models have been developed. Those models are 60 referred to as Vorticity Transport Models (VTMs).<sup>23-25</sup> They 61 can explicitly conserve wake vorticity without any artificial dis-62 sipation and cancel the restriction of empirical parameters. 63

The main work of the present study is to couple a novel 64 Lagrangian-based VTM model with an Eulerian-based CFD 65 solver. The hybrid solver proposed in this paper combines 66 the merits of CFD and the VTM. A CFD module is used to 67 resolve the compressible blade near body aerodynamics and 68 69 a VTM module is used to predict the complex wake convection. Details of the CFD/VTM hybrid solver are described in 70 Section 2. Numerical simulations of rotorcraft in hovering 71 and vertical descending flight are performed in Section 3. 72 Results show good predictions of both the blade near body 73 74 aerodynamics and the wake structure in hover. Induced inflow 75 and time history of rotor thrust in descending flight are also 76 investigated. Main conclusions are summarized in Section 4.

#### 2. CFD/VTM model description 77

The computational zone is decomposed into two domains 78 (Fig. 2): the blade body-fitted Eulerian domain, which covers 79 a relatively small region near the blade and follows a C-O 80



Schematic of the air flow for a rotorcraft in the vortex Fig. 1 ring state.



Schematic of the computational zone. Fig. 2

topology grid (Fig. 3), and the background Lagrangian 81 domain, which employs a set of particles to model the wake 82 vorticity. These two domains are solved by CFD and a 83 VTM, respectively. Since the VTM only solves incompressible 84 flow, the C-O grid of the Eulerian domain extends far enough 85 (over two chord lengths) to ensure that outside the grid, air compressibility could be neglected. 87

### 2.1. CFD solution of blade body-fitted Eulerian domain

The simulation of the rotor blade near flowfield follows the Eulerian description, which relates to the grid-based solutions of compressible Reynold Averaged Navier-Stokes (RANS) equations. RANS equations are solved in terms of the conservation forms of mass, momentum, and energy, and can be written in tensor form as<sup>26</sup>

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_j}{\partial x_j} = 0 \tag{1}$$

$$\frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_i} = -\frac{\partial p}{\partial x_i} + \frac{\partial \tau_{ij}}{\partial x_i}$$
(2)

$$\frac{\partial \rho E}{\partial t} + \frac{\partial (\rho E + p)u_j}{\partial x_j} = \frac{\partial u_i \tau_{ij}}{\partial x_j} - \frac{\partial q_j}{\partial x_j}$$
(3)



Fig. 3 Rotor blade near body C-O topology grid.

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