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Hysteresis behaviors of compressor rotating stall with cusp catastrophic model

Zhiping LI^{a,b,c}, Peng ZHANG^{a,b,c}, Tianyu PAN^{a,b,c,d,*}, Qiushi LI^{a,b,c}, Jian ZHANG^c

^a National Key Laboratory of Science and Technology on Aero-Engine Aerothermodynamics, Beihang University, Beijing 100082, Ching

100083, China

- ⁹ ^b Collaborative Innovation Center of Advanced Aero-Engine, Beihang University, Beijing 100083, China
- ^c School of Energy and Power Engineering, Beihang University, Beijing 100083, China
- ¹¹ ^d Department of Mechanical Engineering and Materials Science, Duke University, Durham, NC 27708, USA
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15 KEYWORDS

- 17 Catastrophe theory;
- 18 Compressor;
- 19 Hysteresis;
- 20 Rotating stall;

Abstract Rotating stall is a complex nonlinear dynamic phenomenon which is always characterized by catastrophe and hysteresis in high aerodynamic-loading compressor. Exploring the key contributing factors and characteristic rules of hysteresis is very important for compressor design and flow instability control. In this paper, a novel model method is proposed to analyze the hysteresis behaviors to extend the understanding of compressor rotating stall. The equilibrium states of compressor system under different conditions are first described based on Moore-Greitzer model. Then, through assessing the stability of the equilibrium points by Liapunov's theorem, the ratio of shutoff head to compressor characteristic semi-height is found to affect the stall hysteresis: the size of hysteresis loop will gradually decrease, even disappear with the increase of the ratio. Combing the effects of both the ratio and throttle coefficient, the hysteresis behaviors of compressor stall under multi-parameters can be found to be consistent with the topological properties of cusp catastrophic model by Thom's catastrophe theory. Finally, according to topological invariant rules, from the perspective of potential function, the equilibrium surface equation of compressor system is developed by standard cusp catastrophic model to describe the various hysteresis behaviors of compressor rotating stall along different control routes.

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* Corresponding author at: National Key Laboratory of Science and Technology on Aero-Engine Aerothermodynamics, Beihang University, Beijing 100083, China.

1. Introduction

E-mail address: pantianyu@buaa.edu.cn (T. PAN).

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by Elsevier instability is very often manifested as a phenomenon known

When the flow rate through a compressor is throttled gradu-

ally and the stall limit is reached, the essentially steady,

axisymmetric flow becomes unstable. The result of this

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as rotating stall, which is an asymmetric phenomenon with one or several stall cells rotating at a fraction of the rotor speed while the overall mass flow rate remains nearly constant once the pattern is fully developed.^{1,2}

Before stalling, two types of stall inception are often 32 detected: model waves and spike.³⁻⁷ The modal wave is charac-33 terized by the gradual growth of small-amplitude, essentially 34 two dimensional, long wavelength disturbances. The spike is 35 a three dimensional disturbance, which is localized at the tip 36 region of a specific rotor in a multistage compressor, and has 37 38 a length scale on the order of several blade pitches. According 39 to the change of whole characteristic of the compressor in stall 40 process, the types of rotating stall can also be divided into gradual stall and abrupt stall. For the early compressors,⁸ in 41 the stall process, the pressure rise often progressively changes 42 as the flow rate increases and decreases. As the design loading 43 of compressor blade increases, the stall-type of current main-44 45 stream compressors is generally abrupt stall; the pressure rise 46 and the flow rate can be markedly reduced, and the efficiency can also drop sharply. In addition, a larger throttle opening is 47 required to move the operating point from rotating stall to 48 normal working condition than throttling at stall inception. 49 These are the catastrophe and hysteresis of abrupt stall, the 50 potentially serious threats to engine reliability. 51

For the catastrophe and hysteresis of compressor rotating 52 53 stall, scholars have made some related researches. Day and 54 Cumpsty⁹ studied the hysteresis of compressor rotating stall through changing the design value of the flow coefficient, 55 and found that the size of hysteresis loop will gradually 56 decrease as the design value of the flow coefficient decreases. 57 Copenhaver and Okiishi¹⁰ tested the overall recoverability of 58 a 10-stage compressor, and the results showed that higher shaft 59 60 speeds cause low recoverability. The hysteresis of compressor rotating stall was first studied through numerical simulation 61 by Choi et al.^{11,12} They found that rotating stall at each oper-62 63 ating point during recovery is stable, and rotating stall becomes unstable to be a transient after stall cells become 64 too small to block the flow. Day et al.¹³ introduced the block-65 age coefficient to assess the hysteresis of compressor rotating 66 stall and found the compressor will recover from rotating stall 67 68 when the blockage coefficient is less than 30%. From the point of structure stability, Abed et al.¹⁴ and McCaughan¹⁵ analyzed 69 the characteristic of stall hysteresis with the help of bifurcation 70 theory. They regarded the hysteresis of rotating stall as the sys-71 tem bifurcation. Liaw and Abed¹⁶ applied the bifurcation the-72 ory to the active control of compressor stall inception, and 73 74 eliminated the undesirable jump and hysteresis behavior of the uncontrolled system. 75

A series of studies have shown that the hysteresis behaviors 76 77 of the compressor stall are affected by multi parameters, and determining the contributing factors and characteristic rule 78 of hysteresis is essential to guide the design and control of 79 80 the compressor. The catastrophe and hysteresis are related to 81 the concept of "bifurcation" in mathematics. Currently, with 82 the advancement of nonlinear dynamics, bifurcation theory has been applied to analyze the compressor rotating 83 stall.^{14–19} However, the bifurcation theory can only consider 84 the effects of a single parameter. In 1983, the French mathe-85 matician Thom²⁰ first proposed catastrophe theory based on 86 the bifurcation theory. The catastrophe theory can describe 87 the effects of more control parameters on a system and has 88 been widely used in the field of nonlinear dynamics.²¹⁻²⁵ There-89

fore, an idea to build a model to describe the hysteresis behaviors of compressor stall under the impact of multiple parameters is proposed based on the catastrophe theory.

This paper is organized as follows. Firstly, the equilibrium 93 points of compressor system are determined based on Moore-94 Greitzer (M-G) model in Section 2. Then, in Section 3, the con-95 tributing factors of the stall hysteresis are analyzed and the 96 physical mechanism of catastrophe and hysteresis is discussed 97 through assessing the stability of the equilibrium points by 98 Liapunov's theorem. Finally, according to topological invari-99 ant rules, the equilibrium surface equation of compressor is developed based on the standard cusp catastrophic model, and it is used to describe the diverse hysteresis behaviors of compressor rotating stall along different control routes in Section 4, which is then followed by conclusions (Section 5).

2. Equilibrium state of compressor system

The basic compressor system under study is shown in Fig. 1. This compressor system consists of a compressor with an inlet duct upstream and outlet duct downstream, followed by a plenum of relatively big volume and an exhaust pipe with a throttle valve at the exit. The simplest model which adequately describes the dynamics of rotating stall and surge in axial-flow compressor systems shown in Fig. 1 is the Moore-Greitzer model.^{26,27} The full model is described in detail in the references and so we move straight to the simplified model.²⁸ The differential equations are as follows:

$$\frac{\mathrm{d}\phi}{\mathrm{d}\xi} = \left[-\frac{\psi - \psi_{c_0}}{H} + 1 + \frac{3}{2}\phi\left(1 - \frac{1}{2}J\right) - \frac{1}{2}\phi^3\right]\frac{H}{l_cW}$$
(1) 118

$$\frac{\mathrm{d}\psi}{\mathrm{d}\xi} = \frac{W}{4B^2 l_{\mathrm{c}}} (\phi - \phi_{\mathrm{T}}) \tag{2}$$

$$\frac{\mathrm{d}J}{\mathrm{d}\xi} = J \left[1 - \phi^2 - \frac{1}{4}J \right] \frac{3aH}{(1+ma)W} \tag{3}$$

where the variable ϕ is nondimensional mass flow coefficient, 125 which has been shifted so that zero mass flow actually occurs 126 at $\phi = -1$, and rescaled with W. W is compressor characteris-127 tic semi-width. ψ is the nondimensional pressure rise of the 128 compressor. Both of these variables are averaged over the 129 annulus of the compressor. H is compressor characteristic 130 semi-height. ξ refers to time for wheel to rotate one radian. 131 The parameter ψ_{c_0} is the shutoff head, and it is proportional 132 to the number of stages in the compressor. J is the square of 133 the amplitude of the first mode of the rotating stall distur-134 bance, so it only has physical meaning when it is positive. l_c 135 refers to the total aerodynamic length of compressor and 136 ducts. The parameter B in Eq. (2) is Greitzer's B parameter, 1,2 137 which determines the type of compressor instability. When the 138 B is small, the flow usually develops into rotating stall. The 139 variable $\phi_{\rm T}$ represents the mass flow leaving the plenum and 140



Fig. 1 Schematic of axial flow compressor system.

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