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## **Research on vibration suppression of a mistuned** blisk by a piezoelectric network

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#### **KEYWORDS**

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15 Amplitude magnification; Bi-periodic; 16 17 Blisk; 18 Mistuning; 19 Mono-periodic; 20 Parallel piezoelectric net-21 work; Statistical analysis; 22 23 Vibration suppression

Abstract The work aims to provide a further investigation of the dynamic characteristics of an integral bladed disk (also called 'blisk') with a Parallel Piezoelectric Network (PPN). The PPN is constructed by parallelly interconnecting the piezoelectric patches distributed in the blisk. Two kinds of PPN are considered, namely mono-periodic PPN and bi-periodic PPN. The former has a piezoelectric patch in each sector, and the later has one patch every few sectors. The vibration suppression performance of both kinds of PPN has been studied through modal analysis, forced response analysis, and statistical analysis. The research results turn out that the PPN will only affect mechanical frequencies near the electrical frequency clusters slightly, and the bi-periodic PPN will make the nodal diameter spectrum of the modes more complex, but the amplitude corresponding to the new nodal diameter component is much smaller than that of the nodal diameter component corresponding to the mono-periodic system. The mechanical coupling between the blades and the disk plays an important role in the damping effect of the PPN, and it should be paid attention to in applications. The mono-periodic PPN can effectively suppress the amplitude magnification of the forced response induced by the mistuning of the blisk; meanwhile, it can mitigate the vibration localization of the mistuned electromechanical system. If piezoelectric patches are set only in part of the sectors, the bi-periodic PPN still has a vibration suppression ability, but the effect is related to the number and spatial distribution of the piezoelectric patches.

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## 1. Introduction

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Bladed disks in aero-engines belong to a class of structures

26 called periodic structures. These structures consist of spatially 27 repetitive substructures which are designed to be identical in 28 ideal situations.<sup>1</sup> However, in reality, there are always small 29 and random deviations in blade properties, and these are due 30

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to factors such as manufacturing tolerance, material inhomo-31 32 geneity, and in-operation wear. These blade-to-blade discrepancies are called mistuning, which are typically small, but 33 can lead to vibration concentrated in a small region of a struc-34 ture. This phenomenon is known as vibration response local-35 ization. As a result, certain blades can have significantly 36 37 higher forced response levels than that in an ideally tuned design. For this reason, the phenomenon is also called ampli-38 tude magnification. It is considered as one of the major factors 39 inducing High Cycle Fatigue (HCF) of blades.<sup>2</sup> Therefore, it is 40 important to reduce amplitude magnification induced by 41 42 mistuning.

43 Dry-friction damping has been the most common approach 44 in vibration mitigation since a long time ago, while it is not favorable due to the absence of contact interfaces in an integral 45 bladed disk ('blisk' for short in the rest of the paper) in modern 46 aero-engines.<sup>3–6</sup> These issues drive researchers to find alterna-47 48 tive damping techniques particularly for vibration suppression 49 of a mistuned blisk with low structural damping. In recent decades, piezoelectric materials have received considerable atten-50 tion because of their properties such as light weight, high 51 bandwidths, efficient energy conversion, and ease of integra-52 tion.<sup>7</sup> When embedded in or bonded on fundamental struc-53 tures, piezoelectric materials can transform mechanical 54 energy to electric energy when they undergo mechanical defor-55 mations, and vice versa. Based on this energy conversion capa-56 57 bility, various vibration reduction techniques have been developed. Passive piezoelectric damping techniques are initi-58 ated by Forward,<sup>8</sup> who investigated the damping effect of a 59 piezoelectric patch shunted with an inductor. Hagood and Flo-60 tow<sup>9</sup> investigated the possibility of dissipating mechanical 61 energy using piezoelectric shunt circuits containing a resistor 62 and an inductor. They showed that a shunt circuit with a resis-63 tor and an inductor performs like a dynamic vibration absor-64 ber, especially in cases where the resistor and the inductor are 65 optimally tuned to structural resonance in a manner analogous 66 to a mechanical vibration absorber. The studies of Yun and 67 Kim<sup>10</sup> and Moheimani<sup>11</sup> showed that the positions of piezo-68 electric patches and the reactance of a shunt circuit should 69 be carefully selected to minimize the maximum forced response 70 71 corresponding to the targeted mode. To overcome the limitation that the value of inductance is too high to be achieved 72 in a low-frequency domain, a synthetic inductance<sup>12</sup> is used, 73 and an inductance with a value of thousands of Henries has 74 been obtained.<sup>13</sup> Min et al.<sup>14</sup> performed a numerical and exper-75 imental study for rotating piezoelectric composite subscale fan 76 77 blades, and they proved that piezoelectric vibration damping could significantly reduce the vibration of composite fan 78 blades in an aero-engine. Zhou et al.<sup>15,16</sup> proposed a vibration 79 control strategy based on the passive piezoelectric shunt damp-80 ing technique for a mistuned blisk. Their numerical simulation 81 results indicated that a good performance could be achieved in 82 terms of reducing the vibration of a slowly time-variant mis-83 tuned blisk. Then, Mokrani et al.<sup>17,18</sup> utilized the shape of a 84 85 targeted mode to organize piezoelectric patches as a modal filter, which decreased the required inductors of a shunted cir-86 cuit. Their method was firstly validated experimentally on a 87 circular plate, and then applied to a prototype of an industrial 88 bladed drum. 89

Wang et al.<sup>19,20</sup> attempted to bond piezoelectric patches on both blades and a disk and then connect them with a network to reduce modal localization of mistuned bladed disks. They

showed that the piezoelectric network could create a new elec-93 trical energy channel, which could destroy the intrinsic mech-94 anism for vibration localization. Focusing on the vibration 95 suppression of a mistuned bladed disk, Yu and Wang<sup>21,22</sup> used 96 a negative capacitance to improve the performance of the 97 piezoelectric network. These research efforts offered a start 98 on applying the piezoelectric network to suppress the multi-99 harmonic vibration of a mistuned bladed disk. Liu et al.<sup>23</sup> con-100 sidered the non-engine-order excitation from a practical point 101 of view, and the mechanisms of vibration-suppression of a 102 piezoelectric network and a piezoelectric shunt circuit were 103 explained by means of modal analysis and energy analysis. 104 Li et al.<sup>24</sup> built piezoelectric networks among several identical 105 structures without any mechanical coupling. It was shown 106 through analytical derivation that the response of each compo-107 nent is composed of two parts: one is the response to the exci-108 tation acting on that component itself, and the other is the 109 response to the average excitation forces over all the compo-110 nents. Such an additional response can perform as a "compen-111 sation" to suppress the overall response of a given component. 112 The vibration suppression performances of both Parallel 113 Piezoelectric Networks (PPNs) and Series Piezoelectric Net-114 works (SPNs) have been studied by parameter studies. Results 115 have shown that both PPNs and SPNs can effectively suppress 116 the vibration level, though with different optimal parameters. 117 The best performances for PPNs and SPNs are identical and 118 better than that of passive piezoelectric shunts. The features 119 of PPNs and SPNs were further investigated by considering 120 a more complex yet more realistic situation where the mechan-121 ical coupling between adjacent blade sectors was taken into 122 account.<sup>25</sup> It turned out that the vibration response to non-123 zero engine-order excitation could be reduced by a PPN, while 124 an SPN only works for zero engine-order excitation. Their 125 analytical and experimental results in their research work<sup>26,27</sup> 126 indicated that a PPN has an advantage in vibration delocaliza-127 tion of a mistuned periodic structure than a traditional piezo-128 electric shunt circuit. Meanwhile, only resistors and capacitors 129 have been considered in their research in order to avoid an 130 inductance with a huge value. In these analytical models, 131 piezoelectric patches are all assumed to be located on the sur-132 faces of blades, which would bring an enormous influence to 133 the flow field. Moreover, because the blade surface is usually 134 a complex curved surface, it is difficult to bond or embed a 135 piezoelectric patch on it. It is easier to set piezoelectric patches 136 on the surface of the disk, which, in addition, can minimize the 137 influence to the flow field. When piezoelectric patches are 138 bonded on the disk surface, there will be different dynamic 139 characteristics of the electromechanical system which should 140 be further studied. 141

When piezoelectric patches are distributed in every sector of 142 a blisk, the electrical period is the same as the mechanical per-143 iod, and the electromechanical system is a mono-periodic sys-144 tem. Meanwhile, in a case where piezoelectric patches are 145 distributed every few sectors, the electromechanical system 146 becomes a bi-periodic system, which means that the electrical 147 period is different from the mechanical period. This work is 148 meant to contribute to a better understanding of the dynamic 149 characteristics of a blisk with both mono-periodic and bi-150 periodic systems. The aim of the research in the paper is to find 151 an effective alternative damping technique for the mistuned 152 blisks with low structural damping. The content of the paper 153 is organized as follows. First of all, the model of a blisk with 154

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