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Fatigue life prediction model of 2.5D woven composites at various temperatures

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KEYWORDS

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- 17 Temperature;
- 18 2.5D woven composites

Abstract As one of the new structural layout in the family of woven composites, 2.5D Woven Composites (2.5D-WC) have recently attracted an increasing interest owing to its excellent properties, i.e. high specific strength and fatigue resistance, in the aerospace and automobile industry. Indepth understanding of the fatigue behavior of this material at un-ambient temperatures is critical for the engineering applications, especially in aero-engine field. Here, fatigue behavior of 2.5D-WC at different temperatures was numerically investigated based on the unit cell approach. Firstly, the unit cell model of 2.5D-WC was established using ANSYS software. Subsequently, the temperature-dependent fatigue life prediction model was built up. Finally, the fatigue lives alongside the damage evolution processes of 2.5D-WC at ambient temperature (20 °C) and unambient temperature (180 °C) were analyzed. The results show that numerical results are in good agreement with the relevant experimental results at 20 and 180 °C. Fatigue behavior of 2.5D-WC is also sensitive to temperature, which is partially attributed to the mechanical properties of resin and the change of inclination angle of warp yarns. We hope that the proposed fatigue life prediction model and the findings could further promote the engineering application of 2.5D-WC, especially in aero-engine field.

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Textile composites are being widely applied in the field of aero-

space engineering due to their excellent mechanical properties,

i.e. high specific stiffness/strength and outstanding fatigue

resistance. 2.5D Woven Composites (2.5D-WC) not only pos-

sess a superior delamination resistance capacity in comparison

with 2D laminated composites, but also have a simpler struc-

tural configuration than 3D textile composites. Recently, many

parts in the aero-engine field, i.e. woven fan/compressor blades

and casing, have been manufactured using resin matrix com-

1. Introduction

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posites. Nevertheless, the characteristics of long-term service and elevated temperature environment in aero-engine inevitably result in difficulty of fatigue-related theoretical research, especially for the study with respect to the fatigue life prediction model at un-ambient temperatures.^{1,2}

Many researches have reported about the mechanical prop-35 erties and prediction models of woven composites based on 36 experimental and finite element methods. Montesano et al.^{3,4} 37 investigated the mechanical behavior of 2D triaxially woven 38 composites at different temperatures by experiment, and found 39 40 that fatigue behavior was not sensitive to temperature at 120 °C. Selezneva et al.⁵ experimentally investigated the failure 41 42 mechanism in off-axis 2D woven laminates at ambient temperature (20 °C), 105, 160 and 205 °C, and demonstrated that the 43 woven varns began to straighten out and rotated towards the 44 45 loading direction just prior to failure. Vieille and Taleb⁶ studied the influence of temperature and matrix ductility on the 46 47 behavior of notched 2D woven composites at ambient temper-48 ature (20 °C) and 120 °C, and the results revealed that the highly ductile behavior of thermoplastic laminates was quite 49 effective to accommodate the overstresses near the hole at 50 the temperature higher than the glass transition temperature 51 $T_{\rm m}$. Koumpias et al.⁷ predicted the strength of 3D fully woven 52 composites at ambient temperature based on a homogenized 53 Representative Volume Element (RVE). Zhou et al.⁸ studied 54 55 the damage and failure characterization of 2D woven compos-56 ites under different uniaxial and biaxial loadings at ambient temperature by adopting a two-step, multi-scale progressive 57 damage analysis. Li et al.⁹ developed a micromechanical finite 58 element model to predict the effective mechanical properties of 59 woven fabric composites at elevated temperatures. Although 60 61 there have been several works in predicting mechanical properties of textile composites by simulation, the specific research 62 pertaining to 2.5D-WC is scarce as yet. Previous works in 63 terms of establishing and simulating the mechanical behavior 64 65 of 2.5D-WC at ambient temperature have been done by us.^{1,10,11} The geometric model, strength prediction model and 66 damage behavior of 2.5D-WC under the warp and weft static 67 loading at ambient temperature have been systematically 68 analyzed. 69

70 Additionally, to the best of our knowledge, very few simulation models related to the fatigue life of woven composites 71 have been reported. Dai and Mishnaevsky¹² simulated the fati-72 gue life of hybrid fiber reinforced composites at ambient tem-73 perature based on X-FEM and unit cell models. Hao et al.¹³ 74 predicted the fatigue behavior of 3D 4-direction braided com-75 posites at ambient temperature based on the unit cell 76 approach, where the prediction model takes into account the 77 variation of stiffness and strength of components induced by 78 cyclic loading. Qiu¹⁴ proposed modified residual stiffness and 79 residual strength models, in which the influence of fiber volume 80 fraction was considered. Coupled with the progression damage 81 82 approach, the fatigue life of 2.5D-WC was predicted at ambi-83 ent temperature.

84 Surprisingly, there is almost no published literature about predicting the fatigue behavior of woven composites at un-85 ambient temperatures using numerical approach. However, 86 the immense popularity of woven composites in the aero-87 engine generally experiences a long-term service under the 88 un-ambient temperatures. Therefore, it is meaningful to estab-89

lish a temperature-dependent fatigue life prediction model of woven composites, especially in the aero-engine field.

In this work, our principal objective is to establish the fati-92 gue life prediction model that can evaluate the temperature-93 dependent fatigue behavior of woven composites. Taking 94 2.5D-WC as a specific research object, three stress levels of 95 warp fatigue loading at 20 and 180 °C were employed to verify 96 the rationality of fatigue life prediction model. Afterwards, the 97 damage evolution histories at 20 and 180 °C were quantita-98 tively observed based on the simulation model. Finally, the 99 fracture morphologies at 20 and 180 °C obtained by simula-100 tion and testing were compared. This work could provide an 101 available approach in predicting fatigue behavior at different 102 temperatures, which will further facilitate the engineering 103 application of 2.5D-WC. 104

2. Fatigue life prediction model

The temperature-dependent fatigue life prediction model of 106 woven composites subjected to uniaxial tension-tension load-107 ing mainly includes: fatigue damage criteria, damage propaga-108 tion model, geometry/finite element model and periodic 109 boundary conditions. 110

Several damage criteria in terms of composite materials, 112 such as Misses, Tsai-Wu and Hashin criteria, have been pro-113 posed to solve different engineering issues. As the 3D 114 Hashin criterion has been successfully applied in estimating 115 the strength of woven composites at ambient temperature 116 previously¹⁵⁻¹⁷, a modified 3D Hashin criterion taking into 117 account temperature and cycle number will be proposed in 118 this work. Furthermore, based on the previous studies,¹ fail-119 ure mechanisms of woven composites can be hypothetically 120 related to two failure modes (two directions) for anisotropic 121 fiber yarns: yarn breaking and matrix cracking. Nevertheless, 122 in addition to temperature, the mechanical properties of 123 fiber yarns are generally sensitive to the volume fraction of 124 fiber in fiber yarns (or called fiber aggregation density).¹⁴ 125 Therefore, the corresponding failure criteria can be given 126 as follows: 127

Yarn longitudinal damage (breakage in axial direction, or 1-axis direction):

$$\left(\frac{\sigma_{11}}{X_{11}(n, V_{\rm f}, T)}\right)^2 + \beta \left(\frac{\sigma_{12}}{S_{12}(n, V_{\rm f}, T)}\right)^2 + \beta \left(\frac{\sigma_{13}}{S_{13}(n, V_{\rm f}, T)}\right)^2 \ge 1 \tag{1}$$

where σ_{ij} (*i*, *j* = 1, 2, 3) are the stress components; X_{11} is the 133 longitudinal tensile strength of fiber yarn; S_{12} and S_{13} are the shear strength of fiber yarn; β is the shear contribution factor; 135 *n* is the cycle number; $V_{\rm f}$ is the fiber aggregation density; *T* is 136 the temperature. 137

Yarn transversal damage (Interior matrix cracking or fibermatrix shear-out failure in in-plane direction, or 2/3-axis direction):

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