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Impact of the thermal effect on the load-carrying capacity of a slipper pair for an aviation axial-piston pump

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KEYWORDS

- 15 Aviation axial piston pump;
- 16 Fluid lubrication;
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- Slipper pair;
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- **Abstract** A thermal hydraulic model based on the lumped parameter method is presented to analyze the load-carrying capacity of a slipper pair in an aviation axial-piston pump under specified operating conditions. Both theoretical and experimental results are presented to demonstrate the validity of the thermal hydraulic model. The results illustrate that the squeezing force and thermal wedge bearing force are the main factors that affect the film thickness and load-carrying capacity. At high oil temperature and high load pressure, the film thickness decreases with increasing clamping force, but the load-carrying capacity will increase. An increase of the film thickness is proven to be beneficial under high shaft rotational speed but especially dangerous as it strongly increases the ripple amplitude of the film thickness, which leads to decreasing the load-carrying capacity. The structural parameters of the slipper can be optimized to achieve desired performance, such as the slipper radius ratio and orifice length diameter ratio. To satisfy the requirement of the load-carrying capacity, the slipper radius ratio should be selected from 1.4 to 1.8, and the orifice length diameter ratio should be selected from 4 to 5.

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An aviation axial-piston pump is widely used in an aircraft

hydraulic system for supplying hydraulic power to a flight

actuator because it has high output pressure, high efficiency,

and high reliability. For the development of an axial piston

pump with a higher efficiency rate and a simultaneously high

service life, an optimal gap design allowing a minimum of fric-

tion and volumetric losses in the given parameter range of a

1. Introduction

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machine is urgently necessary. A large number of studies have been concerned about optimization gap design,¹ vibration and noise reductions,^{2,3} and variable control about axial piston pumps.⁴ A slipper pair is one of the key friction pairs, which provides extremely low friction and high positional accuracy, and is often preferred in an aviation axial-piston pump.

35 In a slipper pair, a fluid film separating the contacting surfaces is maintained by external pressure. The separating film 36 has a high load-carrying capacity and, therefore, does not 37 break down even at extremely low speed during starting, stop-38 39 ping, or changing the direction of rotation. However, an avia-40 tion axial-piston pump generates strengthened interactions 41 among thermal, fluid, and structures in the conversion process from mechanical energy to hydraulic energy at high-pressure 42 and high-rotational speed conditions. The strengthened 43 44 thermal-fluid-structure coupling effect makes the oil viscosity 45 drastically change, the load-carrying capacity drop, lubrication 46 failure, and wear in the slipper pair. Therefore, it is an urgent 47 need to study the load-carrying capacity of the slipper pair.

In the past 40 years, the lubrication performance of a slip-48 per pair in an axial piston pump has been studied from theo-49 retical and experimental aspects. Koc and Hooke⁵ 50 experimentally studied the effects of the clamping ratio and 51 orifice size on the performance of slippers. The results showed 52 that the slippers ran satisfactorily with no orifice and had their 53 54 greatest resistances to tilting couples and minimum film thick-55 ness. Kazama and Yamaguchi⁶ experimentally examined mixed lubrication characteristics of hydrostatic thrust bear-56 57 ings. They measured the frictional force and leakage flow rate under a lubrication range from mixed to fluid film based on an 58 apparatus featuring circular hydrostatic thrust bearings acting 59 on concentric loads. Harris et al.⁷ developed a dynamic model 60 to investigate the dynamic behavior of slipper pads. This 61 model was incorporated into the Computer Aided Pump Per-62 63 formance Analysis (CAPPA) suite of models for use as a part of the simulation package Bathfp, and was used to examine the 64 dynamic stability of slipper pads. It was found that the slipper 65 66 of an axial piston pump ran heavily tilted for high speeds, and touched both the swash-plate and the retaining plate during a 67 pumping cycle. Borghi et al.⁸ investigated the dynamic behav-68 69 ior of a slipper bearing of an axial piston machine. A numerical procedure was used to solve the Reynolds equation with 70 respect to the slipper-swash plate gap. Lu et al.⁹ studied the 71 fluid lubrication characteristics and the anti-turnover ability 72 of a three-cavity independent slipper based on a computational 73 fluid dynamics (CFD) model, taking into account the inertia 74 and the surface roughness. Murrenhoff and Scharf¹⁰ studied 75 the influences of the gaps geometry and their tribological char-76 acteristics on the total efficiency based on a test rig. Deeken¹¹ 77 developed a computer tool DSHplus to evaluate the dynamic 78 behavior of an axial piston machine. The hydraulic character-79 istics and frictions between the key tribo-pairs were analyzed. 80 Canbulut et al.¹² used artificial neural networks to analyze the 81 82 performance of slipper bearings, which included experimental results and a consideration of the elastohydrostatic problem. 83 Manring et al.¹³ experimentally investigated the performance 84 of slippers using different assumed socket geometries at low 85 speed. The results showed that the leakage and capacity were 86 affected by elastic deformation. Nie et al.¹⁴ analyzed the influ-87 ences of structural parameters and running conditions on the 88 wear behavior for a swash plate/slipper pair of a water pump, 89 and drew conclusions by conducting testing. An analytical 90

solution for the hydrostatic leakage and lift characteristic of 91 slippers with multiple lands was outlined by Bergada and Wat-92 ton,¹⁵ and another work by Bergada et al.¹⁶ considered tilt but 93 with no tangential speed effect. Kumar et al.¹⁷ described the 94 static and dynamic characteristics of a piston pump slipper 95 with groove. Three-dimensional Navier-Stokes equations in 96 cylindrical coordinates were applied to the grooved slipper/ 97 swash plate gap. Ma et al.¹⁸ presented a method on the basis 98 of an elasto hydrodynamic lubrication (EHL) model to ana-99 lyze the wear behavior of a swash plate/slipper pair. Based on the analysis of film thickness, the associated internal factors affecting the wear behavior were identified by considering comprehensively structural parameters, working conditions, and material properties. Chen et al.¹⁹ developed a computational fluid dynamics (CFD) simulation method based on a 3-D Navier-Stokes equation and the arbitrary Lagrangian-Eulerian (ALE) method to analyze the grooved slipper performance of a piston pump. Farid Ayada et al.²⁰ performed a parametric study to investigate the effect of the side clearance width on the pump impeller efficiency and head. The pump performance was highlighted through monitoring the changes of the pump head and efficiency. Lin and Hu²¹ proposed a tribo-dynamic model of slipper bearings in axial piston pumps. The tribo-dynamic model was produced that considered the fluid-solid coupling to accurately describe the behavior of slippers. The behavior of the slippers was affected by factors such as the pressure field, the slipper profile, the non-uniform gap between the slipper and the swash plate, external forces and motions, and elastic deformation.

In recent years, Kazama²² investigated the effects of oil 120 physical properties on the thermo-hydrodynamic performance 121 of hybrid thrust bearings and considered various operation 122 conditions. In 2014, the thermo-elasto-hydrodynamic (TEHD) 123 performance of a slipper pair under high pressure and high 124 rotation speed condition was validated using an experimental 125 setup.²³ Meanwhile, the TEHD performance of the slipper pair 126 was studied by solving the Reynolds equation and energy 127 equation using numerical methods. These methods suffered 128 significant limitations, such as wavelet finite element²⁴ or B-129 spline wavelet finite element,²⁵ when advanced fluid-structure 130 coupling and thermal analysis of the slipper pair were dis-131 cussed. Ivantysynova and Huang²⁶ analyzed the elastohydro-132 dynamic effect in the gap flow model of a slipper pair. In 133 2015, a transient TEHD lubrication model for a slipper in an 134 axial piston machine was developed, in which a non-135 isothermal fluid model, the micro dynamic motion of the slip-136 per, as well as pressure and thermal deformation were consid-137 ered,²⁷ and the temperatures at the port and case of the pump 138 were predicted.²⁸ Hashemi et al.²⁹ developed a thermal elasto-139 hydrodynamics and mixed lubrication model for the sliding 140 interface between a slipper and a swash plate in an axial piston 141 pump. A model for calculation of multibody dynamics incor-142 porating a transient, three-dimensional, thermal elastohydro-143 dynamic pivot pad contact in swash plate axial piston pumps 144 was presented. Xu et al.³⁰ established a numerical model of 145 the lubrication between a slipper and a swash plate based on 146 kinematic analysis and laminar flow assumption. This model 147 can calculate the dynamic micro-motion, pressure distribution, 148 and leakage of a slipper/swash-plate friction pair, which helps 149 to reveal the principles for carrying ability and partial abra-150 sion. In 2015,³¹ they used the numerical model of the lubricat-151 ing oil film to study the effect of the case drain pressure on the 152

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