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A novel stability prediction approach for thin-walled component milling considering the material removing process

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- 18 Thin-walled workpiece;
- 19 Vibration

Abstract The milling stability of thin-walled components is an important issue in the aviation manufacturing industry, which greatly limits the removal rate of a workpiece. However, for a thin-walled workpiece, the dynamic characteristics vary at different positions. In addition, the removed part also has influence on determining the modal parameters of the workpiece. Thus, the milling stability is also time-variant. In this work, in order to investigate the time variation of a workpiece's dynamic characteristics, a new computational model is firstly derived by dividing the workpiece into a removed part and a remaining part with the Ritz method. Then, an updated frequency response function is obtained by Lagrange's equation and the corresponding modal parameters are extracted. Finally, multi-mode stability lobes are plotted by the different quadrature method and its accuracy is verified by experiments. The proposed method improves the computational efficiency to predict the time-varying characteristics of a thin-walled workpiece.

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Due to its wide applications in military, energy, and aerospace

industries, milling of thin-walled components is of great signif-

icance. However, the high flexibility of a cutting tool-

workpiece system and improper cutting parameters contribute

to severe vibration, and the most important source of the prob-

lems that emerge during thin-walled components milling is

the cutting amount simultaneously depends on the paths left

by the tooth tips of the current tooth and the previous tooth,

Regenerative chatter is a kind of self-excited vibrations, and

1. Introduction

regenerative chatter.

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so the cutting force varies as well as the chip thickness. There are many methods proposed to predict chatter stability, including frequency-domain methods¹⁻³ and time-domain methods.^{4–8} However, all these studies assumed that the dynamic characteristics of a system did not change during the whole machining process.

As for a thin-walled workpiece, due to the variation of the 38 dynamic characteristic with the motion of the cutter position, 39 the stability also changes during the machining process. Bravo 40 et al.⁹ and Sheng et al.¹⁰ divided the milling process into differ-41 ent stages and obtained frequency response functions (FRFs) 42 43 through an impact test. Although this method would be more 44 accurate, it was almost impractical to conduct enough impact tests to obtain a workpiece's dynamic characteristic during 45 milling. In order to avoid repeated impact tests, a workpiece's 46 47 FRF was updated by the finite element method (FEM).^{11–15} However, this method is of low efficiency since a workpiece 48 49 should be remodeled and correspondingly, modal analysis should also be re-conducted. In this condition, Budak et al.¹⁶ 50 and Song et al.¹⁷ utilized a structural dynamic modification 51 scheme to improve the FEM-based method, where only a 52 workpiece's initial dynamic characteristic was needed. Simi-53 larly, taking into consideration the influence of material 54 removal and the change of the mode shape along the cutting 55 path and tool axis, Yang et al.¹⁸ also obtained in-process 56 workpiece dynamics through structural dynamic modification. 57 58 Neglecting the influence of material removal, Li et al.¹⁹ obtained position-dependent FRFs through the effective stiff-59 ness which was dependent on mode shape. Instead of the com-60 monly adopted FEM, the multispan plate (MSP) mode was 61 proposed to model the varying thickness of a flexible pocket-62 structure.²⁰ Compared with FEM-based methods, the MSP 63 model offers 10-20 times higher computational efficiency. 64 Combining the high computational efficiency of the MSP 65 model and the versatility of FEM-based methods, Ahmadi²¹ 66 67 proposed finite strip modeling (FSM) to model thin-walled structures in pocket milling operations. 68

It is worth noting that due to the change of the mode shape 69 along the cutting path, some specific modes may also affect the 70 71 stability of a thin-walled workpiece. Based on frequency methods, Budak and Altintas²² obtained the stability of a flexible 72 multi-mode structure. However, the dynamic characteristic 73 was assumed as unchanged. Thyenot et al.^{11,12} took the first 74 several modes into consideration and determined the stability 75 limitation by selecting the lowest envelop of each mode. 76 According to Ref. 23, this lowest envelop method (LEM) 77 78 may cause some prediction errors when the modes of a workpiece are not well separated. Zhang et al.²⁴ predicted the stabil-79 ity of a multi-mode cantilever plate and updated the dynamic 80 characteristic by an impact test. Song et al.²⁵ took the influ-81 ences of different modes into consideration. However, material 82 removal was neglected. 83

84 Based on the above literature review, it can be seen that 85 often the dynamic characteristic of a workpiece was obtained 86 by the FEM. Apart from the MSP method, there is no other independent numerical method which is not involved with the 87 FEM. In addition, Refs. 11,12 considering both multi modes 88 and material removal did not give a clear explanation about 89 the relationship between the position, mode shape, and stability 90 limitation. This paper focuses on the mathematic model of a 91 thin-walled flexible part, and tries to conduct theoretical anal-92 ysis of the time-variant modal parameters of the workpiece. 93

The contribution of this paper lies in that the influences of 94 the cutter position and material removal is investigated by the-95 oretical analysis. Since a system does not need to be remodeled 96 during the machining process, compared with the finite ele-97 ment method, the calculation efficiency can be improved a 98 lot. The remainder of this paper is summarized as follows. 99 The equation of motion of the flexible thin-walled part and 100 modal analysis are given in Section 2. Then, the different 101 quadrature method is briefly introduced to calculate stability 102 lobes in Section 3, and the milling stability prediction of flexi-103 ble part milling and experimental results are presented in Section 4. Conclusions are drawn in the last section.

2. Time-varying model of thin-walled plate

As shown in Fig. 1, during the milling process, the material is 107 continuously removed along the trajectory of the moving cut-108 ter. Correspondingly, the workpiece's dynamic characteristics. 109 such as natural frequency and stiffness, also change during this 110 process. In this section, different from Refs. 16-18, where the 111 FEM is used to conduct modal analysis, a more efficient 112 method is proposed to obtain the dynamic characteristics of 113 the workpiece. 114

In Fig. 1, a cantilevered thin-walled rectangular plate under 116 milling machining, with a length of L, a width of W, and a 117 thickness of h, is modeled. The spindle speed is Ω and the feed 118 rate is c. The classical plate theory, which is suitable for thin-119 walled plate analysis, is used, and only the bending effect of the 120 thin-walled plate is considered. Since, during the milling pro-121 cess, the material is removed as the cutter moves along the cut-122 ting path, the shape of the plate is varying during this period. 123 However, it is lucky that the shape of the plate is predictable, 124 and the material removal volume is relatively small compared 125 to that of the unprocessed plate. Therefore, it is reasonable to 126 assume that the plate's modal shape is unchanged and corre-127 spondingly, the kinetic energy, T, of the machined plate can 128 be expressed as 129 130

$$T = \frac{\rho h}{2} \iint_{\mathcal{A}} \dot{w}^2 dx dy - \frac{\rho h_r}{2} \iint_{\mathcal{A}_r(t)} \dot{w}^2 dx dy \tag{1}$$

where ρ is the density, h_r is the thickness of the removed part, 133 namely the radial cutting depth, w is the displacement along z134 direction, and the over-dot denotes differentiation with respect 135



Fig. 1 Model of a cantilevered plate.

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