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Experimental study of curvature effects on jet impingement heat transfer on concave surfaces

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Abstract Experimental study of the local and average heat transfer characteristics of a single round jet impinging on the concave surfaces was conducted in this work to gain in-depth knowledge of the curvature effects. The experiments were conducted by employing a piccolo tube with one single jet hole over a wide range of parameters: jet Reynolds number from 27,000 to 130,000, relative nozzle to surface distance from 3.3 to 30, and relative surface curvature from 0.005 to 0.030. Experimental results indicate that the surface curvature has opposite effects on heat transfer characteristics. On one hand, an increase of relative nozzle to surface distance (increasing jet diameter in fact) enhances the average heat transfer around the surface for the same curved surface. On the other hand, the average Nusselt number decreases as relative nozzle to surface distance increases for a fixed jet diameter. Finally, experimental data-based correlations of the average Nusselt number over the curved surface were obtained with consideration of surface curvature effect. This work contributes to a better understanding of the curvature effects on heat transfer of a round jet impingement on concave surfaces, which is of high importance to the design of the aircraft anti-icing system.

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19 1. Introduction

Heat transfer associated with jet impingement on a flat or curved surface has been the subject of extensive investigation

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for decades because of its enhanced local heat exchange performance in a wide variety of applications such as glass tempering, metal annealing, and engine and turbine blades cooling.^{1,2} Impinging jets are also used in the hot-air antiicing system of commercial aircraft where high-pressure hot air, bleeding from the engine, is ducted forward to a pipe with several small holes on it and impinges on the inner surface of the anti-icing cavity to heat the leading edge of wing. Since the anti-icing cavity is a curved surface, the effect of surface curvature should be taken into account when the jet impingement heat transfer performance is considered.

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Many experiments were designed to study the heat transfer 33 34 of impingement jets, with a focus on flat plates. The very early experimental work for the flat plate case were represented by 35 Gardon³, Goldstein⁴, Hrycak⁵ and Beltaos et al.⁶ with varying 36 37 impingement distance, Reynolds number and oblique angle. Many measurement techniques based on naphthalene sublima-38 tion technique⁷, temperature-sensitive liquid crystal^{8,9} and 39 thermal infrared camera^{10,11} were adopted to measure and 40 analyze the flow and heat transfer characteristics. 41

Metzger et al.¹² were probably the first to experimentally 42 investigate the heat transfer characteristics of jets impinging 43 44 on a concave cylindrical surface. The average heat transfer 45 coefficient of single lines of circular jets was obtained with var-46 ied ratios of nozzle to surface distance H and nozzle diameter d at the Reynolds range from 1150 to 5500. Results indicated 47 that the maximum heat transfer could be obtained at the opti-48 49 mum relative nozzle to surface H/d = 3-5, whose value 50 decreased with increasing Reynolds number. Compared with 51 the heat transfer performance on a flat plate, the stagnation point Nusselt number was higher on the concave cylindrical 52 surface as reported by Hrvcak.¹³ Mayle et al.¹⁴ also presented 53 that the heat transferred to the boundary layer on the concave 54 plate was greater than that on a flat plate. 55

Flow visualization facilities with smoke generation wire 56 were applied by Gau and Chung¹⁵ and Cornaro et al.¹⁶ to visu-57 alize the flow structure of slot and round jet impinging on con-58 59 cave surfaces. The former result showed that the Nusselt 60 number increased with increasing surface curvature for slot jet impingement on a concave surface, which was caused by 61 the initiation of Taylor-Görtler vortices along the surface. Sim-62 ilar observation was also obtained by Cornaro et al.¹⁶, who 63 also found that the heat transfer rate on and around the stag-64 65 nation point increased with increasing surface curvature. Lee et al.¹⁷ experimentally investigated the local heat transfer from 66 67 a long round jet impinging on a smaller relative curvature sur-68 face (d/D = 0.034, 0.056, 0.089) with jet Reynolds number from 11,000 to 50,000. Similarly Yang et al.¹⁸ investigated 69 the concave effect but using a slot jet in the range $5920 \le Re_i$ 70 < 25,500, with a fixed slot-width to diameter ratio of 0.033. 71 72 Their conclusions were consistent and indicated that the sur-73 face curvature and generation of Taylor-Görtler vortices were 74 able to thin the boundary layer and enhance the heat transfer rates further in the downstream region apart from the stagna-75 tion point. 76

Since last decade, impinging jets have been applied to hot-77 air anti-icing system of aircraft and much progress has been 78 achieved. Brown et al.¹⁹ experimentally investigated the heat 79 transfer in an aircraft nacelle anti-icing system and a correla-80 tion of average Nusselt number on the impingement area 81 was presented with consideration of the distance between the 82 jet holes and the jet Reynolds number. Papadakis et al.^{20,21} 83 conducted experiments in the NASA Glenn Icing Research 84 85 Tunnel for a range of external conditions representative of 86 inflight icing. The effects of hot air mass flow and temperature, 87 angle of attack, tunnel airspeed and piccolo jet circumferential placement were investigated. Imbriale et al.²² used IR ther-88 mography to measure 3D surface heat transfer coefficients 89 by a row of jets impinging on a concave surface, representing 90 an airfoil leading edge, and the influences of jet inclination, jet 91 pitch and Reynolds number were analyzed. A more recent 92 study by Bu et al.²³ investigated the heat transfer characteris-93 tics of jet impingement on a variable-curvature concave surface 94

of a wing's leading edge experimentally. Parameters including jet Reynolds number, relative nozzle-to-surface distance and jet circumferential placement were considered for the effects on local Nusselt number distributions.

All of above researches indicated an enhanced heat transfer performance of jet impingement on concave surfaces. However the confinement effect of concave surface, which could decrease the heat transfer effect, was seldom studied. When studying 3D temperature distribution of a concave semicylindrical surface impinged by round jets, Fenot²⁴ noticed that the confinement effect actually reduced heat transfer as the average Nusselt number for the flat plate was higher than that for the curved plate. It was believed that the confinement prevented ambient air from mixing with the jet air, and thereby increased the flow temperature. The range of Reynolds number was from 10,000 to 23,000, and the relative surface curvature d/D = 0.10, 0.15, 0.20 and H/d = 2-5.

Öztekin et al.²⁵ investigated the heat transfer characteristics of slot jet impingement on concave surface for jet Reynolds number from 3423 to 9485 and the dimensionless surface curvature R/L = 0.50, 0.75 and 1.30, where R was the surface radius and L the surface trace length. Results indicated that, compared with the flat plate, the average Nusselt number along the concave surface was larger when R/L = 0.75 and 1.30. The average Nusselt number increased with increasing dimensionless surface curvature R/L, in other words, with decreasing relative surface curvature d/D. A slight increase in Nusslet number with decreasing d/D was also observed in Martin and wright's experiment²⁶ with single row of round jets impingement on a cylindrical surface. This trend was more prevalent for larger nozzle to surface distances in the range of jet Reynolds number from 5000 to 20,000, relative nozzle to nozzle spacing from 2 to 8, nozzle to surface distance from 2 to 8, and d/D = 0.18, 0.28.

As briefly reviewed above, although different studies have 129 shown that surface curvature enhanced the heat transfer, 130 detailed mechanism of heat transfer decay on a concave sur-131 face is still not well understood. This work conducted an exten-132 sive experimental study focusing on the curvature effect along 133 the curved surface. By analyzing the stagnation point Nusselt 134 number, and the average and local Nusselt number distribu-135 tions in chordwise and spanwise directions, both the enhance-136 ment and confinement effects of the surface curvature were 137 investigated. In addition, experimental data-based correlations 138 of the average Nusselt number over the curved surface with consideration of the surface curvature effect were presented and experimentally verified.

2. Experimental apparatus

Fig. 1 schematically shows the jet impinging system used in 143 this investigation. The main elements of the experimental 144 apparatus were a steel pipe with a round nozzle on it and an 145 impingement surface. Both were mounted on independent 146 brackets to keep the surface horizontal and the pipe vertically 147 removable for different nozzle to surface distances. As indi-148 cated in Fig. 1, the high pressure air from the air compressor 149 became much cleaner and more stable after passing through 150 the filter and air tank, and then went through the electronic 151 pressure regulator where its pressure was adjusted to the 152 desired value. The adjusted air flowed into the pipe from one 153

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