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Enhanced wave and finite element method for wave propagation and forced response prediction in periodic piezoelectric structures

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- 21 Wave and finite element
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14 15 **Abstract** As a promising numerical tool of structural dynamics in mid- and high frequencies, the wave and finite element method (WFEM) is receiving increasingly attention and applications. In this paper, an enhanced WFEM has been developed with a reduced model and a new eigenvalue scheme. The reduced model is applicable for structures with piezoelectric shunts or local dampers; the new eigenvalue scheme can mitigate the ill-conditioning when the wave basis is calculated. The enhanced WFEM is applied to a thin-wall structure with periodically distributed piezoelectric materials (PZT). Both free wave characteristics and forced response are analyzed and the influences of the suggested enhancements are presented. It is shown that if the control factors are properly chosen, these enhancements can improve the accuracy while accelerating the calculation. Resulting from the complexity of the application, these enhancements are not optional but imperative.

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1. Introduction

system.

For a problem concerning structural dynamics, it is always possible, at least in principle, to arrive at the same conclusions

by either mode or wave approach. This equivalence is termed

"wave-mode duality" in the literature,¹ and it can be theoreti-

cally demonstrated in some simple cases.^{1,2} In spite of that,

each approach has its own advantages and each provides dif-

ferent views for understanding the same dynamic structural

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At low frequencies, a structure can be regarded as a closed system. The structural motion is dominated by well-separated global stationary modes, so it is reasonable to understand the dynamic deformation of a structure as the superposition of modal motions. For a discrete structural model, the number of modes equals the overall number of degrees-of-freedom (DOFs). However, most of the high-order modes hardly contribute to the deformation. It is therefore possible to reduce the size of the problem by truncating modes.^{3–5} In terms of vibration control, the guidelines given by the mode approach is to control the vibration of a single mode or multiple modes.^{6,7}

45 Alternatively, in the wave perception, structural deformation is regarded as the superposition of the wave motions. 46 while natural modes are understood as standing waves induced 47 by the reflection of waves on the boundaries.⁸ At higher fre-48 quencies, the waves could be transmitted through the bound-49 50 aries and power is radiated or absorbed in the remote parts 51 of the structure.⁹ Then the structure is more suitable to be treated as an open system where resonance behavior is less appar-52 ent. It is then more reasonable to employ the wave approach. 53 The guideline given by the wave approach for vibration reduc-54 tion is to modify the wave properties in the interested fre-55 quency band so as to dissipate or localize the injected 56 energy.^{10,11} This idea has drawn considerable research atten-57 tion these years with the development of the periodic structures 58 or phononic materials.¹² Since the waves are independent of 59 the boundary conditions, the vibration reduction performance 60 induced by waves is insensitive to boundary conditions as 61 well.¹³ 62

The forced response of a structure can be predicted by the 63 wave approach if the structure is periodic.^{14,15} If the structure 64 is partly periodic, for example a structure with several different 65 periodic substructures or a structure with both periodic parts 66 67 and non-periodic parts, wave approach can still be applied by the diffusion matrix method¹⁶ or hybrid WFEM/FEM 68 (wave and finite element method/finite element method).¹⁷ 69 If the structure is near periodic, for example a periodic struc-70 ture with spatially homogeneous random properties, the wave 71 approaches can also be used. A promising method named 72 stochastic wave finite element^{19,20} (SWFE) addresses this prob-73 lem by a hybridization of the deterministic wave finite element 74 and a parametric probabilistic approach. If the structure is 75 generally non-periodic, a homogenization approach can be 76 performed, leading to an equivalent uniform/periodic structure 77 and the wave approaches can be applied. In this case, the 78 79 obtained wave characteristics represent the low frequency global behavior of the original structure. The main advantage of 80 using the wave approach is that a periodic structure/substruc-81 ture can be analyzed by only modeling the smallest repetitive 82 unit cell. In comparison with the full model of the structure/-83 substructure, the dimension of problem is significantly reduced 84 85 and the computing is therefore accelerated. This feature makes 86 the wave approach a promising method in mid- and high fre-87 quency structural analysis²¹ when full FE analysis is rather time-consuming. 88

To manually obtain the desired wave dispersion characteristics, periodically distributed piezoelectric patches with electric circuits have already been considered in the literature.^{22–24} Piezoelectric materials have the ability to transform mechanical energy to electrical one and vice versa.²⁵ This allows one to drastically modify the modal and wave characteristics especially when semi-active circuits are employed.^{13,26}

In all these applications concerning wave approach, the core information is the wave characteristics of the structure. That is, at a given frequency, which waves exist in the structure and how they travel (wavenumbers and wave shapes). Analytical formulas can be found for relatively simple cases.²⁷⁻²⁹ For periodic structures with complex configurations, for example the uniform thin-wall structure studied by Houillon et al.³⁰, the analytical solutions are of limited value, particularly at higher frequencies. In recent years, WFEM has been developed to access the wave characteristics of the periodic structures.¹⁵ In WFEM, a unit cell is firstly modeled by FEM and the Bloch theory is then imposed. It finally leads to an eigenvalue problem, yielding the frequency, wavenumbers and wave shapes. WFEM has been applied to 1D periodic structures,³ plates,^{32,33} thin-wall structures,³⁰ piezoelectric structures¹⁷ and fluid-filled pipes.³⁴ The experimental studies have also been conducted concerning the wave characteristics of the perforated plates³⁵, ribbed panels³⁶ and 1D piezoelectric waveguides.³⁷ The dispersion curves can be recognized by a spatial Fourier transform of the steady-state response of the finite structure; the results match very well with the numerical results in the aforementioned studies.

However, WFEM still has a series of numerical issues^{38,39} including matrix ill-conditioning in free wave analysis and the incorrect estimation of strongly evanescent waves in forced response analysis. Moreover, if the number of DOFs in the FE mesh of the unit cell is numerous, the computing will become slow.

To overcome the matrix ill-conditioning while analyzing the free waves, several eigenvalue schemes have been suggested^{10,40} and they mitigate the problem to some extent. To improve the accuracy of the forced response analysis, it is suggested to truncate the wave basis^{41,42} so that only the propagating and less-decaying waves are retained. However, the methods have only been validated on rather simple structures. To accelerate the WFEM, reduced models have been developed, and the coordinates transfer matrix can be formed by the wave shapes at selected frequencies⁴³ or the modal shapes of a unit cell³¹ with all the DOFs connecting the adjacent cells fixed. However, the former strongly depends on the selection of waves and the latter is not applicable when there are local dampers or piezoelectric shunts inside the unit cell.

In this paper, an enhanced WFEM has been developed with a reduced model which works for piezoelectric structures. A new eigenvalue formula is proposed to further improve the accuracy of the scheme used in the literature.^{10,31,43} The method is applied to a thin-wall structure with periodically distributed piezoelectric patches shunted by identical circuits. The method is validated not only by comparing the dispersion curves but also by checking an energy criterion featured by piezoelectric systems. The forced response of the structure is conducted by WFEM, where the influences of the factors, such as the number of the retained modes, eigenvalue scheme and the number of the kept waves, are separately presented and discussed. Eventually the guidelines for choosing the factors are given. Download English Version:

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