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Sound insulation performance of plates with interconnected distributed piezoelectric patches

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Abstract This paper deals with the sound insulation performance of a thin plate with interconnected distributed piezoelectric patches. Piezoelectric patches are periodically bonded on the surfaces of the plate in a collocated fashion, and are interconnected via an inductive circuit network. This piezoelectric system is termed as piezo-electromechanical (PEM) plate in the paper. Homogenization methods are involved under a sub-wavelength assumption to analytically develop the dynamical equations for the PEM plate. The dispersion relationships and energy densities of the wave modes propagating in the PEM plate are studied; the sub-wavelength assumption is verified for the simulations in this paper. The coincidence frequency of the PEM plate is researched, and results show that the coincidence frequency of the PEM plate will disappear at certain circumstances; mathematical and physical explanations are made for this phenomenon. The disappearance of the coincidence frequency is used to optimize the value of inductance, for the purpose of improving the sound transmission loss of the PEM plate.

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19 1. Introduction

The intensive uses of light plate-like structures in aerospace and transportation industries result in more serious vibration and noise issues for their higher dynamical sensitivities. To

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deal with these problems, techniques based on piezoelectric materials have been proposed and numerous papers have contributed to their developments and applications. In these applications, localized piezoelectric shunt techniques^{1–8} and periodic distributed piezoelectric control techniques^{9–34} have attracted a lot of attention. Among periodic distributed piezoelectric control techniques, two kinds of strategies can be found in the literature. The first one only uses separated shunted piezoelectric patches, and the second one interconnects all the distributed piezoelectric transducers via a circuit network.

The idea of using separated periodic shunted piezoelectric patches was proposed by Thorp et al.¹⁰ They periodically placed shunted piezoelectric patches along rods to control

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103

37 the longitudinal wave propagation. They found that at certain 38 frequency ranges (namely the stop bands) no propagative longitudinal waves existed and these stop bands could be extended 39 or relocated by tuning the shunting inductive/resistive circuits. 40 Later, this concept has been extended to flexural beams^{11,12} 41 and plates.^{13,14} Distributed shunted piezoelectric patches were 42 also exploited to control energy flow in structures.^{15–21} In Col-43 let et al.'s work,¹⁵ piezoelectric patches were distributed on a 44 host beam to form a periodic piezo-composite beam; this func-45 tional beam was connected with a passive beam with identical 46 47 parameters to the host beam. It was found that at the interface 48 of these two different beams, total reflection or total absorp-49 tion of certain types of waves incident from the passive beam could be achieved by tuning the shunting parameters. In 50 another work of Collet et al.¹⁷, an interface composed of a host 51 plate and periodically distributed piezoelectric patches shunted 52 53 with negative capacitance and resistance was designed. This 54 semi-active interface was arranged between two passive plates 55 to diminish energy translation from one passive domain to another one by trapping waves at their original domains or dis-56 sipating them. Its effectiveness was further verified by experi-57 ments in Tateo et al.'s work.^{18,19} More recently, distributed 58 shunted piezoelectric patches were successfully employed to 59 focus waves by using gradient shunting parameters.²¹ Along 60 with the control of vibration and waves, periodic shunted 61 piezoelectric patches were also used in the noise control 62 domain. Casadei et al.²² numerically and experimentally inves-63 tigated the application of a periodic array of resistive-induc-64 tive (RL) shunted piezoelectric patches for the attenuation of 65 broadband noise radiated by a flexible plate in an enclosed 66 cavity. They demonstrated that the noise radiated by the plate 67 was significantly attenuated. Zhang et al.²³ studied the sound 68 transmission loss (STL) of a thin plate with periodically dis-69 tributed piezoelectric patches shunted by an inductive circuit, 70

and their results showed that the STL of the thin plate could
be improved within the mass-law region and the coincidence
region.
Interconnected distributed piezoelectric patches were
mainly researched by Dell'Isola et al.^{24–34} Firstly, they periodically distributed piezoelectric actuators in a truss and interconnected them by circuits. This integrated structure was

77 called piezo-electromechanical (PEM) truss in their paper.²⁴ 78 79 Research shows that there are waves in both the mechanical structure and the electric networks, and the maximum 80 electro-mechanical coupling factor occurs when the speeds of 81 the waves in these two mediums approach. Later, they 82 extended this interconnected distributed configuration to 83 beams and plates to build PEM beams^{25,26,29,31,32} and PEM 84 plates.^{27,28,30,33,34} Results show that in these structures, inter-85 nal resonances exist between the mechanical and electrical 86 parts and multimode control effectiveness can be obtained 87 by delicately designing the electric networks.^{24,31–33} 88

89 However, previous works that used distributed piezoelectric 90 techniques mainly focused on controlling vibration, associated 91 sound radiation, or wave propagation in the structures, and few of research concerned the control of sound transmission 92 especially by using interconnected distributed piezoelectric 93 patches. In this paper, the sound insulation performances of 94 a thin plate with interconnected distributed piezoelectric 95 patches are studied. Firstly, the analytical dynamical equations 96 97 for this PEM plate are established by using homogenization methods under a sub-wavelength assumption (Section 2). 98

Then, the dispersion relationships and energy densities of wave99modes propagating in the PEM plate are analyzed and the sub-100wavelength assumption is verified (Section 3). At last, the coin-101cidence frequency as well as the STL is studied (Section 4).102

2. Model and dynamical equations

Consider an infinite thin plate lying in x - y plane; its upper 105 and lower surfaces are periodically bonded with piezoelectric 106 patches to constitute a piezoelectric composite plate, as shown 107 in Fig. 1. A detailed configuration of one unit piezoelectric cell 108 in this composite plate is illustrated in Fig. 2. The piezoelectric 109 patches on both sides of the thin plate are respectively inter-110 connected with their horizontal and vertical adjacent transduc-111 ers via a circuit network shown in Fig. 3. In the circuit 112 network, only inductors are used and they are all identical. 113 The bonding surfaces of the piezoelectric patches are 114 grounded, and the free electrodes are directly connected with 115 the circuit network. For example, the free electrodes of the 116 piezoelectric patches in the unit cells (m,n), (m+1,n), 117 (m, n+1), and (m+1, n+1) in Fig. 1 are respectively con-118 nected with the corresponding intersections (m, n), (m + 1, n), 119 (m, n+1), and (m+1, n+1) in Fig. 3. The piezoelectric com-120 posite plate and the circuit network together construct a new 121 functional system, which is called piezo-electromechanical 122 plate in this paper, or PEM plate for short as in Refs. 30, 33 123

Assume that the wavelengths corresponding to the frequen-124 cies under consideration are much greater than the length of 125 the unit cell. Under this sub-wavelength assumption, an ana-126 lytical model is developed for the PEM plate. In the analytical 127 model, an approximation method is employed to deal with the 128 circuit network, which has been widely used in modelling of 129 PEM structures,^{29–33,35} and its effectiveness in characterizing 130 the global dynamic behaviors of circuit networks has been 131 experimentally demonstrated in Refs. 31, 35 The piezoelectric 132 composite plate is homogenized through a well-validated 133 method used in Refs. 21, 23, and after the homogenization, 134 the composite plate can be treated as a homogeneous structure 135 with equivalent dynamical parameters. The modelling process 136 is introduced below, and for the sake of simplicity, a subscript 137 comma is used to indicate the partial differential with respect 138



Fig. 1 Piezoelectric composite plate.

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