

Chinese Society of Aeronautics and Astronautics & Beihang University

Chinese Journal of Aeronautics

cja@buaa.edu.cn www.sciencedirect.com

JOURNAL

Discretized Miller approach to assess effects on boundary layer ingestion induced distortion

Esteban Valencia^{a,*}, Víctor Hidalgo^a, Devaiah Nalianda^b, Laskaridis Panagiotis^b, 5 Riti Singh^b

7 ^a Departamento de Ingeniería Mecánica, Facultad de Ingeniería Mecánica, Escuela Politécnica Nacional, Ladron de Guevara

E11-253, Quito 17-01-2759, Ecuador 8

^b School of Engineering, Cranfield University, Bedford MK43 0AL, United Kingdom g

10 Received 19 November 2015; revised 27 June 2016; accepted 19 October 2016

KEYWORDS

- 13 14 15 BL1
- 16 Correlations;
- Distortion; 17
- 18 Embedded propulsors;
- 19 Empirical;
- 20 Mean-line analysis;
- Turbomachinery 21

22

3

11

Abstract The performance of propulsion configurations with boundary layer ingestion (BLI) is affected to a large extent by the level of distortion in the inlet flow field. Through flow methods and parallel compressor have been used in the past to calculate the effects of this aerodynamic integration issue on the fan performance; however high-fidelity through flow methods are computationally expensive, which limits their use at preliminary design stage. On the other hand, parallel compressor has been developed to assess only circumferential distortion. This paper introduces a discretized semi-empirical performance method, which uses empirical correlations for blade and performance calculations. This tool discretizes the inlet region in radial and circumferential directions enabling the assessment of deterioration in fan performance caused by the combined effect of both distortion patterns. This paper initially studies the accuracy and suitability of the semiempirical discretized method by comparing its predictions with CFD and experimental data for a baseline case working under distorted and undistorted conditions. Then a test case is examined, which corresponds to the propulsor fan of a distributed propulsion system with BLI. The results obtained from the validation study show a good agreement with the experimental and CFD results under design point conditions.

© 2016 Production and hosting by Elsevier Ltd. on behalf of Chinese Society of Aeronautics and Astronautics. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/ licenses/by-nc-nd/4.0/).

The performance of axial fans under distorted conditions has

been studied extensively in the past. Different approaches

and tools such as through flow methods,¹ semi-empirical cor-

relations,² and fan map based methods (parallel compressor³)

have been utilized to assess their performance. It has been

found that even though through flow methods such as stream-

1. Introduction

24

25

26

27

28

29

Corresponding author.

E-mail address: esteban.valencia@epn.edu.ec (E. Valencia). Peer review under responsibility of Editorial Committee of CJA.

ELSEVIER Production and hosting by Elsevier

http://dx.doi.org/10.1016/j.cja.2016.12.005

1000-9361 © 2016 Production and hosting by Elsevier Ltd. on behalf of Chinese Society of Aeronautics and Astronautics. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

Please cite this article in press as: Valencia E et al. Discretized Miller approach to assess effects on boundary layer ingestion induced distortion, Chin J Aeronaut (2016), http://dx.doi.org/10.1016/j.cja.2016.12.005

ARTICLE IN PRESS

2

i	incidence, $\beta_{LE} - \beta'_{LE}$	$k-\varepsilon$	k-epsilon turbulence model
С	absolute flow velocity, m/s	k–ω	k- ω turbulence model
Р	total pressure, Pa	Н	H grid type
р	static pressure, Pa	С	C grid type
T	total temperature, K	0	O grid type
t	static temperature, K	ATM	automatic topology and meshing
()f	fan property	$P_{\rm BI}$	total pressure in the boundary layer region at
ŐD	off design conditions	DL	propulsor intake
BLI	boundary layer ingestion	$M_{\rm BL}$	Mach number in the boundary layer region at
3	deflection, $\beta_{\rm LE}$ - $\beta_{\rm TE}$	BE	propulsor intake
β	relative air angle	M_{∞}	Mach number at free stream conditions
V	relative velocity, m/s	P_{∞}	total pressure at free stream conditions
U	tangential velocity, m/s	TeDP	turboelectric distributed propulsion
C_a	axial velocity	у	perpendicular distance from the wall, m
α	absolute air angle	$C_{\rm cl}$	airframe length
δ	deviation angle, $\beta_{\rm TE} - \beta'_{\rm TE}$	$R_{\rm c}$	Reynolds number
ω	total loss coefficient	ψ	flow coefficient
ω_{p}	profile loss coefficient	CFD	computational fluid dynamics
$\omega_{\rm sec}$	secondary loss coefficient	BL	boundary layer
$\omega_{\rm sw}$	shock wave loss coefficient	DM	discretized Miller
$\Delta P_{\rm ideal}$	ideal total pressure increment, Pa	DC ₁₂₀	distortion coefficient for 120°
$\Delta P_{\rm real}$	real total pressure increment, Pa	θ	angular position, rad or °
$P'_{\rm LE}$	ideal total pressure at leading edge, Pa	ml	minimum loss
$P_{\rm LE}$	total pressure at leading edge, Pa	'n	mass flow
$\bar{\omega}$	average total loss coefficient	r _{rt}	root to tip ratio
$\omega_{\rm p, par}$	parametric profile loss coefficient	FPR	fan pressure ratio
$\omega_{\rm ew, par}$	parametric end wall loss coefficient	$V_{\rm tip}$	tip velocity, m/s
$V_{\rm LE}$	relative velocity at leading edge	$\eta_{\rm f}$	fan efficiency
$V_{\rm TE}$	relative velocity at trailing edge	DP	design point
$\beta_{\rm TE}$	relative air angle at trailing edge	NB	number of blades
$\beta'_{\rm TE}$	relative blade angle at trailing edge	$r_{\rm t}$	tip radius, m
h	blade height, m	r _r	root radius, m
С	blade chord, m	01	properties at rotor entry
h/c	blade aspect ratio	02	properties at stator entry
r	radius, m	TSFC	thrust specific fuel consumption
y^+	dimensionless distance of the node from the wall		

line curvature^{4,5} and CFD can predict fan performance with 30 31 higher accuracy than other methods, they also require more resources in terms of computational power and time. For 32 boundary layer ingestion (BLI) systems, streamline curvature 33 and parallel compressor have been combined in order to assess 34 circumferential and radial distortion.⁴ In the case of CFD, this 35 tool enables the assessment of the fan performance radially 36 37 and circumferentially, and for this reason CFD has also been 38 utilized for the assessment of BLI distortion problems. This 39 approach has been preferred for cases where the detailed 40 geometry is known and accuracy is paramount. In this study, 41 CFD has been used to compare some results obtained under 42 uniform conditions with the discretized Miller approach. Some experimental test-rigs have been set for the assessment of BLI 43 type distortion; however testing engines or in this case fans are 44 expensive and the cost increases with advanced engine technol-45 ogy and designs. Furthermore, the cost of the energy required 46 for each run and the possibility of damaging the tested equip-47 ment increase the difficulty of carrying out these procedures. 48 Jerez et al.¹ experimentally studied the validation of a CFD 49

model for a fan working under distortion. Redmond⁶ described a test-rig and experimental results for BLI type distortion; however in this latter case, the uncertainties achieved are large and it is difficult to assess the real benefits of BLI.

At the preliminary design stage when the detailed geometry of a system/component is still undefined and several configurations have to be tested, reducing requirements of computational resources becomes imperative.

Due to excessive simulation times, these methods have also been found unsuitable in cases where full annular simulation is required and circumferential distortion is present (such as in boundary layer ingesting systems^{7–9}). These reasons, therefore, make methods such as the parallel compressor³ more attractive for preliminary design at design point. However, this method has its limitations, as it only enables to assess circumferential distortion. Hence it may be considered to have limited accuracy in the case of BLI systems where a combination of circumferential and radial distortion of flow is observed.

This paper addresses this limitation of the method and proposes a novel approach to overcome it. Using a semi-empirical

67

68

69

50

51

Download English Version:

https://daneshyari.com/en/article/7154177

Download Persian Version:

https://daneshyari.com/article/7154177

Daneshyari.com