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## FULL LENGTH ARTICLE

# **Turbulent boundary layer separation control using** plasma actuator at Reynolds number 2,000,000

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15 Dielectric barrier discharge;

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- 17 Plasma actuator;
- 18 Turbulent boundary layer;
- 19 Wing-body configuration

Abstract An experimental investigation was conducted to evaluate the effect of symmetrical plasma actuators on turbulent boundary layer separation control at high Reynolds number. Compared with the traditional control method of plasma actuator, the whole test model was made of aluminum and acted as a covered electrode of the symmetrical plasma actuator. The experimental study of plasma actuators' effect on surrounding air, a canonical zero-pressure gradient turbulent boundary, was carried out using particle image velocimetry (PIV) and laser Doppler velocimetry (LDV) in the 0.75 m  $\times$  0.75 m low speed wind tunnel to reveal the symmetrical plasma actuator characterization in an external flow. A half model of wing-body configuration was experimentally investigated in the  $\emptyset$  3.2 m low speed wind tunnel with a six-component strain gauge balance and PIV. The results show that the turbulent boundary layer separation of wing can be obviously suppressed and the maximum lift coefficient is improved at high Reynolds number with the symmetrical plasma actuator. It turns out that the maximum lift coefficient increased by approximately 8.98% and the stall angle of attack was delayed by approximately 2° at Reynolds number  $2 \times 10^6$ . The effective mechanism for the turbulent separation control by the symmetrical plasma actuators is to induce the vortex near the wing surface which could create the relatively largescale disturbance and promote momentum mixing between low speed flow and main flow regions. © 2016 Chinese Society of Aeronautics and Astronautics. Production and hosting by Elsevier Ltd. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

Currently, active flow control (AFC) technology is a popular

method that can improve the aircraft aerodynamics perfor-

mance without added drag and also liberate designers from

method has been extensively proved to be a promising AFC

technology<sup>1</sup> in the field of separation control for wing,<sup>2,3</sup> lift

Dielectric barrier discharge (DBD) plasma flow control

the restriction of traditional aerodynamic design.

#### 1. Introduction

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enhancement<sup>4,5</sup> and separation flow control for airfoil,<sup>6</sup> 29 boundary layer control,<sup>7-10</sup> separation control for low-30 pressure turbine blades,<sup>11</sup> control of bluff body,<sup>12–14</sup> control of compressor cascade,<sup>15,16</sup> control of broadband noise,<sup>17</sup> 31 32 and control of jet diffusers.<sup>18</sup> Compared with the traditional 33 AFC technology, the benefits of plasma actuator are obvious, 34 such as simple structure without moving parts and rapid 35 response. Remarkable reviews on plasma flow control technol-36 ogy have been published lately.<sup>19-2</sup> 37

Separation control of wing using plasma actuators at low-38 middle Reynolds number was investigated by numerous research-39 ers with experimental and computational methods.<sup>22-32</sup> By 40 41 numerical simulation method, Asada and Fujii made an investigation on the laminar separation control by a plasma actuator 42 around NACA 0015 at Reynolds number 63,000 recently.<sup>33</sup> They 43 indicated that the plasma actuation can promote the transition to 44 45 turbulence at the laminar separation shear layer more effectively 46 and then the turbulent mixing led to early reattachment of the separated flow. The effect of the location and operating conditions of 47 the plasma actuator was widely studied by Sato et al.<sup>34</sup> It was 48 found that the most effective location is just upstream of the nat-49 ural separation point. The deep stall flow control was investigated 50 by Aono et al. at Reynolds number 260,000.<sup>35</sup> They carried out an 51 optimization study of the burst frequency of the plasma actuator 52 and proved the applicability of the plasma actuator for control of 53 54 the laminar separated flow at middle Reynolds number. It was 55 suggested that the optimum burst frequency becomes higher than that at low Reynolds number. From these investigations, the pro-56 57 motion of the turbulent transition at the shear-layer is the key for effective laminar-separation control with the plasma actuator at 58 low-middle Reynolds number.35 59

However, some researchers could question the applications 60 61 of the plasma actuator. Because the Reynolds number of real airplane is usually over  $10^6$  that could be beyond the plasma 62 63 authority from the literature. In order to meet the requests 64 of engineering application, the plasma authority must be 65 improved at higher Reynolds number. In this high Reynolds 66 number zone, flow is often separated in turbulence but not 67 in laminar. Therefore, the separation characteristics are different from the laminar separation. It is not clear whether the 68 69 same tactic for the laminar separation control at low-middle Reynolds number could be suitable for the turbulence separa-70 tion control. 71

The purpose of this investigation was to study the turbulent 72 boundary layer separation control over a wing-body configu-73 ration using a symmetrical plasma actuator at Reynolds num-74 75 ber  $2 \times 10^6$ . The integral control effect of the symmetrical plasma actuator is described by the force measurements and 76 particle image velocimetry (PIV) results. Moreover, this paper 77 highlights how the induced airflow by the plasma actuator 78 79 interacts with the boundary layer with laser Doppler velocimetry (LDV) technology and smoke visualization, and discusses 80 81 the controlling mechanism of the plasma actuator.

#### 82 2. DBD plasma actuator

Classical DBD plasma actuator comprises an upper electrode
and a lower electrode that are separated by insulating material.
One of the electrodes is exposed to the ambient air and the
other is completely encapsulated by dielectric material (Fig. 1
(a)). When a high voltage power supply is applied to the two



(b) Symmetrical DBD plasma actuator

Fig. 1 Electrodes configuration of DBD plasma actuators.

electrodes, ionized air (plasma) at the edge of the exposed electrode is produced. The plasma covers the region projected by the covered electrode. As a result of the electric field gradient, the plasma produces a body force<sup>36–38</sup> that acts on the surrounding air and induces the airflow in the direction from the upper electrode towards the lower electrode.<sup>39,40</sup> The process of ionizing the air at this configuration is referred to as DBD. Fig. 2(a) presents the plasma discharge image for the ordinary plasma actuator. It can be seen that a single bluish line in the darkness is close to the edge of the exposed electrode.

Compared with the typical one, this work used the testing model made of metal and copper foil tape as a lower electrode and an upper electrode respectively (Fig. 1(b)). Therefore, there are two bright lines on both sides of the exposed electrode for symmetrical actuator (Fig. 2(b)). These discharge photographs are consistent with DBD theory as mentioned above that the glow usually occurs at the edge of exposed electrode and spreads to the projected area of covered electrode. Since the lower electrode covers the whole upper electrode, the symmetrical actuator could produce the double bluish lines. The induced velocity field of the plasma actuator at the test arrangement will be discussed in more details later in this paper.

#### 3. Plasma actuator characterization

#### 3.1. Experimental setup 113

#### (1) Wind tunnel

The experiments were carried out in an open-circuit low 117 tunnel speed wind with а test section 118  $1.05 \text{ m} \times 0.75 \text{ m} \times 0.75 \text{ m}$  at China Aerodynamics Research 119 and Development Center (CARDC), which is capable of gen-120 erating a maximum wind speed of 55 m/s with the turbulence 121 Download English Version:

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