



Performance evaluation of an open-cathode PEM fuel cell stack under ambient conditions: Case study of United Arab Emirates



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ABSTRACT

The open-cathode polymer electrolyte membrane (PEM) fuel cell stack has been a promising candidate as a sustainable energy conversion system for replacing fossil fuel-based energy conversion devices in portable and automotive applications. As the ambient air is directly used to provide both oxidant and cooling, the complex cooling loop can be avoided which reduces the complexity and cost. However, the stack performance is highly affected by ambient conditions, i.e., ambient temperature and humidity. In this study, the effect of monthly ambient air conditions (temperature and humidity) is evaluated with respect to the stack's power production performance as well as thermal, water and gas management by employing a validated three-dimensional open-cathode PEM fuel cell stack model. The annual climate data from the hot and arid environment of Abu Dhabi, United Arab Emirates (UAE) are used as a case study. The objective is to develop a better fundamental understanding of the interactions of physical phenomena in a fuel cell stack, which can assist in improving the performance and operation of an open-cathode PEM fuel cell-powered vehicle. The results indicate that the stack performance can vary significantly (up to 40%) from winter to summer, especially at high operating currents, with significant changes in the stack temperature and the water content at the membrane. Moreover, the anode humidification results in a significant improvement in the stack performance (up to 40%) in hot and dry conditions. However, a careful balance has to be struck between the humidifier parasitic load and the stack power.

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1. Introduction

Due to escalation of the economics, infrastructure development and population growth supported by abundant oil and gas resources, the United Arab Emirates (UAE) is considered to have one of the highest energy consumptions per capita in the world [1]. UAE's emission per capita has also been reported to be very high in comparison to that of many developed countries. The average emission for the UAE in the past 23 year period is about 10.5 tones carbon equivalent (TCE) per capita as compared to only about 1.1 TCE per capita for the world's annual average emission [2]. A major contribution to the UAE's emissions comes from the transportation sector since the demand for personal vehicles has been increasing rapidly (annual growth rate of 6%) since past 15 years [3].

In tandem, the UAE government plans to diversify its fossil fuel-based energy portfolio by adding cleaner new and renewable energy sources. The establishment of Masdar City in 2009 – the world's pioneer carbon neutral city – is a major realization and implementation of the government's efforts for cleaner alternatives. Kazim [1] proposed a strategy for the UAE sustainable development through a hydrogen energy program where, fuel cell vehicles, especially the proton exchange membrane (PEM) fuel cell vehicles, were introduced in the UAE transportation sector.

PEM fuel cell vehicles are gaining significant interest all over the world because of the general awareness of reducing air pollution and carbon dioxide (greenhouse gas) emissions as well as the need of reducing dependence on fossil fuels. Much progress has been made in the research and development of fuel cell technology in the last decade. Several leading automotive companies have also successfully demonstrated their fuel cell vehicles, such as Honda FCX Clarity and Mercedes-Benz F-cell [4]. In the UAE, the BMW group optimistically projected a scenario that up to 30% of fuel cell vehicles would be used in the country by 2020–2030 [3].

Despite the promising achievements and plausible prospects for fuel cell vehicles, there are several major challenges that need to be

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Nomenclature

a	water activity	<i>Greek</i>	
$c_i^{(g)}$	molar concentration of species i , mol m ⁻³	α	transfer coefficient
$c_{i,ref}^{(g)}$	reference molar concentration of species i , mol m ⁻³	$\beta^{(m)}$	membrane modification coefficient
$c_p^{(g)}$	specific heat capacity of gas mixture, J kg ⁻¹ K ⁻¹	ε	porosity
$c_{p,i}^{(g)}$	specific heat capacity of species i , J kg ⁻¹ K ⁻¹	η	overpotential, V
c_r	condensation/evaporation rate constant, s ⁻¹	θ	wetting angle
c_1, c_2, c_3, c_4	constants for the saturation pressure of water; -, K ⁻¹ , K ⁻² , K ⁻³	κ	permeability, m ²
$C_1, C_2, C_3, C_4, C_5, C_6, C_7, C_8$	polynomial constant for fan model, Pa s ⁶ m ⁻⁶ , Pa s ⁵ m ⁻⁵ , Pa s ⁴ m ⁻⁴ , Pa s ³ m ⁻³ , Pa s ² m ⁻² , Pa s m ⁻¹ , Pa	λ	membrane water content
$D^{(c)}$	capillary diffusion, m ² s ⁻¹	μ	dynamic viscosity, kg m ⁻¹ s ⁻¹
$D_i^{(g)}, D_{i,eff}^{(g)}$	diffusivity and effective diffusivity of species i , m ² s ⁻¹	ξ	stoichiometry
$D_{H_2O}^{(m)}$	diffusivity of water in the membrane, m ² s ⁻¹	ξ_1, ξ_2, ξ_3	correction factors for agglomerate model
$D_{O_2}^{(l)}, D_{O_2}^{(p)}$	diffusion coefficient of oxygen in liquid water and in polymer film, m ² s ⁻¹	ρ	density, kg m ⁻³
e_x, e_y, e_z	coordinate vectors	τ	surface tension, Pa
E_{cell}, E_{stack}	cell and stack voltage, V	σ	total stress tensor, Pa
E_a	activation energy, J mol ⁻¹	σ	conductivity S m ⁻¹
E_{rev}	reversible cell potential, V	ϕ	potential, V
F	Faraday constant, C mol ⁻¹	<i>Superscripts</i>	
h_j	height of layer j , m	(c)	capillary
H_{vap}	heat of vaporization, J kg ⁻¹	(C)	carbon
H	relative humidity, %	(g)	gas phase
i, \mathbf{i}	current density, A m ⁻²	in	inlet
$j_{a,c}^{ref}$	anode and cathode volumetric reference exchange current density, A m ⁻³	(l)	liquid phase
J	volumetric current density, A m ⁻³	(m)	membrane
\mathcal{J}	Leverett function	ox	oxidation
k	thermal conductivity, W m ⁻¹ K ⁻¹	(p)	polymer phase
L	length of channel, m	rd	reduction
\dot{m}_{H_2O}	interphase mass transfer due to condensation/evaporation of water, kg m ⁻³ s ⁻¹	ref	reference
$M^{(g)}$	mean molecular mass of the gas phase, kg mol ⁻¹	(s)	solid
M_i	molecular mass of species i , kg mol ⁻¹	sat	saturation
$M^{(m)}$	equivalent weight of the dry membrane, kg mol ⁻¹	set	setting
n_d	electroosmotic drag coefficient	<i>Subscripts</i>	
$\mathbf{n}_i^{(g)}, \mathbf{n}_{H_2O}^{(m)}$	mass flux of species i and water in the membrane, kg m ⁻² s ⁻¹	α, β	index for species
$p^{(c)}, p^{(g)}$	capillary and gas pressure, Pa	a	anode
P	power W	ave	average
$p_{H_2O}^{sat}$	saturation pressure of water, Pa	c	cathode
R	gas constant, J mol ⁻¹ K ⁻¹	cc	current collector
s	liquid saturation	cl	catalyst layer
S	source term	co	coolant channel
T_0, T_1, T_2	constant, K	cool	coolant
T	temperature, K	eff	effective
\mathbf{u}, u, v, U	velocities, m s ⁻¹	ff	flowfield
V	volume, m ³	fin	fins
$x_i^{(g)}$	molar fraction of species i	gdl	gas diffusion layer
x, y, z	coordinates, m	H ₂	hydrogen
		H ₂ O	water
		i	species i
		j	functional layer j
		m	membrane
		mass	mass
		N ₂	nitrogen
		O ₂	oxygen
		pot	potential
		ref	reference
		sp	separator plate
		temp	temperature

addressed before the fuel cell can be considered as a viable alternative to the established internal combustion engine technology [5]. Hydrogen supply-chain and infrastructures, fuel cell performance, fuel cell durability and cost are amongst the major challenges [6]. In addition, the successful operation of fuel cell vehicles depends on several factors related to technological, economic, political

and environmental aspects. From the technological point of view, the complexity of the fuel cell system can be reduced significantly by introducing an open-cathode fuel cell concept, for which the ambient air is used directly to feed-in oxygen to the cathode as well as to dissipate the heat generated by electrochemical reactions. Thus, cooling loop, compressor, radiator, humidifier

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