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# A hydrogen and oxygen combined cycle with chemical-looping combustion

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#### ABSTRACT

In the current paper, new systems integrating chemical-looping hydrogen (CLH) generation and the hydrogen ( $H_2$ ) and oxygen ( $O_2$ ) combined cycle have been proposed. The new methane-fueled cycle using CLH has been investigated with the aid of the exergy principle (energy utilization diagram methodology). First,  $H_2$  is produced in the CLH, in which FeO and Fe<sub>3</sub>O<sub>4</sub> are used as the looping material. The  $H_2$  and  $O_2$  combined cycle then uses  $H_2$  as fuel. Two types of these combined cycles have been analyzed. Waste heat from the  $H_2$ - $O_2$  combined cycle is utilized in the CLH to produce  $H_2$ . The advantages of CLH and the H2 and  $O_2$  combined cycle have resulted in a breakthrough in performance. The new system can achieve 59.8% net efficiency with CO<sub>2</sub> separation when the turbine inlet temperature is 1300 °C. Meanwhile, the cycle is environmentally superior because of the recovery of CO<sub>2</sub> without an energy penalty.

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## 1. Introduction

At present, we face a potentially serious problem of rapid climate change attributed to anthropogenic emissions of greenhouse gases (e.g.,  $CO_2$ ). One option to control greenhouse gas emission is the use of  $CO_2$  capture technologies from flue gases. In a fossil fuelfired power plant,  $CO_2$  capture can be carried out mainly through three available technologies: pre-combustion, post-combustion, and oxy-fuel combustion. The progress in this field has been addressed by Abu-Khader [1]. The main disadvantages of these techniques are the substantial addition to the power generation costs and the large amount of energy required for the  $CO_2$  separation, which amounts to a relative reduction of 15–20% in the overall efficiency of a power plant [2,3]. A new method of separating  $CO_2$  from flue gases in power plants with a negligible energy penalty is therefore urgently needed.

Chemical-looping combustion (CLC) with inherent separation of  $CO_2$  is a promising technology proposed by Ishida and Jin in 1994 [4,5]. It is the most attractive, energy-efficient method of  $CO_2$  capture from fuel conversion using the combustion process. CLC involves the use of a metal oxide as an oxygen ( $O_2$ ) carrier, which transfers  $O_2$  from the combustion air to the fuel, thereby avoiding direct contact between the fuel and the mixture of fuel and air. In this way,  $CO_2$  and  $H_2O$  are inherently separated from the other components of flue gases, so that no energy is needed for  $CO_2$  separation. This novel  $CO_2$  capture technology simultaneously re-

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http://dx.doi.org/10.1016/j.enconman.2014.03.013 0196-8904/© 2014 Elsevier Ltd. All rights reserved. solves both energy and environmental problems in combustion processes because the conversion of fuel-based chemical energy into thermal energy in traditional combustion not only results in the largest irreversibility in the power system, but also has serious environmental impact. In recent years, several researchers have investigated and contributed to the development of the CLC technology [6,7]. For example, Mattisson and Lyngfelt [8] designed and proposed a 10 kW fluidized-bed boiler using CLC [8]. Korea [9] developed a 50 kW CLC for future industrial application. A project for a novel CO<sub>2</sub> separation system using CLC has been initiated by the Department of Energy of the United States [10]. A recent 1 MWth chemical looping plant is reported by Ströhle et al. [11].

In addition, the use of the chemical-looping process was recently proposed for the production of hydrogen (H<sub>2</sub>). There are two kinds of processes to product hydrogen with CLC, the chemical looping reforming (CLR) and chemical looping hydrogen generation (CLH). The CLR produces hydrogen using the CLC principle [12][13]. The main reactions in CLR are as follows, with nickel used as an example:

 $NiO+CH_4 \rightarrow Ni+2H_2+CO \quad \Delta H=211 \ kJ/mol$ 

 $2NiO+CH_4 \rightarrow 2Ni+2H_2+CO_2 \quad \Delta H = 148 \ kJ/mol$ 

 $CH_4 + Ni \rightarrow C - Ni + 2H_2$   $\Delta H = 191 \text{ kJ/mol}$ 

The first reaction is considered as the primary pathway, whereas the other two reactions are possible reactions. Natural gas is used as fuel in CLR research. To supply enough heat to drive the reforming reaction on the fuel reactor side, part of the natural

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2

## ARTICLE IN PRESS

X. Zhang et al. / Energy Conversion and Management xxx (2014) xxx-xxx

## Nomenclature

CC combined cycle CLC chemical-looping combustion	$\Delta H$ enthalpy change
CLHchemical-looping hydrogen generationHO-CLH $H_2$ and $O_2$ combined cycle with CLHRHO-CLHreheat $H_2$ and $O_2$ combined cycle with CLHTITturbine inlet temperature (°C) $\pi$ pressure ratio $\eta$ thermal efficiency (LHV) $\Delta E$ exergy change	SubscriptsOptoptimal valueOxoxidation reactionRereduction reactionCompcompressorSTsteam turbine

gas is burned directly to support the reaction. Another method to produce hydrogen using CLC is water splitting applied to chemical looping (chemical looping hydrogen generation, CLH) [14]. The CLH process is based on two reactors. The CLH fuel reactor is similar to that used in CLC, but the CLC air reactor in is replaced with a steam reactor, in which steam reacts with the metal to produce hydrogen. In CLH, both sides of the reactions are endothermic. These reactions are as follows:

 $Ni + H_2 O \rightarrow NiO + H_2 \quad \Delta H \ (900\ ^\circ C) = 186\ kJ/mol$ 

 $CH_4 + 4NiO \rightarrow Ni + CO_2 + 2H_2O \quad \Delta H \ (800\ ^\circ C) = 58\ kJ/mol$ 

Approximately 10–20% of natural gas is burned directly to supply the heat for the reactions in SMR and CLH systems. Sung et al. [15] reported that 3.7 L of H<sub>2</sub> per kilogram was generated through the reaction between the fully reduced copper-based oxide and steam. Kang et al. [16] investigated H<sub>2</sub> production using the chemical-looping of methane (CH<sub>4</sub>) in a fluidized-bed reactor using an iron-based O<sub>2</sub> carrier.

The H<sub>2</sub> and O<sub>2</sub> combined cycle was first proposed by Cai and Fang [17]. A fairly high efficiency has been obtained based on the stoichiometric reaction of H<sub>2</sub> and O<sub>2</sub>. The combination of CLH and the H<sub>2</sub> and O<sub>2</sub> combined cycle can capture CO<sub>2</sub> without an energy penalty and with high efficiency.

## 2. Description of the novel systems

Fig. 1 shows the plant scheme for the integration of the mixing  $H_2$  and  $O_2$  combined cycle with CLH (HO-CLH). The plant consists of three main parts, namely, the CLH subsystem, the  $H_2$  and  $O_2$  combined cycle subsystem, and the CO<sub>2</sub> separation subsystem.

### 2.1. CLH subsystem

In the CLH subsystem, two separate reactors, CH<sub>4</sub> with metal oxide (reduction) and the resulting metal with H<sub>2</sub>O (oxidation), are used. In the current study, ferric oxide (Fe<sub>3</sub>O<sub>4</sub>) is used as a solid metal oxide (i.e., looping material) in the chemical-looping hydrogen generation. Oxygen is transferred between the two reactors through an O<sub>2</sub> carrier. CH<sub>4</sub> is first reacted with the solid Fe<sub>3</sub>O<sub>4</sub> [reaction (1)] in a reduction reactor, producing solid ferrous oxide (FeO) and steam. When 95–98% of Fe<sub>3</sub>O<sub>4</sub> is reduced, the equilibrium temperature of reaction (1) is approximately 600–800 °C. To achieve a higher Fe<sub>3</sub>O<sub>4</sub> conversion ratio, the temperature of the reduction reactor, H<sub>2</sub>O is reacted with solid FeO [reaction (2)] in the high temperature produced from the first reactor, yielding Fe<sub>3</sub>O<sub>4</sub> and H<sub>2</sub> through strong exothermic oxidation.

Reduction:

$$CH_4 + 4Fe_3O_4 \rightarrow 12FeO + 2H_2O + CO_2 \quad \Delta H_{Red}^0 = 406 \text{ kJ/mol}$$
 (1)



Fig. 1. Mixing  $H_2$  and  $O_2$  combined cycle with chemical-looping hydrogen (HO-CLH).

Oxidation:

$$H_2O + 3FeO \rightarrow Fe_3O_4 + H_2 \quad \Delta H^0_{Ox} = -60 \text{ kJ/mol}$$

## 2.2. $H_2$ and $O_2$ combined cycle subsystem

 $H_2$  produced by the CLH subsystem then enters the  $H_2$  and  $O_2$  combined cycle subsystem. The reaction per mole of  $H_2$  and a half mole of  $O_2$  produce one mole of  $H_2O$ , with a very large amount of energy released compared to any other conventional type of fuel. The oxygen comes from a low pressure air separate unit (ASU) outlet and is further compressed by a compressor. After the combustion with  $O_2$  from the ASU, steam from the combustor can be used as the working fluid to generate power in the steam turbines. Finally, steam from the steam turbines releases heat in the reduction reaction, which is then used to supply the endothermic reaction.

### 2.3. CO<sub>2</sub> separation

The CO<sub>2</sub> separation subsystem is used to separate CO<sub>2</sub> from the CO<sub>2</sub>/H<sub>2</sub>O mixture. The mixture is cooled using liquid H<sub>2</sub>O from the steam turbine, releasing heat in the reduction reactor. The mixture is then cooled to 70–90 °C in the condenser. At this temperature, H<sub>2</sub>O turns into its liquid form and CO<sub>2</sub> is separated. After heating using the CO<sub>2</sub>/H<sub>2</sub>O mixture, the liquid H<sub>2</sub>O is separated and flowed to the oxidation reactor and combustor.

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