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Review

Analytical flaw assessment

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ABSTRACT

The paper provides a review on analytical flaw assessment methods with the focus on fracture under monotonic loading and fatigue crack propagation. The first topic comprises linear elastic as well as elastic-plastic fracture mechanics approaches. It essentially follows their historical development. Topics which are separately discussed are reference/limit loads, the treatment of secondary stresses, strength mismatch, constraint, unstable crack propagation (monotonic R-curve analyses) and statistical aspects. With respect to fatigue crack propagation the analytical treatment of crack closure and constraint and the determination of the cyclic elastic-plastic crack driving force is discussed. Finally, cyclic R-curve analyses are briefly addressed.

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Nomenclature crack length (crack depth for surface cracks) a plastic zone corrected crack length $a + r_p$ (Section 2.2.2) aeff initial crack depth (for cyclic fracture mechanics analysis; Fig. 51) ai initial crack depth (for monotonic fracture mechanics analysis; Fig. 11) a٥ El Haddad parameter, Eq. (185) a_0 correction term for modified El Haddad's model, Eqs. (189) and (191) a* crack aspect ratio a/c half crack length at surface (semi-elliptical crack) c Ē half length of an equivalent through-thickness crack (design curve) C. n fit parameters of the da/dN- Δ K curve in the Paris regime d length of plastic strip (Dugdale model, Section 2.2.3) coefficient (HRR field solution) d_n da/dN fatigue crack propagation rate Ε modulus of elasticity (Young's modulus) E'= E for plane stress and $E/(1 - v^2)$ for plane strain conditions f crack closure function of the NASGRO equation, Eq. (146) F_{Y} net section yield load (general) F_Y of base plate material (weldments) F_{YB} equivalent strength mis-match corrected F_Y F_{YM} F_Y of weld metal (weldments) F_{YW} plasticity correction function (monotonic loading, reference stress method) $f(L_r)$ $f(\Delta L_r)$ plasticity correction function (cyclic loading) reserve factor (fracture resistance) in the FAD approach, Eq. (137) F^{σ} reserve factor (yield strength) in the FAD approach, Eq. (138) G_{Y} (elastic) energy release rate at the unset of general yield (Eqs. (21)–(28)) influence functions (EPRI scheme, Section 2.2.7) for I and δ h_1, h_2 Η width or half width of the weld strip (strength mismatch consideration) J J-integral (monotonic loading) critical I-integral J_c elastic component of the J-integral Ĭe J_i , $J_{0.2/BL}$ resistance against stable crack initiation (monotonic loading) plastic component of the J-integral $J_{p} \\ J^{s}$ I-integral due to secondary stresses J_{Y} I-integral at the onset of general yield stress intensity factor (K-factor) $K_{\rm eff}$ K^J plastic zone corrected K factor (Section 2.2.2) K factor formally derived from J-integral K_I^S ligament yielding corrected K^J $\dot{K_{mat}}$ fracture resistance, monotonic loading (general) K_{mat}^c constraint-corrected K_{mat} (R6 routine; Eq. (130)) K_{max} maximum K-factor in a loading cycle (fatigue crack propagation) minimum K-factor in a loading cycle K_{min} K_{op} K-factor at crack opening (cyclic loading) K^p K factor due to primary stresses ordinate of the FAD diagram (= K/K_{mat}) K_r Ks K factor due to secondary stresses K-factor for mode-I-crack opening (normal to the crack faces) K_{I} fracture resistance of the material (small scale yielding conditions) K_{Ic} characteristic dimension (EPRI scheme) L L_r ligament yielding parameter for monotonic loading

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