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## Rate dependent behavior of crash-optimized adhesives – Experimental characterization, model development, and simulation



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### ABSTRACT

The mechanical properties of crash-optimized adhesive BETAMATE 1496V are characterized over a wide range of strain rates. The information gathered from the mechanical tests are used for developing a fully rate-dependent constitutive law for cohesive interface elements considering both, the strain rate dependency of the initiation stress and the strain rate dependency of the fracture toughness. The model is calibrated and verified against experimental data for tapered double cantilever beam (TDCB) and tapered end notched flexure (TENF) tests. Finally, the model is validated against quasi-static and dynamic experimental results on an adhesively bonded T-joint. The numerical predictions show good correlation with the experimental results.

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#### 1. Introduction

In recent years, structural adhesives have become more important in the automotive industry due to the possibility of vehicle weight reduction and the associated reduction of fuel consumption and CO<sub>2</sub> emissions. At the same time, the crash worthiness must be maintained and considered in the design process. Consequently, there is a requirement to simulate the mechanical response of structural adhesives subjected to crash loading accurately. A good understanding of the mechanical response of structural adhesives is required in order to develop numerical models with predictive capabilities. A state-of-the-art technique for modeling damage and failure in structures with well-defined fracture planes, such as laminated composites or adhesively bonded structures is the application of cohesive zone models. Cohesive zone models are particularly interesting due to their intrinsic ability to model damage initiation and subsequent propagation in a single, coherent analysis which cannot be achieved with numerical methods requiring the presence of a pre-crack such as the Virtual Crack Extension Technique [1] or the Virtual Crack Closure Technique (VCCT) [2]. In addition to the well-established cohesive interface formulations (see recent review by Wisnom [3]) for describing quasi-static loading, there have recently been efforts for modeling the fatigue (see recent review by Pascoe et al. [4]) and crash response (see for example Marzi et al. [5], Samudrala et al. [6] or May et al. [7]. The promising results presented by Marzi et al. [5] and May et al. [7] indicate the need for taking into

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#### Nomenclature

Latin characters	
C <sub>I</sub>	constant
C <sub>II</sub> D	constant damage
E	Young's modulus
C G <sub>IC</sub>	mode I fracture toughness
G <sub>IC</sub> , ref	quasi-static mode I fracture toughness
$G_{IC,inf}$	upper bound of the mode I fracture toughness
$G_{IIC}$	mode II fracture toughness
G <sub>IIC.ref</sub>	quasi-static mode II fracture toughness
$G_{diss}$	total energy dissipated
KI	stiffness of the adhesive layer
κ <sub>π</sub>	shear stiffness of the adhesive layer
$l_{cz}$	cohesive zone length
$m_I$	constant
$m_{II}$	constant
Μ	constant
Т	specimen thickness
ta	thickness of the adhesive layer
Greek characters	
β	mode-mixity
$\Gamma_{II}$	pseudo-plasticity parameter
$\delta_I$	mode I displacement
$\delta_{II}$	mode II displacement
$\delta_m$	mixed-mode displacement
$\delta_I^0$	displacement at initiation, pure mode I
$\delta^f_I$	displacement at failure, pure mode I
$\delta_{II}^0$	displacement at initiation, pure mode II
$\delta^{f}_{II}$	displacement at failure, pure mode II
$\delta_{II}^{pl}$	displacement at the end of the plastic plateau, pure mode II
$\delta_m^0$	mixed-mode displacement at initiation
$\delta_m^f$	mixed-mode displacement at final failure
$\delta_m^{pl}$	mixed-mode displacement at the end of the plastic plateau
ė ė	strain rate
Ė <sub>I</sub>	strain rate in peel-direction
E <sub>II</sub>	shear rate
$\mathcal{E}_{I,ref}$	reference strain rate in peel-direction defining quasi-static loading reference shear rate defining quasi-static loading
E <sub>II,ref</sub>	constant
$\eta$	Poissons' ratio
$\sigma_I$	mode I stress
$\sigma_{II}$	mode II stress
$\sigma_I^0$	stress at initiation, pure mode I
$\sigma_{\mu}^{0}$	stress at initiation, pure mode II
$\sigma^{\mu}_{Irof}$	mode I initiation stress at quasi-static loading
$\sigma^{I}_{II,ref}$	mode II initiation stress at quasi-static loading

account potentially rate dependent properties. Previous experimental work on structural adhesives has shown that both, the strength [8–11] and the fracture toughness [5,11–13] are sensitive to high strain rate loading. In the first part of this paper an extensive experimental programme for characterization of rate dependent material properties of the crash-optimized structural adhesive BETAMATE 1496V is presented. Using the information obtained from the experimental work (rate dependent properties, shape of the cohesive law), a cohesive zone model is developed and implemented into the commercial FE package ABAQUS/Explicit. The model is an extension to the formulation previously presented by May et al. [7]. In the original formulation given in [7], rate dependent material properties such as the initiation stress and fracture toughness are assumed to be constant once damage initiation has occurred. However, in real life, the strain rate is usually not constant. This paper

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