



Dynamic interaction of heat transfer, air flow and disc vibration of disc drives – Theoretical development and numerical analysis



Yong-Chen Pei^a, Huajiang Ouyang^{b,*}, Cong-Hui Wang^a

^a School of Mechanical Science and Engineering, Jilin University, Nanling Campus, Changchun 130025, People's Republic of China

^b School of Engineering, University of Liverpool, Liverpool L69 3GH, UK

ARTICLE INFO

Article history:

Received 24 April 2014

Received in revised form

19 August 2014

Accepted 14 September 2014

Available online 19 September 2014

Keywords:

Rotating flexible disc

Multi-physical interaction

Air flow

Convective heat transfer

Thermoelastic dynamics

Disc drive

ABSTRACT

Steady state air flow, heat transfer and thermoelastic dynamics in the multi-field coupling system of a rotating flexible disc in an enclosure filled with air are investigated within a large speed range. The system represents rotating discs in hard disc drives and optical disc drives. With Navier–Stokes and continuity equations and an improved penalty finite element method, air velocities and pressure induced by disc rotation in the enclosure are obtained. Temperature distribution of the rotating disc, driving shaft, enclosure and air flow is determined under the external heat sources from the shaft-driving motor and the circuit board inside the enclosure, the internal heat source from aerodynamic heating due to viscous dissipation of fluid, the heat convection in air flow, and the free convection heat loss at the enclosure's outside surfaces. Natural frequencies of the rotating disc are solved under the stresses induced by the disc temperature distribution and centrifugal force. Effects of heat convection and aerodynamic heating induced by disc rotation on system heat balance and dynamic characteristics of the rotating disc are investigated. The method presented is helpful to design of hard/optical disc drives and many other applications that involve rotating discs in fluids and with heat transfer.

© 2014 Elsevier Ltd. All rights reserved.

1. Introduction

Discs are a widely used component in engineering, and they can rotate at high speed in the surrounding environment with fluid and heat transfer. The fluid flow and heat transfer induced by disc rotation and their influences on the dynamics of rotating discs are the fundamental and crucial issues concerning the performance of rotating discs, and they are subjects of great interest in academic research and industrial design [1]. Examples include turbo machineries, computer hard disc drives and optical disc drives. They can operate in harsh environments and involve multi-physical processes.

Firstly, considerable vibration and even flutter instability of a rotating disc can be caused by the fluid flow induced by disc rotation at supercritical speeds. In view of acoustic and structural interactions, Jana and Raman [2] and Kang and Raman [3,4] took the air flow to be initially quiescent, irrotational and infinitesimal, and they solved the wave equation governing the propagation of infinitesimal disturbances of air flow to analyse the vibration and stability of a rotating flexible disc. They found that coalescence between the

acoustic and structural modes could lead to flutter instability at supercritical speeds. Some researchers [5–9] treated the coupling dynamics of the fluid flow and rotating disc as fluid and structure interaction problems. With the Reynolds equation of lubrication for thin film flows, Naganathan et al. [5] and Bajaj et al. [6] studied flutter instability and the forced harmonic response of a flexible disc rotating near a rigid wall in the presence of air, and found that the rotating disc could undergo flutter instability when the speed of rotation was above a critical speed, as discovered by a number of researchers in the recent past. Using Navier–Stokes and continuity equations, Gad and Rhim [7] investigated dynamics of a flexible disc coupled to thin air film and rotating close to a rigid rotating wall, and it was shown that the stability of the rotating flexible disc could be improved by a counter-rotating flat stabiliser. With the Navier–Stokes equations for an incompressible air flow of constant viscosity, Yuan et al. [8] studied the self-excited vibration induced by fluid forces of a rotating, umbrella-shaped disc in an open shroud, and Cheng et al. [9] designed several enclosure covers of an optical disc drive to improve the flow-induced vibration of rotating discs.

Secondly, heat transfer in the surrounding environment of rotating discs is affected considerably by the fluid flow induced by disc rotation in many applications [1]. Inamuro et al. [10] investigated the axisymmetric incompressible flow and heat transfer in a rotating cylindrical container with a counter-rotating disc, and discussed effects of disc rotation and of Prandtl numbers on them.

* Corresponding author. Tel.: +44 151 794 4815.

E-mail addresses: yongchen_pei@hotmail.com (Y.-C. Pei), H.Ouyang@liverpool.ac.uk (H. Ouyang).

Nomenclature

a	disc's outer radius	$w_{m,n}$	modal coordinate of disc's transverse deflection corresponding to disc mode (m, n)
b	disc's inner radius	z	transverse coordinate
c_a	specific heat of air	z_0	transversal coordinate at centre of a ring element
e	the e -th ring element	α_T	coefficient of linear thermal expansion
e_{\max}	maximum element length	$\gamma_{m,0}$	self-adjoint eigenvalue
e_{\min}	minimum element length	Γ	temperature increment
E	Young's modulus	$\bar{\Gamma}$	averaged temperature increment
g_r	the second r -component of thermal membrane stress in the r direction	Γ_{Air}	temperature increment due to internal heat generation
g_θ	the second r -component of thermal membrane stress in the θ direction	$\bar{\Gamma}_{\text{Air}}$	averaged temperature increment due to internal heat generation
h	disc's thickness	Γ_{Base}	mean temperature increment due to internal heat generation
h_a	convective heat transfer coefficient of air	$\bar{\Gamma}_{\text{Base}}$	averaged temperature increment due to external heat generations
J_m	thermal membrane stress resultant	ε	penalty parameter
k_a	thermal conductivity of air	η_r	dimensionless radial coordinate
k_r	the first r -component of thermal membrane stress in the r direction	η_z	dimensionless transversal coordinate
k_s	thermal conductivity of shaft, disc and enclosure	θ	circumferential coordinate
k_θ	the first r -component of thermal membrane stress in the θ direction	Θ_M	mean temperature increment
l_r^m	the third r -component of thermal membrane stress in the r direction	Θ_M^{Air}	mean temperature increment due to internal heat generation
l_θ^m	the third r -component of thermal membrane stress in the θ direction	Θ_M^{Base}	mean temperature increment due to external heat generation
L_b	enclosure's base thickness	Θ_Q	'moment' of the temperature increment
L_g	enclosure's gap width	λ	eigenvalue
L_r	element size in the r direction	μ_a	coefficient of air viscosity
L_t	enclosure's cover thickness	ν	Poisson's ratio
L_w	enclosure's wall thickness	ξ_r	radial thermal membrane stress resultant
L_z	element size in the z direction	ξ_θ	circumferential thermal membrane stress resultant
L_1	enclosure's upper cavity height	ρ	disc's density
L_2	enclosure's lower cavity height	ρ_a	air density
m	number of nodal circles of a disc mode	σ_r	radial membrane stress resultant due to centrifugal force
n	number of nodal diameters of a disc mode	σ_θ	circumferential membrane stress resultant due to centrifugal force
p	relative air pressure	$\varphi_{m,n}$	mode shape of disc mode (m, n)
\bar{p}	averaged relative air pressure	Φ	potential function of viscous dissipation
P	steady state pressure difference across disc thickness	Ψ	thermal stress function
P_A	total heat generation power of aerodynamic heating	Ψ_H	homogenous part of thermal stress function
P_B	heat generation power of enclosure base	Ψ_N	non-homogenous part of thermal stress function
P_S	heat generation power of shaft base	$\omega_{m,n}$	natural frequency of disc mode (m, n)
q	aerodynamic heating flux	Ω	disc's rotating speed
\bar{q}	averaged aerodynamic heating flux	Ω_{cr}	lowest disc's critical speed
q_B	heat flux to the enclosure's base	Ω_M	maximum disc speed
q_S	heat flux to the driving shaft	$I_n(r)$	modified Bessel function of the first kind
r	radial coordinate	$J_n(r)$	Bessel function of the first kind
r_0	radial coordinate at centre of a ring element	$K_n(r)$	modified Bessel function of the second kind
R	enclosure's inside radius	$Y_a(r)$	Bessel function of the second kind
Re	Reynolds number	Superscript $^{-1}$	matrix inverse
t	time	Superscript T	matrix transpose
T	temperature	Superscript $'$	derivative with respect to radial coordinate r , i.e. d/dr
T_a	atmospheric temperature	Superscript \sim	conversion matrix or vector at heat flux boundaries
u_r	radial air velocity component	Superscript $^{\wedge}$	$(I_P$ or J_P rows, I_P or J_P columns) elements in a matrix; $(I_P$ or J_P rows) elements in a vector
u_z	transversal air velocity component	Superscript $^-$	$(I_P$ or J_P rows, i_B or j_B columns) elements in a matrix; $(i_B$ or j_B rows) elements in a vector
u_θ	circumferential air velocity component	Constant	normal upright 'A'
\bar{u}_r	averaged radial air velocity component	Matrix	bold upright 'A'
\bar{u}_z	averaged transversal air velocity component	Variable	normal italic 'A'
\bar{u}_θ	averaged circumferential air velocity component	Vector	bold italic 'A'
V_a	solution domain of air media		
V_s	solution domain of solid media		
w	disc's transverse deflection		

Download English Version:

<https://daneshyari.com/en/article/7174339>

Download Persian Version:

<https://daneshyari.com/article/7174339>

[Daneshyari.com](https://daneshyari.com)