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# The identification of coherent structures using proper orthogonal decomposition and dynamic mode decomposition

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## ABSTRACT

A comprehensive comparison was conducted on the identification of coherent structures in fluid flow using Proper Orthogonal Decomposition (POD) and Dynamic Mode Decomposition (DMD). The influences that multi-dominant structures and high-order harmonics had on the decomposed modes were taken into extensive consideration. To this end, a series of fabricated patterns was constructed for the benchmark testing to simulate multi-dominant convective structures superimposed in a stationary field. The comparison showed that the temporal DMD method could clearly separate each structure in the spatial and spectral senses, while the POD mode corresponding to the desired structure is contaminated by the other uncorrelated structures. Subsequently, two case studies of the real wake flows, which were determined from high-repetition TR-PIV measurements, were employed to demonstrate the discrepancies of the POD and DMD algorithms in extracting coherent structures. For the wake flow behind a single cylinder at  $Re_D = 8000$ , the temporal DMD algorithm accurately determined the frequency, wavelength and convection speed of the Karman-like vortex street and its higher-order harmonics. However, although the first two POD modes are closely related to the Karman-like vortex street, the higher POD modes embedded as larger structures are obscure in the physical significance. Finally, the wake flow behind two side-by-side cylinders of different diameters at  $Re_D = 1000$  based on the diameter of the small cylinder was measured; two configurations with different gaps were chosen for comparison, i.e.,  $G/D = 0.5$  and  $2.0$ . For the wake flow at  $G/D = 0.5$ , the POD and DMD algorithms determined the major features of the single-dominant structure. For the wake flow at  $G/D = 2.0$ , the first and second temporal DMD modes effectively and independently extracted the Karman-like vortex structures behind the large and small cylinders, respectively. Meanwhile, although the first and second pairs of POD modes generally captured these two convecting structures, respectively, there was obvious existence of the undesirable contamination of the POD mode, as reflected in the interaction between the desired and uncorrelated structures.

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## 1. Introduction

Fluid flows such as wakes, jets, and separated flows are largely characterized by coherent structures with different spatial and temporal scales and the common existence of multi-dominant structures in fluid flows makes identifying the spatio-temporal

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Nomenclature		$\bar{u}$	time-mean velocity [m s <sup>-1</sup> ]
$A$	matrix comprised of mode coefficients $a_i(t)$	$u'$	fluctuation velocity [m s <sup>-1</sup> ]
$B$	system matrix	$v_j$	Koopman mode
$C$	companion matrix	<i>Greek symbols</i>	
$\hat{C}$	full companion matrix	$\alpha_n(t)$	growth rate factor
$D$	diameter of small cylinder [m]	$\beta_n$	wavelength factor
$G$	gap between two cylinders [m]	$\gamma_n$	velocity factor
$G_{aa}$	power spectra of coefficient $a(t)$	$\delta$	thickness of turbulent boundary layer
$M$	finite number of POD modes	$\Lambda$	diagonal matrix with eigenvalues
$R$	temporal correlation matrix	$\lambda_x$	characteristic wavelength along the stream-wise direction
$Re_D$	Reynolds number based on diameter of small cylinder	$\lambda_i$	eigenvalues of Koopman operator
$S$	infinite Vandermonde matrix	$\mu$	eigenvalues mapping onto the complex plane
$\tilde{S}$	finite Vandermonde matrix	$\rho$	density of the glass beads [kg m <sup>-3</sup> ]
$K$	Koopman operator	$\sigma$	growth rate of DMD modes
$U$	discrete velocity matrix	$\sigma_k(x)$	spatial eigenfunctions
$U_0$	free stream velocity [m/s]	$\Phi$	dynamic modes
$a_i(t)$	mode coefficients of POD	$\ \Phi\ $	energy norm of dynamic mode
$a_n$	constant	$\varphi_i$	Koopman eigenfunctions
$b_n$	constant	$\omega$	phase velocity of DMD modes
$c_i$	$C = (C_1, \dots, C_{N-1}, C_N)$	<i>Abbreviations</i>	
$d$	diameter of glass beads [m]	DMD	Dynamic Mode Decomposition
$d_n$	size factor of fabricated structure	DNS	Direct Numerical Simulation
$e$	$e = (0, \dots, 0, 1)^T$	LES	Large Eddy Simulation
$f$	frequency [Hz]	PIV	Particle Image Velocimetry
$f()$	a map comparing a manifold to itself	POD	Proper Orthogonal Decomposition
$g$	vector-valued observable	RAID	Redundant Arrays of Inexpensive Disks
$q$	fabricated pattern	SSD	Solid State Disk
$q_n$	component of the fabricated pattern	TR-PIV	Time-resolved Particle Image Velocimetry
$r$	residual vector	WAG	Window Average Gradient
$T$	period of the shedding structures		
$\Delta x$	distance between two adjacent points along the streamwise direction		
$u$	instantaneous velocity [m s <sup>-1</sup> ]		

features of each coherent structure challenging. Such identification, however, plays a significant role in study of various physical processes, e.g., heat and mass transfer, and flow noise. Recent decades have seen rapid developments in remarkable applications of Large Eddy Simulation (LES) and Direct Numerical Simulation (DNS), along with the state-of-the-art Time-resolved Particle Image Velocimetry (TR-PIV) – all of which have enabled the accurate capture of instantaneously varying flows at reasonable spatial and temporal resolutions. It is highly desirable to extract the salient coherent structures from a large quantity of numerical and experimental information.

In the last two decades, many techniques have been proposed to identify the coherent structures, e.g., vorticity concentration, critical points, Window Average Gradient (WAG) detection and Q-criterion. By plotting vorticity contour maps, Hussain and Hayakawa (1987) characterized large-scale organized structures in the turbulent plane wake of a circular cylinder; the spatially phase-correlated vorticity was employed to examine the dynamics of coherent structures in turbulent shear flow (Hayakawa and Hussain, 1989) and cylinder wake (Zhou and Antonia, 1993). Using the Q-criterion, the kinematical and dynamical properties of the flow, for example kinetic energy, Reynolds stress, were made clear by describing the flows in terms of individual events or streamline patterns (Hunt et al., 1988). Bisset et al. (1990) detected the organized motion in a cylinder wake by calculating the WAG value. Zhou and Antonia (1994) applied the critical point method in analysis of a turbulent near wake, demonstrating that the spanwise vortices provide the dominant contribution to the Reynolds shear stress. The above-mentioned methods have been extensively employed in fluid-mechanics community to determine characteristics of the vortices buried in turbulent flows. However, such methods would obscure the underlying complexity of fluid flow superimposed with multi-dominant coherent structures. Among all of the data-driven algorithms that have been used to determine the spatio-temporal features of multi-scale coherent structures, Proper Orthogonal Decomposition (POD) and Dynamic Mode Decomposition (DMD) have enjoyed widespread use. A comprehensive understanding of the roles of POD and DMD algorithms in the identification of multi-dominant coherent structures in spatial and spectral domains is of essential significance.

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