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Investigation into use of piezoelectric sensors in a wheeled robot tire for surface characterization

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Abstract

A differential steered, 13.6 kg robot was developed as an intelligent tire testing system and was used to investigate the potential of using piezoelectric film sensors in small tube-type pneumatic tires to characterize tire-ground interaction.

The robot was instrumented with low-cost piezoelectric film sensors between the inner tube and the tire. An unlaminated and a laminated sensor were placed circumferentially along the tread and an unlaminated sensor was placed along the sidewall. The analog signal passed to the robot via a slip ring. The robot was tested with a controlled power sequence carried out on polished cement, ice, and sand at three power levels, two payload levels, and with two tire sizes.

The results suggest that the sensors were capable of detecting normal pressure, deflection, and/or longitudinal strain. Added payload increased signal amplitude for all sensors. On the smaller tires, sensors generally recorded a smaller, wider signal on sand compared to cement, indicating potential to detect contact patch pressure and length. The signals recorded by the unlaminated sensor along the tread of the smaller tire were smaller on ice than cement, indicating possible sensitivity to tractive force. Results were less consistent for the larger tires, possibly due to the large tread pattern.

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Keywords: Intelligent tire; Wheeled robot; Terramechanics; Piezoelectricity; Full width at half maximum

1. Introduction

In the past two decades, a focus of tire research has been on implementing sensors into tires to gather information about the tires, the vehicle, or the operating environment (APOLLO, 2005; Ergen et al., 2009). Tires with embedded sensors are known as 'smart' or 'intelligent' tires.

While a large amount of research has been done on development of 'smart' tires for passenger vehicles, less work has been conducted on instrumentation of small tires, like those that are used in small wheeled robots. Instrumenting tires of small wheeled robots with sensors to detect the forces or moments acting on a tire has potential to both improve robot mobility and enable a robot to sense its external environment. Sensors in a small robotic tire could be used to detect terrain type (e.g. terrain roughness, soil properties), geometry of terrain and any obstacles, contact patch pressure (Roth, 2010), or tire sinkage. This type of information gathered by 'smart' robot tires could be used to:

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- Improve traction, handling, and steering (Cheli et al., 2010; Iagnemma et al., 2004).
- Improve vehicle durability (Pinto, 2012).

Nomenclature F_z force in the z direction, vertical load [N] measured weight of the right side of the robot W_{right} F_y F_x force in the y direction, lateral force [N] force in the x direction, longitudinal or tractive W_{right}^* adjusted weight of the right side of the robot force [N] [kg] slip W_{total} measured total weight of the robot [kg] S linear velocity of vehicle $\left[\frac{m}{s}\right]$ W_{FL} calculated front left weight of the robot [kg] vcalculated front right weight of the robot [kg] W_{FR} angular velocity of tire $\left[\frac{\text{rad}}{\text{s}}\right]$ ω W_{RL} calculated rear left weight of the robot [kg] effective rolling radius of tire [m] r_{eff} calculated rear right weight of the robot [kg] W_{RR} coefficient of friction μ maximum allowable current for a motor I_{max} static coefficient of friction μ_{static} channel [A] sliding coefficient of friction $\mu_{sliding}$ current from one motor channel, measured by I_{mot} peak coefficient of friction μ_p CImotor controller [A] cone index [kPa] V_{batt} battery voltage [V] PPRpulses per revolution applied relative power level for a motor channel GRR gear reduction ratio $[\%P_{max} \times 10]$ PVDFpolyvinylidene fluoride measured relative power level for a motor chan- P_{rel} Vvoltage [V] nel [% $P_{max} \times 10$] V_0 initial voltage [V] measured power level for a motor channel [A] P_{mot} V_p voltage measured across a piezoelectric sensor maximum theoretical power level for a motor P_{max} [V] channel [A] charge [C] relative motor speed, measured by the motor ω_{rel} Ccapacitance [F] controller [$\%\omega_{max} \times 10$] Ι current [A] maximum specified motor speed [RPM] ω_{max} Y Young's modulus set of time values recorded corresponding to t_{mot} length of piezoelectric sensor electrode [m] l_p motor measurements [ms] width of piezoelectric sensor electrode [m] w_p set of evenly spaced time values recorded corre t_{dag} thickness of piezoelectric material between elec t_p sponding to the DAQ measurements [s] trodes [m] angle [rad] thickness of piezoelectric sensor, measured out t_s θ_{12} angle by which sensor 2 leads sensor 1 [rad] side of protective film and/or laminate [m] angle by which sensor 3 leads sensor 1 [rad] θ_{13} width of piezoelectric sensor protective film [m] W_f AVDLAdvanced Vehicle Dynamics Laboratory, length of piezoelectric sensor protective film [m] l_f Virginia Tech Z_C electrical impedance of a capacitor $[\Omega]$ Center for Vehicle Systems and Safety, Virginia **CVeSS** Z_R electrical impedance of a resistor $[\Omega]$ Tech time constant of a circuit [s] CMSComputational Multi-Physics Systems k_B Boltzmann's constant Laboratory, Virginia Tech Tabsolute temperature [K] Full Width at Half Maximum *FWHM* C_p capacitance of a piezoelectric sensor [F] gain $\left[\frac{V}{V}\right]$ or $\left[\frac{V}{C}\right]$ Afrequency [f] applied stress, 6×1 vector $\left[\frac{N}{m^2}\right]$ Z σ_m electrical impedance $[\Omega]$ D_i dielectric displacement, 3×1 vector $\left[\frac{C}{m^2}\right]$ R resistance $[\Omega]$ time constant [s] R_p resistance of a piezoelectric sensor $[\Omega]$ dielectric permittivity, 3×3 matrix $\left| \frac{F}{m} \right|$ e_{ij} W_{front} measured weight of the front of the robot [kg] piezoelectric strain constant, 3×6 matrix d_{ii} W_{front}^* adjusted weight of the front of the robot [kg] W_{rear} measured weight of the rear of the robot [kg] pyroelectric coefficient $\left[\frac{C}{m^2}K\right]$ p W^*_{rear} adjusted weight of the rear of the robot [kg] dielectric constant where $\epsilon_0 = 8.85 \frac{\text{pF}}{\text{m}}$ W_{left} measured weight of the left side of the robot [kg] W^*_{left} adjusted weight of the left side of the robot [kg]

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