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Research paper

Comparison of experimental and operational modal analysis on a back to back planetary gear

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ABSTRACT

Several modal analyse techniques are widely used to study the dynamic characteristics of a structure by identifying the modal parameters. This paper presents a comparison between an Experimental Modal Analysis (EMA) test, an Operational Modal Analysis (OMA) test and an Order Based Modal Analysis (OBMA) applied on a recirculating energy planetary gear. The OMA and OBMA offer a test of the planetary gear under its real boundary conditions, whereas the EMA is based on the frequency response function estimation. Using these different techniques, the back to back planetary gears modal parameters were identified. In a first step, the experimental results determined by EMA and OMA were correlated to the numerical results model obtained by a three-dimensional lumped parameter model. In a second step, the OBMA estimated modal parameters were compared to those of the EMA.

According to the obtained results, OMA cannot excite all the modes. However, it was noticed that there is no significant difference between the modal parameters obtained by the EMA and the OBMA. The natural frequencies and damping ratios were deviating by 11% and 2.43%, respectively.

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1. Introduction

Nowadays, planetary gear transmissions are widely used in different mechanical applications such as cars, wind turbine and a lot of rotating machinery. These systems are characterized by complex kinematic and dynamic compositions. The diagnosis of these systems could be a very important task for research. Many developments were achieved to characterize these systems. The modal properties determination is one of the main investigated issues.

The different available modal analysis kinds are the Experimental Modal Analysis (EMA), Operational Modal Analysis (OMA) and Order Based Modal Analysis (OBMA). EMA techniques are based on impact test, and an excited mechanical structure by means of a hammer or shaker. The frequency response functions are determined, and modes as well as modal damping are estimated. The EMA has three critical drawbacks: firstly, the impact test needs to be repeated to accurately

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A. Mbarek et al./Mechanism and Machine Theory 000 (2018) 1-22

Nomenclature

r	Ring	
c	Carrier	
S	Sun	
P1	Planet 1	
P2	Planet 2	
P3	Planet 3	
Krn	The ring-planet mesh stiffness	
Ken	The sun-planet mesh stiffness	
k _e	The carrier's shaft flexural stiffness	
k _{ef}	The sun 's shaft flexural stiffness	
kct	The carrier's shaft torsional stiffness	
ket	The sun 's shaft torsional stiffness	
kca	The carrier 's shaft axial stiffness	
ken	The sun 's shaft axial stiffness	
Wi	Natural pulsations	
φ_{i}	Vibrations modes	
q	Degree of freedom vector	
Ń	Global mass matrix	
K _b	Bearing stiffness matrix	
$K_{e}(t)$	Time varying mesh stiffness matrix	
Kc	Coupled matrix	
С	Damping matrix	
F(t)	External force	
$\psi_{\rm r}$	Ring-planet pressure angle	
ψ_{s}	Sun-planet pressure angle	
α_{i}	Planet i angular position	
α_{s}	The sun pressure angle	
$\alpha_{\rm r}$	The ring pressure angle	
R _{br}	The rings base radius	
R _{bs}	The suns base radius	
R _{bp}	The planets base radius	
m _{ij}	Masses of component i of gear j	
I _{ij}	Inertia of component i of gear j	
k _{ijk}	Bearing stiffness of component i of gear j in k direction	
fs	Sampling frequency	
Subscript	2	
i=rcsn	~ 1 p2 p3 Denotes respectively ring, carrier, sun, planet1 planet2 planet3	
$i = r_i t$	Denotes respectively ring, current, sun, planets, planets, planets	
k = u.v.w	$t \oplus \Psi$. θ Denotes axis direction	
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understand the dynamic behaviour. Secondly, in many engineering applications, and under real operating conditions the obtained results may differ significantly from those achieved in lab testing with an artificial excitation. Thirdly, the use of shaker can be an additional load for structures and may lead to erroneous results.

Many researchers implemented this technique to study the dynamic properties of planetary gears. Hammami et al. [1] studied a modal analysis of back to back planetary gear. They validated their experimental results using those issued from the lumped parameters model. Ericson and Parker [2] applied an experimental modal analysis to characterize the dynamic behaviour of two spur planetary gears. They validated the experimental results by those obtained from both of the finite elements model and lumped parameter model.

Kahraman [3] proposed a simplified rotational lumped-parameter model, providing closed-form expressions for the torsional natural frequencies in terms of system parameters. Zhang et al. [4], however, established a translational-rotational coupled dynamic model of a two-stage planetary gear set to anticipate natural frequencies and vibration modes.

Lin and Parker [5] used a two-dimensional planetary gear model with equal planet spacing to explain the unique modal properties. The compound planetary gears vibration modes were studied by Kiracofe and Parker [6] and Guo and Parker [7].

The second technique is the OMA also known as an output-only modal analysis. It is based on the determination of the modal proprieties under operational tests. It is widely used for the rotating machinery to characterize their modal proprieties. Chauhan et al. [8] studied the dynamic characterization of a wind turbine gearbox. They identified its modes shapes through the finite element model and correlated the numerical modes shapes with those obtained experimentally.

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