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and loads considering misalignment, torque, and friction influences

Theoretical and experimental study on gear-coupling contact

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ABSTRACT

A new analytic model addresses the tooth contact and induced loads of gear couplings that are affected by misalignment, torque, and friction. The contact model accounts for Hertzian, bending, and shear deformations of coupling teeth considering crown modifications. For a specified torque and shaft misalignment, the model calculates the number of teeth in contact, tooth load, stiffness, stress, deformation, and safety factors. The tooth load distribution around the circumference compares well with high fidelity finite-element/contact-mechanics analyses. Simulation time with the analytic model is orders of magnitude less. Using the local contact characteristics, the model computes coupling loads that are primarily caused by the disrupted tooth contact and sliding friction caused by axial motions. This analytic model was validated by experiments. The load amplitude depends on the misalignment, torque, and friction. At low torque, coupling motion was induced by the eccentricity between the hub and sleeve even with nearly perfect alignment. This eccentricity was caused by its self-weight. When torque was larger than a threshold, the motion amplitude was greatly reduced. This torque threshold was analytically derived and validated by experiments.

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1. Introduction

Gear couplings are a common machine component used extensively in a wide range of applications including aerospace, manufacturing, automotive, and wind power. Aside from transmitting the driving torque, crowned-tooth gear couplings accommodate some axial motion and angular misalignment between the two connecting shafts. An important aspect of gear couplings is the existence of forces and moments that are transmitted to the driveline when misaligned. Amplitudes of these loads have been reported to be between 12% and 16% of the drive torque for crowned- and straight-tooth couplings [1]. These forces can increase other component loads in the driveline and could lead to high vibration.

The National Wind Technology Center (NWTC) at the National Renewable Energy Laboratory (NREL) operates two multimegawatt wind-energy-specific dynamometers. These dynamometers offer a unique opportunity to perform measurements of coupling performance. Gear couplings used in the NWTC's 5-MW dynamometer testing facility are key components that accommodate angular misalignment and transmit torque from the dynamometer gearbox to the device under test during operation. Coupling-induced loads are ultimately reacted by both the device under test and the dynamometer gearbox, contributing to the

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Nomenclature	
A	Arc of year tooth contact
h	Backlash
C C	Single pair tooth stiffness
Ē	Young's modulus
F	Facewidth
f_c	Half tooth facewidth in contact
f_d	Distance from the tooth center to the contact point
F _c	Contact length of a single tooth
F _d	Distance between tooth center and contact point for a tooth
F _i	Maximum distance between tooth center and contact point
i _d	Design misalignment angle
L _s	Coupling shaft length
M^{y} , M^{z}	I otal bending moments of a coupling around y' and z' axis
M_d^{ν} , M_d^{z}	Single tooth bending moments around y and z axis
M_{S}^{y}, M_{S}^{z}	I otal bending moments of a coupling around y' and z' axis at sensors
M_t^{γ} , M_t^{z}	lotal bending moments of a coupling around y and z axis
IN N	Number of teeth
N _{c,d}	Number of teeth in contact at the sleeve bolloni
N,	Normal tooth load to the counting surface
N a	Number of slices along the facewidth
P	Diametral pitch
P_d	Individual normal tooth load
P_d^{s}	Load on a single tooth slice along the facewidth
P_i^{u}	Maximum normal tooth load
P'_i	Load per unit length
P_t	Total mean normal tooth load
P'_t	Mean normal tooth load
q	Load sharing ratio (number of teeth in contact)
R	PITCh radius Usb next another radius at nitab diamatan
K _C	Hub root crown radius at plich diameter Distance from the hub center to the contact area in the π direction
R _d	Hub face crown radius (normal plane)
Sc2	Design sleeve circular space width
S*2	Sleeve circular space width at the contact point
T^{c_2}	Transmitted torque
T _m	Restoring torque
t_{c1}, t_{c2}	Hub and sleeve tooth circular thickness
t_{c1}^{*}	Hub tooth circular thickness at the contact point
W _c	Coupling weight
W _d	Axial load that balances a coupling tooth
VV sh	Coupling shaft weight
W _{sh} V, V ₂	Hub and sleeve tooth ACMA form factor
$7_1, 7_2$	Hub and sleeve cloth Advia form lactor
7.0	Maximum tooth separation
Z e	Elastic tooth deformation
α	Tooth position angle offset
β	Misalignment direction
5	Misalignment angle
ξ	Jam angle
δ_b	Tooth backlash
δ _d	Normal tooth deformation
Δ_c	Accessible tooth root clearance
Δ_r	Design tooth root clearance
γ	1 III dilgit
і ф	Normal pressure angle
Ψ	Norman pressure angle

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