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## Low Temperature Sintering Characteristics of Hot Press Sintered SrFe<sub>12</sub>O<sub>19</sub> Ferrites for Use in Microwave LTCC Circulators

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**Abstract:** The SrFe<sub>12</sub>O<sub>19</sub> ferrites with different amounts of Bi<sub>2</sub>O<sub>3</sub> additive were prepared by a hot press sintering process at a low fired temperature of 870 °C in order to be compatible to the LTCC (low temperature co-fired ceramics) technology, and their low temperature sintering characteristics were investigated, including the crystal phase composition, sintering density, porosity, and magnetic properties. Results show that the addition of Bi<sub>2</sub>O<sub>3</sub> promotes the formation of SrFe<sub>12</sub>O<sub>19</sub> phase structure and increases the sintering compactness and magnetic properties of the ferrites fabricated at 870 °C. The ferrites with Bi<sub>2</sub>O<sub>3</sub> content from 2 wt% to 4 wt% exhibit a compact microstructure with sintering density higher than 4.65 g·cm<sup>-3</sup> and porosity lower than 10%, which contributes to the enhanced saturation magnetization  $M_s$  and intrinsic coercivity  $H_{ci}$  above 252.4 kA·m<sup>-1</sup> and 312.9 kA·m<sup>-1</sup>, respectively. Moreover, the potentiality of the SrFe<sub>12</sub>O<sub>19</sub> ferrites for use in microwave LTCC circulators was also discussed based on their low temperature sintering characteristics.

**Key words:** SrFe<sub>12</sub>O<sub>19</sub> ferrites; LTCC; hot press sintering; circulators

Low temperature sintering of gyro-magnetic ferrites is a crucial problem for microwave LTCC (low temperature co-fired ceramics) ferrite devices<sup>[1-6]</sup>. Because of high sintering temperature, the traditional and commercial gyro-magnetic ferrite materials are unable to co-fire with the inner electrode metal Ag in LTCC systems. M-type hexagonal barium ferrites (BaFe<sub>12</sub>O<sub>19</sub>) and strontium ferrites (SrFe<sub>12</sub>O<sub>19</sub>) can be used in microwave and millimeter wave ferrite devices due to their relatively high saturation magnetization  $M_{\rm s}$ , moderate intrinsic coercivity  $H_{ci}$ , large crystalline anisotropy field  $H_{a}$ , and appropriate resistivity  $\rho$ , which have been considered as the promising microwave LTCC ferrite materials<sup>[7-9]</sup>. Different additives were used as sintering aids to reduce the sintering temperature of the ferrites, typically including Bi<sub>2</sub>O<sub>3</sub>, BaCu  $(B_2O_5)$  and  $Bi_2O_3{\cdot}B_2O_3{\cdot}SiO_2{\cdot}ZnO$  (BBSZ), and their low

temperature sintering characteristics were improved<sup>[10-12]</sup>.

Hu Yun

In the present paper, the  $SrFe_{12}O_{19}$  ferrites with different amounts of  $Bi_2O_3$  additive were prepared by a hot press sintering process at a low fired temperature in order to be compatible to the LTCC technology. The crystal structure and magnetic properties of the ferrites were mainly investigated, and their potential applications in microwave LTCC circulators were also discussed.

## **1** Experiment

High purity ( $\geq$ 99.99 wt%) SrCO<sub>3</sub> and Fe<sub>2</sub>O<sub>3</sub> were weighed in composition of SrFe<sub>12</sub>O<sub>19</sub> for preparing stoichiometric ferrites. Raw materials were mixed and ball-milled at 300 r/min for 6 h, then dried and calcinated at 1250 °C for 2 h. Powders were further ball-milled with different amounts of Bi<sub>2</sub>O<sub>3</sub> additive from 0 to 5 wt% at 400

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r/min for 4 h, and then pressed into disks using a graphite mold and sintered at 870 °C under 60 MPa for 10 min. Particle size of powders was tested by laser particle analyser (JL-1178). Sintering density was measured by precision density balance (FA2004J) with resolution of 0.1 mg based on the Archimedes method. Crystal structure was detected by X-ray diffraction (XRD, DX-2700) with Cu Ka radiation. Direct-current resistivity was measured by precision power supply (Agilent, B2912A) from 0 to 200 V with resolution of 10 fA/100 nV. Magnetic hysteresis loops were tested by vibrating sample magnetometer (VSM, Versalab) to obtain the magnetic properties.

## 2 Results and Discussion

XRD patterns of the strontium ferrites with different  $Bi_2O_3$  contents are shown in Fig.1. The SrFe<sub>12</sub>O<sub>19</sub> phase with M-type hexagonal structure is formed in the ferrites with different Bi2O3 contents. For the ferrites without  $Bi_2O_3$  additive, the SrFe<sub>12</sub>O<sub>19</sub> phase coexists with the non-magnetic  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> phase and SrO<sub>2</sub> phase, where the diffraction peaks of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> phase like (110), (020), (130) peaks and a weak (002) peak of SrO<sub>2</sub> phase are observed. This is in agreement with the formation mechanism of  $SrFe_{12}O_{19}$  ferrites. The formation of  $SrFe_{12}O_{19}$  ferrites prepared by a solid phase method is mainly based on the reaction as  $SrCO_3+6Fe_2O_3=SrFe_{12}O_{19}+CO_2\uparrow$ , and the sintering temperature usually reaches above 1200 °C. Generally, Fe<sub>2</sub>O<sub>3</sub> can not fully participate in the reaction to produce SrFe<sub>12</sub>O<sub>19</sub> at low sintering temperatures. When the content of Bi<sub>2</sub>O<sub>3</sub> increases to 1 wt%, the crystal phase composition of the ferrites is still unchanged. It is worthwhile to note that the SrFe<sub>12</sub>O<sub>19</sub> ferrites with single phase structure are successfully obtained when the Bi<sub>2</sub>O<sub>3</sub> content increases to 3 wt%. The strength of (006) peak and (008) peak is obviously enhanced, suggesting an increased c axis preferred orientation in the ferrites. Redundant addition of Bi<sub>2</sub>O<sub>3</sub> additive is observed in the ferrites when the  $Bi_2O_3$  content further increases to 5 wt%, where a small amount of Bi<sub>2</sub>O<sub>3</sub> phase with weak (112), (121), and (012) peaks is detected. Moreover, the inter-planer spacing  $d_{hkl}$  of most crystal faces is found to get a significant decrease, which is strongly correlated with the lattice constants a and c.

Lattice constants of the strontium ferrites are calculated from the values of  $d_{hkl}$  corresponding to (107) peak and (114) peak by the following equations:

$$d_{hkl} = \left(\frac{4}{3}\frac{h^2 + hk + k^2}{a^2} + \frac{l^2}{c^2}\right)^{-1/2} \tag{1}$$

and the porosity P of the ferrites is obtained from

$$P = 1 - \frac{d_s}{d_x} \tag{2}$$

$$d_x = (1 - x)d_{\rm M} + xd_{\rm A} \tag{3}$$



Fig.1 XRD patterns of the SrFe<sub>12</sub>O<sub>19</sub> ferrites with different Bi<sub>2</sub>O<sub>3</sub> contents

$$d_{\rm M} = \frac{2M}{NV} \tag{4}$$

$$V = 0.8666a^2c$$
(5)

where h, k, and l are the Miller indices,  $d_x$  is the theoretical density of the ferrites,  $d_s$  is the sintering density of the ferrites, x is the amount of the additive,  $d_M$  is the X-ray density of SrFe<sub>12</sub>O<sub>19</sub>,  $d_A$  is the theoretical density of the additive, M is the molar mass of SrFe<sub>12</sub>O<sub>19</sub>, V is the lattice volume, and N is the Avogadro's number.

Evident effect of the  $Bi_2O_3$  content on the lattice constants of the strontium ferrites is observed, as shown in Fig.2. The large lattice constant *a* from 0.5898 nm to 0.5922 nm is obtained with  $Bi_2O_3$  content from 1 wt% to 4 wt%, which clearly exceeds the typical value of 0.588 nm. Correspondingly, the lattice constant *c* decreases to a range between 2.196 and 2.226 nm from a typical value of 2.307 nm. This indicates that the (001) face of the hexagonal structure is chiefly perpendicular to the pressure direction, leading to the lattice deformation.

Fig.3 gives the sintering density and porosity of the strontium ferrites with different contents of  $Bi_2O_3$  additive. The addition of  $Bi_2O_3$  is found to be conducive to increase the sintering density and to decrease the porosity of the ferrites, which is suggested to be strongly associated with the formation of  $Bi_2O_3$  liquid phase during the sintering process. The ferrites can provide a relatively compact microstructure with sintering density higher than 4.65 g·cm<sup>-3</sup> and porosity lower than 10% when the  $Bi_2O_3$  content varies from 2 wt% to 4 wt%. Low porosity can reduce the demagnetization field inside the ferrites and decrease the electromagnetic loss in high frequency applications.

Moreover, the enhanced saturation magnetization  $M_s$  and intrinsic coercivity  $H_{ci}$  are obtained for the ferrites due to the promoted low temperature sintering with appropriate amount of Bi<sub>2</sub>O<sub>3</sub> additive, as shown in Table 1. To the contrary, the redundant non-magnetic Bi<sub>2</sub>O<sub>3</sub> phase results in depressed magnetic properties, and there is a great Download English Version:

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