



Harmonic elastic inclusions in the presence of point moment

Xu Wang^a, Peter Schiavone^{b,*}

^a School of Mechanical and Power Engineering, East China University of Science and Technology, 130 Meilong Road, Shanghai 200237, China

^b Department of Mechanical Engineering, University of Alberta, 10-203 Donadeo Innovation Centre for Engineering Edmonton, Alberta T6G 1H9, Canada

ARTICLE INFO

Article history:

Received 16 August 2017

Accepted 14 October 2017

Available online 26 October 2017

Keywords:

Inverse problem

Harmonic elastic inclusion

Conformal mapping function

Point moment

ABSTRACT

We employ conformal mapping techniques to design harmonic elastic inclusions when the surrounding matrix is simultaneously subjected to remote uniform stresses and a point moment located at an arbitrary position in the matrix. Our analysis indicates that the uniform and hydrostatic stress field inside the inclusion as well as the constant hoop stress along the entire inclusion–matrix interface (on the matrix side) are independent of the action of the point moment. In contrast, the non-elliptical shape of the harmonic inclusion depends on both the remote uniform stresses and the point moment.

© 2017 Académie des sciences. Published by Elsevier Masson SAS. All rights reserved.

1. Introduction

In the manufacture of composite materials, ‘harmonic’ inclusions are designed to leave unperturbed everywhere the first invariant of the uncut stress field (or the mean stress) when inserted into a stressed matrix [1–5]. The terminology ‘harmonic’ is used in this context since the first invariant of the stress tensor is a harmonic function in linear plane elasticity. In previous studies [1–5], the analysis of harmonic inclusions has been undertaken in cases when the matrix is subjected to only uniform or non-uniform stresses at infinity without the possibility of any additional concentrated loading (e.g., a point moment or a circular transformation strain spot). The importance of the analysis of elastic fields subjected to pointwise singularities such as point moment is well-documented. These singular fields are important not only because of their physical significance within micromechanics but also because they often form the basis for fundamental solutions used in, for example, the boundary integral equation method (see, for example, [6]). With this in mind, we pose the following question:

Is it possible to design harmonic inclusions if the matrix is additionally subjected to a point moment?

In this paper, we will address this question. Using complex variable methods, we will demonstrate the design of harmonic elastic inclusions when the matrix is subjected to remote uniform stresses and a point moment applied at an arbitrary position in the matrix. A novel conformal mapping function is first constructed to account for the existence of the point moment. The interface and boundary conditions then allow us to determine analytically the two complex parameters appearing in the mapping function for given loadings. Our results indicate that the internal stress distribution inside the harmonic inclusion is uniform and hydrostatic whilst the hoop stress along the entire inclusion–matrix interface (on the matrix side) remains constant. Both of these stress distributions are found to be independent of the point moment. Consequently, our design also attains the “constant strength” design criterion proposed by Cherepanov [7]. Furthermore, the shape of the harmonic

* Corresponding author.

E-mail addresses: xuwang@ecust.edu.cn (X. Wang), p.schiavone@ualberta.ca (P. Schiavone).

inclusion depends on both the remote uniform stresses and the point moment. Several specific examples are presented to illustrate our results.

2. Problem formulation

For plane deformations of an isotropic elastic material, the stresses $(\sigma_{11}, \sigma_{22}, \sigma_{12})$, displacements (u_1, u_2) and stress functions (ϕ_1, ϕ_2) can be expressed in terms of two analytic functions $\varphi(z)$ and $\psi(z)$ of the complex variable $z = x_1 + ix_2$ as [8]

$$\sigma_{11} + \sigma_{22} = 2[\varphi'(z) + \overline{\varphi'(z)}] \quad (1)$$

$$\sigma_{22} - \sigma_{11} + 2i\sigma_{12} = 2[\bar{z}\varphi''(z) + \psi'(z)]$$

$$2\mu(u_1 + iu_2) = \kappa\varphi(z) - z\overline{\varphi'(z)} - \overline{\psi(z)} \quad (2)$$

$$\phi_1 + i\phi_2 = i[\varphi(z) + z\overline{\varphi'(z)} + \overline{\psi(z)}]$$

where the constant $\kappa = 3 - 4\nu$ in the case of plane strain deformations (assumed here), $\kappa = (3 - \nu)/(1 + \nu)$ for plane stress and μ , ν ($0 \leq \nu \leq 1/2$) are the shear modulus and Poisson's ratio, respectively. In addition, the stresses are related to the stress functions by [9]

$$\sigma_{11} = -\phi_{1,2}, \quad \sigma_{12} = \phi_{1,1} \quad (3)$$

$$\sigma_{21} = -\phi_{2,2}, \quad \sigma_{22} = \phi_{2,1}$$

Consider a domain in $\mathbb{R}^2$, infinite in extent, containing a single internal elastic inclusion with elastic properties different from those of the matrix. We represent the matrix by the domain S_2 and assume that the inclusion occupies a region S_1 . The inclusion-matrix interface is denoted by L . The matrix is subjected to remote uniform in-plane stresses $(\sigma_{11}^\infty, \sigma_{22}^\infty, \sigma_{12}^\infty)$ and a point moment M at some arbitrary point $z = z_0$ in the matrix. The criterion to be satisfied in the design of a harmonic elastic inclusion is that the mean stress $\sigma_{11} + \sigma_{22}$ in the matrix is not disturbed when the inclusion is inserted into the matrix. In what follows, the subscripts 1 and 2 are used to identify the respective quantities in S_1 and S_2 .

The corresponding boundary value problem thus takes the form

$$\varphi_2(z) + z\overline{\varphi_2'(z)} + \overline{\psi_2(z)} = \varphi_1(z) + z\overline{\varphi_1'(z)} + \overline{\psi_1(z)} \quad (4)$$

$$\kappa_2\varphi_2(z) - z\overline{\varphi_2'(z)} - \overline{\psi_2(z)} = \Gamma\kappa_1\varphi_1(z) - \Gamma z\overline{\varphi_1'(z)} - \Gamma\overline{\psi_1(z)}, \quad z \in L$$

$$\varphi_2(z) \equiv \frac{\sigma_{11}^\infty + \sigma_{22}^\infty}{4}z, \quad z \in S_2 \quad (5)$$

$$\psi_2(z) \cong \frac{\sigma_{22}^\infty - \sigma_{11}^\infty + 2\sigma_{12}^\infty}{2}z + O(1), \quad |z| \rightarrow \infty \quad (6)$$

$$\psi_2(z) \cong \frac{iM}{2\pi} \frac{1}{z - z_0} + O(1), \quad \text{as } z \rightarrow z_0 \quad (7)$$

where $\Gamma = \mu_2/\mu_1$. The singular behavior in Eq. (7) for a point moment follows from the analysis in [6]. We note here that the point moment will not induce any singular behavior in $\varphi_2(z)$ [6].

3. Harmonic elastic inclusions

The conformal mapping function is assumed to take the following form

$$z = \omega(\xi) = R\left(\xi + \frac{p}{\xi} + \frac{q}{\xi - \xi_0^{-1}}\right), \quad \xi = \omega^{-1}(z), \quad |\xi| \geq 1 \quad (8)$$

where R is a real scaling constant, p and q are complex constants to be determined, and $\xi_0 = \omega^{-1}(z_0)$. The region occupied by the matrix in the z -plane is mapped onto $|\xi| \geq 1$ in the ξ -plane, and the interface L is mapped onto the unit circle $|\xi| = 1$. The appearance of the first-order pole in Eq. (8) is to account for the existence of the point moment at $z = z_0$.

In order to ensure that the mean stress in the surrounding matrix is not disturbed by the inclusion, the two analytic functions defined in S_1 should take the following form

$$\varphi_1(z) = \frac{A}{R}z, \quad \psi_1(z) = 0, \quad z \in S_1 \quad (9)$$

where A is a real constant.

Download English Version:

<https://daneshyari.com/en/article/7216188>

Download Persian Version:

<https://daneshyari.com/article/7216188>

[Daneshyari.com](https://daneshyari.com)