

# Electrohydrodynamic gas flow in a positive polarity wire-plate electrostatic precipitator and the related dust particle collection efficiency

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## Abstract

In this paper, the results of the particle image velocimetry measurements of the flow velocity fields in an intermediate spacing wire-to-plate type electrostatic precipitator (ESP) with a single positive polarity wire electrode are presented. The observation plane was placed perpendicular to the wire electrode at its half-length. The investigation showed significant influence of the electric field and charge on the flow patterns in the intermediate spacing ESP under an extreme large electrohydrodynamic (EHD) number. The EHD forces cause the formation of strong vortex pairs in the upstream and downstream ESP regions for  $Ehd/Re^2 > 1$ .

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## 1. Introduction

The motion and precipitation of particles in the duct of an electrostatic precipitator (ESP) depend on the dust-particle properties, electric field, space charge and gas-flow field. It has been shown [1,2] that a significant interaction between these factors exists, resulting in considerable turbulent flow structures in the volume between the stressed and collecting electrodes. However, it is not yet clear whether these turbulent flow structures advance or deteriorate the fine particle precipitation process. To elucidate the influence of the electrically generated flow disturbances in the case of a high resistivity cleaning process in intermediate spacing ESPs, more experimental investigations are needed.

Recently, the method of particle image velocimetry (PIV) [3] was introduced for instantaneous measurement of the flow velocity field, including the turbulence, in large cross-sections of the flow. In particular, the PIV technique has been used for investigating the structure of electrohydrodynamically induced secondary flow in ESPs [4–7].

In this paper, the results of PIV measurements of the flow velocity fields for large electrohydrodynamic (EHD) numbers in an intermediate spaced wire-plate ESP with positive polarity wire are presented.

## 2. Experimental setup

The apparatus used in this experiment consisted of an ESP, a high-voltage supply, and standard PIV equipment for the measurement of velocity fields. The

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measuring method and schematics of the apparatus were described in detail in reference [4].

The ESP had a single wire electrode (diameter 1 mm, length 200 mm) placed in the middle of the ESP between two grounded, stainless steel plate electrodes. The plate electrode widths were 200 mm each, while the plate-to-plate electrode spacing was 100 mm. The PIV measurements were carried out in a plane placed perpendicular to the wire electrode at its half-length.

Airflow seeded with fine  $\text{TiO}_2$  particles (size less than  $1 \mu\text{m}$ ) was blown along the reactor duct with an average velocity that varied from 0 to 1.0 m/s. The positive voltage applied to the wire electrode through a 10-M $\Omega$  resistor was varied between 0 and 35 kV. The Reynolds and EHD numbers varied from 0 to 6000, and from 0 to  $2 \times 10^8$ , respectively [8].

The flow velocity field maps ( $100 \times 400 \text{ mm}$ ) presented in this paper are composed of four adjacent velocity fields ( $100 \times 100 \text{ mm}$  each). All the velocity fields presented resulted from the averaging of 100 measurements; thus each velocity map shown is time averaged.

### 3. Results

The flow velocity field patterns and corresponding flow streamlines in the intermediate spacing wire-plate type ESP are shown in Fig. 1 for the case of no primary flow ( $U_0 = 0 \text{ m/s}$ ), and in Fig. 2 for a primary

flow velocity of 0.3 m/s. Figs. 1a and 2a show the flow velocity field patterns and the corresponding flow streamlines in the ESP without the primary flow ( $Re = 0$ ;  $Ehd/Re^2 \rightarrow \infty$ ) for a time-averaged discharge current of value  $I = 150 \mu\text{A}$ . Two pairs of strong vortices of the secondary flow are clearly visible in both the upstream and downstream regions of the corona wire. The flow in the vortices moves from the wire electrode almost perpendicularly towards the plate electrodes, then along the plate electrodes, turning back towards the wire electrode at a distance of about 120–130 mm from the wire electrode. The secondary flow vortices are caused by the EHD forces resulting from the applied electric field and space charge formed. The apparent asymmetry in the velocity field pattern shown in Fig. 1, usually not expected for  $U_0 = 0 \text{ m/s}$  and  $Ehd/Re^2 \rightarrow \infty$ , might not result from the imperfection of the electrode and duct arrangement only. Rather, it might be a result of the stochastic onset of an asymmetric, unsteady turbulent flow. This effect was not removed in the relatively short image averaging process (over 40 s).

Figs. 1b and 2b show the flow patterns and the corresponding streamlines in the ESP at a primary flow velocity of 0.3 m/s and total discharge current  $I = 150 \mu\text{A}$ . At this velocity, the Reynolds number ( $Re = U_0 L / \nu$ ) is equal to 2000, the Ehd number ( $Ehd = L^3 I / \mu_i \rho \nu^2 A$ ) is equal to  $2 \times 10^8$ , and the ratio  $Ehd/Re^2$  is equal to 50 [8]. The parameters used to calculate  $Re$  and

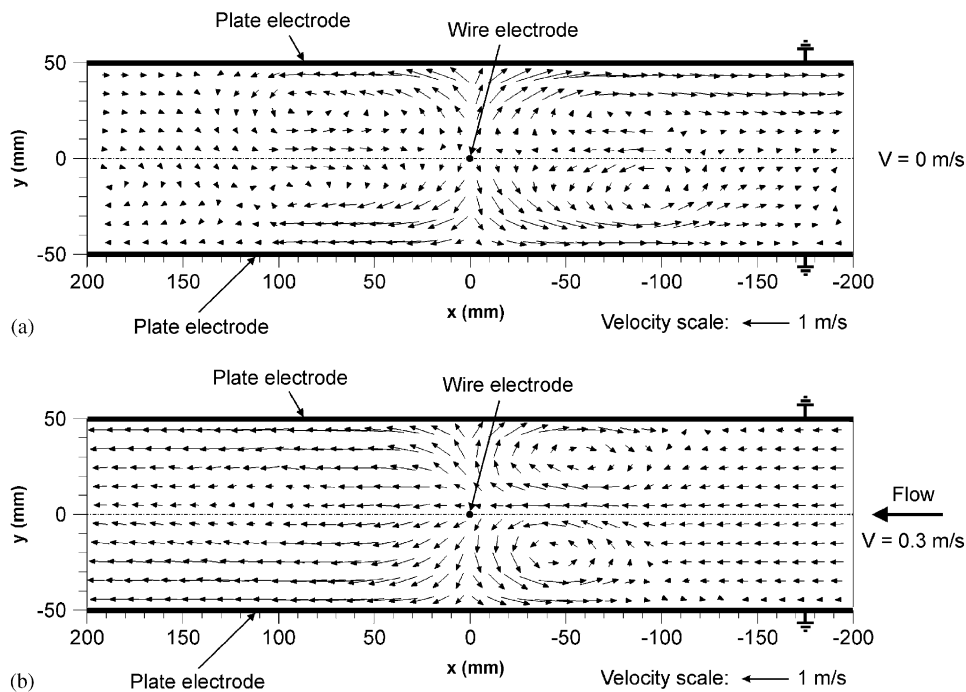


Fig. 1. Flow velocity field patterns in the wire-to-plate type ESP. The primary flow velocities: (a) 0 m/s ( $Re = 0$ ), (b) 0.3 m/s ( $Re = 2000$ ). Positive voltage varied from 30 to 32 kV to maintain discharge current at  $150 \mu\text{A}$  ( $Ehd = 2 \times 10^8$ ).

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