

A novel angle-tuned thin film filter with low angle sensitivity

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ABSTRACT

An angle-tuned thin film narrowband filter is widely used in the dense wavelength division multiplexing (DWDM) system. With increase of incident angle of the thin film filter, the central wavelengths of both S-polarization and P-polarization will separate obviously and shift to short wavelength much faster, which will cause serious polarization sensitivity and angle sensitivity. In conventional angle-tuned thin film filters, the research works usually focus on the polarization sensitivity. However, their angle sensitivity is very high because the effective refractive indexes of their spacer are very low. Their precision of the angle controlling system is very rigorous (less than 0.005°) and their incident angles are usually less than 20° , which will limit their wavelength tuning range. In the present paper, we propose and fabricate a novel 100 GHz angle-tuned thin film filter stack with low angle sensitivity which uses the high refractive index material α -Si as the spacer and its incident angle can be expanded to 32° . Using the polarization beam-splitters and the half wave plates, this angle-tuned thin film filter can also eliminate the polarization sensitivity. The simulation results and the experiments show that the angle-tuned thin film filter with low angle sensitivity has a effective tuning range of 40 nm, which can cover the whole C-band and its precision of the angle control is relatively easy (more than 0.05°).

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1. Introduction

With low insertion loss, high adjacent channel isolation and good temperature stability, the multiple-cavity narrowband thin film filter is widely used in the DWDM system [1]. When thin film filter is used in oblique incidence, the spacer effective optical thickness will decrease and the central wavelength will shift to short wavelength, and the central wavelength of P-polarization will not coincide with that of S-polarization [2], which will cause serious polarization sensitivity [3]. With the rapid development of thin film de-polarization technique, more and more angle-tuned thin film filters are emerging [4–7]. For conventional dielectric angle-tuned thin film filter, the central wavelength shift velocity is too high in large incident angle because its spacer effective refractive index is relatively low (usually less than 1.8), which will cause the serious angle sensitivity, and it will cause the high cost and difficult precision of its the angle controlling system.

According to the ITU protocol, the central wavelength positioning precision of current 100 GHz channel spacing DWDM system should be less than ± 8 pm. So the angle controlling precision of the conventional 100 GHz angle-tuned thin film filter is very rigorous, especially in the large angle oblique incidence, even less

than 0.005° [8]. It will cause serious angle sensitivity and high cost of the angle controlling systems, which will limit its tunable wavelength range and the incident angle range (usually less than 20°).

In this paper, we design and fabricate a novel 100 GHz channel spacing angle-tuned thin film filter with low angle sensitivity by using the high refractive index material α -Si as its spacer, which incident angle can be enlarged to 32° . Based on the polarization beam-splitters and the half wave plates, the polarization sensitivity of the angle-tuned thin film filter can also be eliminated. The theoretical analysis and the experimental results indicate that its tunable range is more than 40 nm and its easy precision of the angle controlling system is more than 0.05° .

2. Theoretical analysis

2.1. Angle sensitivity

The variation of the performances of a dielectric Fabry–Perot thin film filter with incident angle is a well known effect, which has been widely studied and often used by manufactures to ease a little some too tight production tolerances. The tuning equation of such a filter is given by [9]:

$$\lambda = \lambda_0 \sqrt{1 - (\sin^2 \theta / n_{\text{eff}}^2)} \quad (1)$$

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where λ_0 is the central wavelength in normal incidence, λ is the central wavelength in oblique incidence, θ is the incident angle of the collimated light beam and n_{eff} is the effective refractive index of the spacer.

From Eq. (1) we can see that the central wavelength of the thin film filter will shift to short wavelength while the incident angle is increasing. The wavelength shift velocity is determined by the spacer effective refractive index n_{eff} , which is intermediate between the high and low refractive index materials of the thin film filter [10,11]:

$$n_{eff} = n_L \left[\frac{m - (m-1)(n_L/n_H)}{m - m(n_L/n_H) + (n_L/n_H)^2} \right]^{1/2} \quad \text{for a low-index spacers} \quad (2)$$

$$n_{eff} = n_H \left[\frac{m - (m-1)(n_L/n_H)}{(m-1) - (m-1)(n_L/n_H) + (n_H/n_L)} \right]^{1/2} \quad \text{for a high-index spacers} \quad (3)$$

where n_H is the refractive index of the high refractive index material, n_L is the refractive index of the low refractive index material and m is the order number of the spacer.

Conventional narrowband thin film filter usually use the $\text{Ta}_2\text{O}_5/\text{TiO}_2$ and SiO_2 as its high and low refractive index materials. According to the 100 GHz channel spacing DWDM system protocol, the passband (@ -0.5 dB) of the thin film filter should be large than 0.3 nm and the stopband (@ -25 dB) should be less than 1.3 nm. Two typical 100 GHz three-cavity narrowband thin film filter stacks which use only the low or high refractive index materials as the spacer are given by:

$$G/[(HL)^8 6L(LH)^8 L]^3 / A \quad (4)$$

$$G/[(HL)^8 4H(LH)^8 L]^3 / A \quad (5)$$

where G and A denote glass and air, respectively. Low index material L is SiO_2 ($n_L = 1.46$) and high index material H is Ta_2O_5 ($n_H = 2.05$), which are both quarter wavelength coatings [12]. Given $n_G = 1.523$ and reference wavelength $\lambda_0 = 1565$ nm in normal incidence.

In oblique incidence, the refractive of S-polarization is $n_s = n \cos \theta$ and the refractive of P-polarization is $n_p = n / \cos \theta$, where n is the refractive index in normal incidence. Hence, the central wavelengths of both the S-polarization and P-polarization light will separate while the incident angle is increasing. The theoretical central wavelengths (of all the average light, S-polarization and P-polarization light) of the stack (4) and stack (5) vary with the angle of incidence are shown in Fig. 1, respectively. From Fig. 1 we can see that the central wavelength

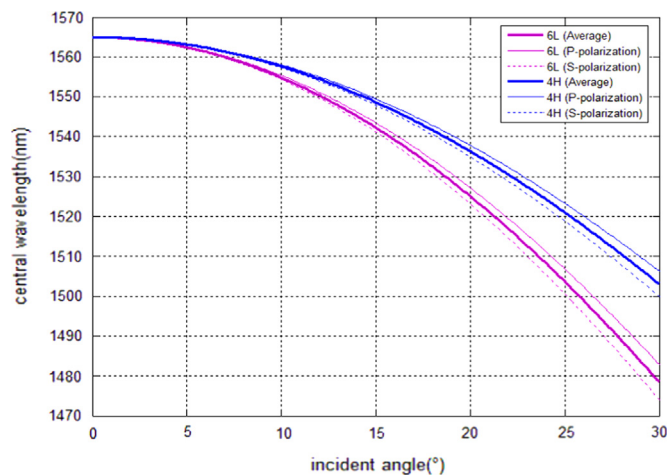


Fig. 1. Shift of central wavelength with angle of incidence.

of the average light shift to short wavelength is much faster while the incident angle is increasing and the wavelength shift velocity of the high refractive index spacer is much slower than that of low refractive index spacer. For a 100 GHz DWDM system, the adjacent channel spacing should be 0.8 nm, so the angle controlling system precision in large angle incidence is much higher than that of in small angle incidence. The high angle sensitivity in large incident angle of the thin film filter will limit the wavelength tunable range and the wavelength positioning precision. So conventional angle-tuned thin film filter usually used within 20° oblique incidence and it should have high-cost rigorous angle controlling system.

2.2. Low angle sensitivity stack design

In oblique incidence, the central wavelength shift for the S-polarization in a low-index-spacer filter is larger than that for a P-polarization; the central wavelength shift for S-polarization in a high-index-spacer filter is less than that for P-polarization [13], which will cause serious polarization sensitivity and the polarization dependent loss. In our former work, we found that the central wavelengths of the S-polarization and P-polarization light will coincide by using both high and low refractive index materials (Ta_2O_5 and SiO_2) as the spacer. In this way, a four-cavity 100 GHz narrowband de-polarization angle-tuned thin film filter is designed and fabricated, which stack structure is as follows [8]:

$$G/[(HL)^7 2L3H4L3H2L(LH)^7 L(HL)^8 2L3H4L3H2L(LH)^8 L(HL)^8 2L3H4L3H2L(LH)^8 L(HL)^7 2L3H4L3H2L(LH)^7] / A \quad (6)$$

The stack (6) has a tunable wavelength range from 1561 nm to 1528 nm. However, the angle sensitivity of the stack (6) is very high because its spacer effective refractive index is very low ($n_{eff} = 1.65$), which can only be used within 20° oblique incidence. According to the ITU protocol, the central wavelength positioning precision of the 100 GHz channel spacing DWDM system should be less than ± 8 pm, so that its angle controlling precision should be less than 0.005° . In its angle controlling system we had to use the high-precision Faulhaber motor, related reducer and encoder to get the rigorous angle controlling precision so that the cost of this device is very high.

In order to decrease the cost of the angle controlling system, the spacer effective refractive index should be increased, which will decrease the wavelength shift velocity and increase the incident angle range. Compared with the conventional high refractive index materials TiO_2 ($n = 2.25$) and Ta_2O_5 ($n = 2.05$), the material α -Si has higher refractive index. So we can use α -Si and SiO_2 to construct a novel narrowband angle-tuned thin film filter stack with low angle sensitivity, especially use the high refractive index material α -Si as the spacer of the thin film filter. Using the ion-beam-sputtering technology, the α -Si film can be fabricated in the Leybold Helios sputtering system, which its material refractive index is 3.2 and its extinction coefficient K is 1.45×10^{-5} . Using the global optimization algorithm [8], we designed a novel α -Si spacer three-cavity angle-tuned thin film filter stack as follows:

$$G/[(HL)^4 4H(LH)^4 L]^3 1.83H0.6L / A \quad (7)$$

where low index material L is SiO_2 , high index material H is α -Si ($n_H = 3.2$, $K = 1.45 \times 10^{-5}$) and reference wavelength $\lambda_0 = 1565$ nm. The double layer coating $1.83H0.6L$ in the stack (7) is the anti-reflection film. The stack (7) has fewer layers than that of the stack (4) to stack (6) due to its larger refractive index difference between the high and low refractive index materials used in the stack.

The theoretical central wavelengths (of all the average light, S-polarization and P-polarization light) of the stack (6) and stack (7) vary with the angle of incidence are shown in Fig. 2,

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