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Detecting the internal short circuit in large-format lithium-ion battery using model-based fault-diagnosis algorithm



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ABSTRACT

The spontaneous internal short circuit that sporadically occurs during operation is an unsolved safety problem that hinders the widespread application of lithium ion batteries. An online fault-diagnosis algorithm is an urgent requirement for early detection of the spontaneous internal short circuit of lithium-ion batteries to guarantee safe operation. This paper presents a model-based fault-diagnosis algorithm for online internal-short-circuit detection. Relying on the theory of model-based control, the algorithm transforms the measured voltage and temperature to the intrinsic electrochemical status that can reflect typical internal-short-circuit faulters, i.e. the excessive depletion of capacity and abnormal heat generation. The estimated status of the suspicious cell deviates from the average value of the battery pack, therefore the algorithm can capture the internal-short-circuit fault by evaluating the levels of deviation. Simultaneously considering the diagnosis result calculated from both the voltage and temperature signal helps enhance the robustness of the algorithm with few false alarms. Substitute internal-short-circuit tests confirm that the algorithm is capable of identifying the internal-short-circuit fault before it develops into a severe hazard, e.g., thermal runaway. The equivalent short resistance, which can reflect the level of the internal short circuit, can be estimated with small error by the online fault-diagnosis algorithm.

1. Introduction

The new energy vehicle market is thriving, owing to breakthroughs in the energy density and cycle life of lithium-ion batteries [1,2]. However, safety problems have appeared as the industry is pursuing higher energy densities for lithium-ion batteries [3–5]. Cramming more active materials within a battery package is an intuitive solution to enhance the energy density, but this causes a higher potential for an internal short circuit (ISC) [6], e.g., the accidents in the Boeing Dreamliner [7] and Samsung Galaxy S7 [8].

The actual formation mechanism of a spontaneous ISC during onboard operation still requires further study; while researchers have not ceased to explore the "truth." A lithium dendrite that pierces the separator and connects the cathode with the anode is thought to be one of the causes for the spontaneous ISC [9]. The growth of a lithium dendrite has been confirmed by microscopy [10–12], whereas the growth behavior can be predicted by electrochemical models [13]. Current models cannot simulate the full growing process of a lithium dendrite including all the interactions at the interface between the anode, electrolyte, and the separator [14,15]. Therefore modeling the formation of the full electric circuit for ISC still requires further study. Evidences indicate that once an electric circuit that discharges the cell is formed, the ISC will influence the thermal runaway behavior of lithium-ion batteries [16–18]. However, the mechanism of thermal runaway induced by an ISC is still unclear [19], and new interpretations are emerging sporadically [20,21].

To secure the battery pack from an ISC hazard, an online fault-diagnosis algorithm that can early detect an ISC is essential [6]. Fig. 1 shows the scheme of developing an online fault-diagnosis algorithm for ISC detection, including three correlated levels. Level I is for data generation, which can be used for model calibration, knowledge (of the ISC characteristics) accumulation, and algorithm validation. Level II is for the ISC characterization, which indicates the key features that can be used for fault diagnosis. Level III is for algorithm development, which utilizes all types of fault-diagnosis algorithms.

The objective of Level I is to generate sufficient data for the researchers/engineers to characterize the ISC behavior, and to validate the fault-diagnosis algorithm. Researchers are attempting to develop a proper substitute ISC test approaches to simulate the real failure of an ISC and to facilitate the characterization of the ISC features [22].

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Nomenclature		$y_{1,k}^{\rm F}, y_{2,k}^{\rm F}$	The intermediate vector for temperature filtering, the su- perscript "F" means "after filtering" (°C)	
Ak. Ck	Matrix for the state-space model of battery $(/)$	Ζ	The data observation in the algorithm of parameter iden-	
$A_{\rm S}$	The surface area of the battery (m^2)		tification using recursive least squares (V)	
C_1	The first-order capacitance in the battery model (F)	$z_{1,k}^{\rm F}, z_{2,k}^{\rm F}$	The intermediate Z vector for temperature filtering, the	
C_p	The heat capacity of the battery (J·kg-1·K-1)		superscript "F" means "after filtering" (W)	
Ε	The error between the measured voltage and the predicted	α	The first-order time constant for the battery model (s)	
	voltage (V)	β	The forgetting factor in the parameter identification al-	
h T	The heat convection coefficient (W·m-2·K-1)		gonum (1)	
1	The current (A)	γ Δ R ο	The level of abnormal heat generation defined as the	
Iheat	the mean current in the test for the determination of the mean support houndary in an ISC case (A)	1 1(2)	quotient of the worst $R_{\rm O}$ and the average $R_{\rm O}(\Omega)$	
i.	The index number of the cell that has the minimum tem-	ΔSOC	The difference between the average value and the worst	
-1	perature ((1))		value of the SOC of the battery pack (1)	
i _V	The index number of the cell that has the minimum vol-	ΔT	The difference between the average temperature and the	
	tage ((1))		maximum temperature in the battery pack (°C)	
L	The feedback gain for state update ((1))	Δt	The sampling interval of time (s)	
M	The mass of the battery (kg)	ΔV	The difference between the average voltage and the	
Р	The covariance matrix for the parameter identification	e	The estimation error in the parameter identification al-	
D	algorithm (/) The heat newer in the test for the determination of	ε	gorithm (W)	
I heat	thermal runaway boundary in an ISC case (W)	$\eta_{\rm C}$	The columbic efficiency (1)	
$Q_{\rm st}$	The standard capacity of the battery (Ah)	Θ	The vector for the parameters to be identified in the al-	
R_0	The direct-current resistance in the battery model (Ω)		gorithm of parameter identification using recursive least	
R_1	The first-order resistance in the battery model (Ω)		squares (/)	
R _{heat}	An embedded resistance to generate ohmic heat to heat	Λ_{S}	The preset threshold for judging ISC relying on the value	
_	the battery to thermal runaway (Ω)	v ⁻	of $\Psi_{\Sigma}(1)$ The priori covariance matrix (1)	
R _{ISC}	The equivalent short resistance at the ISC point (Ω)	Σ^+	The posteriori covariance matrix (1)	
K_{Ω}	approximation power considering the surrout (Q)	Σ	The error covariance matrix for the state undate (1)	
$\overline{R_{o}}$	The average $R_{\rm o}$ in the battery pack (O)	$\Sigma_{\rm w}$	The covariance matrix for the measurement noise (1)	
Row	The $R_{\rm O}$ for the "worst cell" that has the highest tempera-	Φ	The vector for the data input in the algorithm of parameter	
-22,77	ture (Ω)		identification using recursive least squares (/)	
SOC	The state of charge (1)	φ	The intermediate Φ vector for temperature filtering (A ²)	
SOC	The average SOC in the battery pack (1)	Ψ_1	The fault level indicating excessive capacity depletion (1)	
SOC_W	The SOC for the "worst cell" that has the lowest voltage	Ψ_2	The fault level indicating abnormal heat generation (1)	
T	(1) The tensor (20)	Ψ ₃ Ψ.	The fault level indicating large temperature deviation (1)	
$\frac{1}{T}$	The exercise temperature in the bettery pack (°C)	Ψ_{T}	The fault level calculated from the temperature signal (1)	
T T	The temperature rise rate (°C·s -1)	$\Psi_{\rm V}$	The fault level calculated from the voltage signal (1)	
T _{IN}	The internal temperature of the battery (°C)	Ψ_{Σ}	The overall fault level for ISC detection (1)	
$T_{\rm lim}$	The temperature limit for safe operation (°C)			
$T_{\rm OUT}$	The temperature measured on the surface of the battery	Subscript		
	(°C)	::	Index number for better cell or thermoscuples	
T _W	The maximum temperature in the battery pack (°C)	l, j k	Time index	
T.∞ +	The ambient temperature (°C) The time when the internal short aircuit is detected by the	K V	For the voltage.	
$\iota_{\rm DT}$	algorithm (s)	T	For the temperature.	
tisc	The triggering time of internal short circuit (s)		*	
$t_{\text{Lev},1}, t_{\text{Lev}}$	$t_{1,1}, t_{1,ev,2}, t_{1,ev,3}$ The moment when the algorithm returns fault flag		Superscript	
	$\Psi_1 = 1, \Psi_1 = 2, \Psi_1 = 3$ (s)			
$t_{\rm TR}$	The time when thermal runaway occurs (s)	-	The priori state estimates.	
U_1	The voltage at the first-order resistance in the battery	+	The posteriori state estimates.	
	model (V)	Abbreviations		
$\frac{V}{V}$	The every voltage (V)			
v V	The real voltage measures in experiment (V)	BMS	Battery management system	
$V_{\rm exp}$	The voltage limit for safe operation (V)	FUDS	Federal urban driving schedule	
$V_{\rm mdl}$	The voltage predicted by the model (V)	ISC	Internal short circuit	
$V_{\rm W}$	The minimum voltage in the battery pack (V)	OCV	Open circuit voltage	
V_{1-3}	The average voltage between the time from $\Psi_1=1$ to	SOC	State of charge	
0 0	$\Psi_1 = 3 \text{ (V)}$	USARC	I S advanced battery consortium	
$y_{1,k}^0, y_{2,k}^0$	The intermediate vector for temperature filtering, the superscript "0" means "before filtering" (°C)	05/100	o.o. advanced battery consortium	

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