



# Development and validation of a semi-empirical model for the estimation of particulate matter in diesel engines



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## ABSTRACT

A semi-empirical correlation for the estimation of PM (particulate matter) emissions in diesel engines, as a function of significant engine operating variables, has been developed and validated on a GM (General Motors) Euro 5 diesel engine.

The experimental data used in the present study have been acquired at the dynamic test bench of ICEAL-PT (Internal Combustion Engine Advanced Laboratory at the Politecnico di Torino), in the frame of a research activity with GMPT-E (General Motors PowerTrain-Europe) for the calibration of a Euro 5 prototype 2.0 liter diesel engine equipped with a twin-stage turbine and a piezo-driven Common Rail injection system. The experimental data were acquired for six key-points representative of the engine working conditions over a NEDC (New European Driving Cycle). The experimental tests have been carried out according to the Design of Experiment approach and for each point several variation lists of the main engine variables have been considered.

As a first step, the main engine variables which are expected to be related to the formation and oxidation of PM have been identified. An exponential mathematical model has then been introduced and a detailed statistical analysis has been carried out for each key-point in order to identify the most robust combination of the input variables among all the possible ones.

It was verified that PM emissions are correlated to a great extent to the value of the chemical heat release at the end of the injection of the main pulse. This quantity is in fact related to the mass of burned gases which is generated by the oxidation of the pilot pulses that precede the main injection. Such a mass can have a large impact on the local oxygen concentration and temperature of the charge in which the fuel of the main pulse is injected, with a consequent effect on PM formation. Additional quantities have also been considered in the investigation: the relative air-to-fuel ratio  $\lambda$ , the intake charge oxygen concentration, the accumulated fuel mass, the equivalence ratio of the spray at the main pulse start of combustion and some combustion metrics related to the heat release rate.

At the end of the statistical analysis, the most influencing parameters have been selected and a semi-empirical model to predict the in-cylinder formed PM mass has been developed. The model has hence been tested under both steady-state and transient conditions.

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## 1. Introduction

Several studies have been carried out on a scientific basis on the effect of the particulate matter (PM) emissions on the human health as well as on the climate changes [1–8] and it is worth observing that diesel engines highly contribute to the overall PM emissions. Thus, the reduction of diesel emissions holds a key role for further penetration of the diesel engine in the automotive market. The emission legislations have become even more stringent

and have resulted into increasing interest into the understanding of the mechanisms of PM formation and oxidation in internal combustion engines.

PM is made up of clusters of spherical particles, which widely vary in size, on which several compounds are absorbed [9,10]. The insoluble fraction of the diesel particulate matter is usually referred to as soot, and consists of solid carbonaceous substances carrying unburned hydrocarbons, metals and superficially absorbed sulfates [11]. The mechanism that leads to the formation of soot from the liquid- or vapor-phase hydrocarbons is generally related to six fundamental processes [11], namely pyrolysis, nucleation, coalescence, surface growth, agglomeration and oxidation. Several experimental studies, conducted in the past years with

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**Nomenclature**

$a$	reduction coefficient of the spreading angle of the idealized spray model	PPM	pilot-pilot-main injection strategy
AC	alternating current	PPMA	pilot-pilot-main-after injection strategy
BMEP	brake mean effective pressure	$q$	injected fuel volume
$c$	coefficient of sensitivity	$q_{\text{aft}}$	injected fuel volume quantity of the after injection
$C$	PM mass emissions in mg/Nm <sup>3</sup>	$q_{\text{av,max,main}}$	maximum value of the accumulated fuel mass after SOI <sub>main</sub>
$C_a$	contraction area coefficient	$q_{\text{f,inj}}$	total injected fuel volume quantity
$C_d$	discharge coefficient	$q_{\text{pil2}}$	injected fuel volume quantity of pil2 injection
$C_v$	velocity coefficient	$q_{\text{pil1}}$	injected fuel volume quantity of pil1 injection
CA	crank angle	$Q_{\text{ch}}$	chemical energy release
CFD	Computer Fluid-Dynamics	$Q_{\text{ch}}(\text{EOI}_{\text{main}})$	chemical energy release at the end of the injection of the main pulse
CN	combustion noise	$R$	gas constant; correlation coefficient
CO	Carbon Monoxide	$R_{\text{corr}}$	adjusted correlation coefficient
$d$	nozzle hole diameter	$R_{\text{corr,best}}$	adjusted correlation coefficient of the best combinations
DI	Direct Injection	$R_{\text{exh}}$	gas constant of the exhaust gases
DoE	Design of Experiment	SOC	start of combustion
ECU	Electronic Control Unit	SOI	start of injection
EGR	Exhaust Gas Recirculation	$t$	time
EOI	end of injection	$t^+$	characteristic time
$\text{EOI}_{\text{main}}$	end of injection of the main pulse	$\tilde{t}$	dimensionless time
EVO	Exhaust Valve Opening	$T$	temperature
FSN	filter smoke number [0–10]	$T_{\text{b}}(\text{MFB95})$	temperature of the burned gases at MFB95 crank angle
GM	General Motors	THC	total unburned hydrocarbon
GMPT-E	General Motors PowerTrain-Europe	$T_{\text{n}}$	standard temperature
HRR	heat release rate	$u^2$	variance
ICEAL-PT	Internal Combustion Engine Advanced Laboratory at the Politecnico di Torino	$U$	expanded uncertainty
IMEP	Indicated Mean Effective Pressure	UEGO	Universal Exhaust Gas Oxygen sensor
IVC	intake valve closing	$u_{\text{EGR}}$	EGR valve duty-cycle signal
$k$	coverage factor	$U_{\text{f}}$	fuel velocity at nozzle exit
$m$	mass; coefficient of the spray model	WG	wastegate
$\dot{m}_{\text{a}}$	air mass flow rate	$x$	generic axial spray coordinate
$\dot{m}_{\text{f}}$	fuel mass flow rate	$x^+$	characteristic spray length
$m_{\text{PM}}$	net formed mass of particulate matter per cycle/cylinder	$\tilde{x}$	dimensionless distance
MFB5	crank angle at which 5% of the fuel mass fraction has burned	$x_{\text{SOC,main}}$	axial spray coordinate at the SOC of the main pulse
MFB50	crank angle at which 50% of the fuel mass fraction has burned	$x_{\text{u,ivc}}$	unburned air mass concentration at IVC
MFB70	crank angle at which 70% of the fuel mass fraction has burned	$x_{\text{u,evo}}$	unburned air mass concentration at EVO
MFB80	crank angle at which 80% of the fuel mass fraction has burned		
MFB95	crank angle at which 90% of the fuel mass fraction has burned		
$N$	engine rotational speed; mole number		
$N_{\text{cyl}}$	number of cylinders		
NEDC	New European Driving Cycle		
NO <sub>x</sub>	Nitrogen Oxides		
O <sub>2</sub>	Intake charge oxygen concentration		
OPA	opacity [0–100%]		
$p$	pressure		
$p_{\text{a}}$	ambient pressure		
$p_{\text{f}}$	injection pressure		
pil	pilot injection		
PM	particulate matter		
PMA	pilot-main-after injection strategy		
$p_{\text{n}}$	Standard pressure		

**Greek symbols**

$\alpha$	air-to-fuel ratio; spreading angle of the idealized spray model
$\alpha_{\text{st}}^{\text{u}}$	stoichiometric ambient-to-fuel ratio
$\Delta CA_{\text{comb}}$	combustion duration parameter
$\Delta CA_{\text{diff}}$	diffusive combustion duration parameter
$\Delta \text{MFB}_{70-95}$	difference between MFB95 and MFB70 parameters
$\phi$	equivalence ratio
$\phi_{\text{SOC,main}}$	equivalence ratio of the spray at SOC <sub>main</sub>
$\lambda$	relative air-to-fuel ratio
$\theta$	spreading angle of the spray
$\rho$	mass density
$\rho_{\text{a}}$	ambient density
$\rho_{\text{f}}$	fuel density
$\tau_{\text{char}}$	characteristic mixing time coefficient
$\tau_{\text{HL}}$	half-life parameter
$\tau_{\text{id}}$	ignition delay
$\tau_{\text{id,main}}$	ignition delay of the main pulse

the laser-sheet imaging technique, have led to a deeper insight into understanding of the combustion process and PM formation in DI diesel engines. On the basis of these results, Dec has introduced a novel conceptual scheme for diesel combustion, which is currently considered as the reference one in the literature [12]. According to

the Dec scheme, diesel combustion is basically a two-stage process, made up of a fuel-rich premixed phase ( $\phi = 2-4$ ), which leads to the formation of products of incomplete combustion (soot, CO, THC), and a stoichiometric diffusive phase located at the jet periphery, in which the oxidation of the previously formed products takes

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