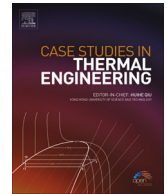




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Analytical approach for evaluation of thermo hydraulic performance of roughened solar air heater



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ABSTRACT

Mathematical modeling and simulations are seen as vital methodologies to predict the thermal performance optimization of thermal systems. Solar air heater roughened with 20° angled rib is simulated using an algorithm developed in MATLAB to predict the optimal set of design and operating parameters. Correlations developed using second order polynomial are used for simulations. In the entire range of flow rates, the thermal efficiency of the roughened solar air heater is higher as compared to smooth duct. In fixed value of solar insolation, thermal efficiency increases with the increase in mass flow rate while effective efficiency decreases. The effective efficiency of the system increases with an addition in the number of glass covers and width of the duct. Thermal and effective efficiency increases with the increase in solar insolation. An increase in velocity increases the convective heat transfer coefficient of air, which reduces the useful heat gain by increasing the top losses which in turn affects the increase in effective efficiency for the rise in velocity in the solar air heater. The effect of mass flow rate, the number of glass covers, heat flux, velocity and variation in width of duct on thermal and effective efficiencies of roughened solar air heater are presented in the form of plots in the present study.

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1. Introduction

A solar air heater is a thermal system which is used to convert solar energy into thermal energy. A wider application of solar air heater involves drying of agricultural and marine products, space heating and heating of buildings to maintain comfort in the winter season. Solar fish dryers are very useful for small fisherman groups. It has been noted that the performance efficiency of solar air heater is very low because of low convective heat transfer coefficient between absorber plate and flowing working fluid (air). The presence of a laminar viscous sub layer is the possible cause for low convective heat transfer coefficient. The resistance to heat transfer arises due to this laminar viscous sub layer is eliminated by providing artificial roughness on the underside of the absorber plate. Many researchers investigated the effect of various roughness geometries on heat transfer and friction characteristics in the solar air heater. The researchers have also developed mathematical algorithms as an analytical tool to simulate solar thermal systems and to optimize the thermal performance of solar air heater. The optimization technique helps to predict an optimized set of designs and operating parameters. Ahmad et.al. [1] experimentally investigated the effect of system and operating parameters, viz. geometry of

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Nomenclature		U_e	Edge loss coefficient, $W m^{-2} K^{-1}$.
D	Equivalent or hydraulic diameter of duct, mm.	<i>Dimensionless parameters</i>	
A_p	Surface area of the absorber plate, m^{-2} .	e/D	Relative roughness height.
C	Conversion factor.	f	Friction factor.
e	Rib height, mm.	f_r	Friction factor for rough surface.
F_0	Heat removal factor.	f_s	Friction factor for smooth surface.
F_p	Collector efficiency factor.	Nu	Nusselt number.
G	Mass velocity of air, $kg s^{-1} m^{-2}$.	Nu_r	Nusselt number of rough surfaces.
h	Heat transfer coefficient, $W m^{-2} K^{-1}$.	Nu_s	Nusselt number of smooth surfaces.
h_w	Convective heat transfer coefficient of wind, $W m^{-2} K^{-1}$.	Pr	Prandtl number.
W	Height of the duct, mm.	P/e	Relative roughness pitch.
I	Solar insolation, $W m^{-2}$.	Re	Reynolds number.
K	Thermal conductivity of air, $W m^{-1} K^{-1}$.	W/H	Duct aspect ratio.
K_i	Thermal conductivity of insulation, $W m^{-1} K^{-1}$.	I	Turbulence intensity,.
m	Mass flow rate, $kg s^{-1}$.	<i>Greek symbols</i>	
A_0	Cross section area of orifice, m^2 .	μ	Dynamic viscosity, $N s m^{-2}$.
W	Width of the duct, mm.	ρ	Density of air, $kg m^{-3}$.
ΔP_0	Pressure drop across orifice meter, $N m^{-2}$.	ρ_m	Density of manometer fluid, $kg m^{-3}$.
ΔP_d	Pressure drop across duct test section, $N m^{-2}$.	k	Turbulent kinetic energy, $m^2 s^{-2}$.
C_p	Specific Heat of air, $J kg^{-1} K^{-1}$.	β	Ratio of orifice diameter to pipe diameter.
L_1	Inlet length of duct, mm.	ν	Kinematic viscosity, $m^2 s^{-1}$.
L_2	Test length of the duct, mm.	θ	Tilt angle of manometer, degree.
L_3	Outlet length of duct, mm.	K	Thermal diffusivity, $m^2 s^{-1}$.
P	Pitch, mm.	α	Chamfer angle.
U	Mean airflow velocity in the duct, $m s^{-1}$.	ϵ_p	Emissance of plate.
C_d	Coefficient of discharge for orifice meter.	ϵ_g	Emissance of glass cover.
u	Air flow velocity in x direction, $m s^{-1}$.	η_{th}	Thermal efficiency.
v	Air flow velocity in y direction, $m s^{-1}$.	η_{eff}	Effective efficiency.
T	Air temperature, K.	η_{Tr}	Transmission efficiency.
Δh_0	Difference in levels of U-tube manometer, m.	η_m	Motor efficiency.
T_o	Outlet temperature of air, K.	η_f	Pump efficiency.
T_i	Inlet temperature of air, K.	$\tau\alpha$	Transmittance absorptance product of glass cover.
T_p	Mean temperature of absorber plate, K.	<i>Subscripts</i>	
Q_u	Useful heat gain, W.	THPP	Thermo hydraulic performance parameter.
T_p	Average plate temperature, K.	r	Roughened.
T_f	Average air temperature, K.	s	Smooth.
N	Number of glass covers.	CFD	Computational Fluid Dynamics.
L	Length of the test section.		
ΔT	Bulk mean temperature of flowing fluid, K.		
$\Delta T/I$	Temperature rise parameter, $m^2 KW^{-1}$.		
U_L	Overall heat loss coefficient, $W m^{-2} K^{-1}$.		
U_t	Top loss coefficient, $W m^{-2} K^{-1}$.		
U_b	Bottom loss coefficient, $W m^{-2} K^{-1}$.		

wire screen matrices, insolation, inlet temperatures and mass flow rates on thermohydraulic performance characteristics of packed bed solar air heaters. Their study reported that relatively higher enhancement in the thermohydraulic efficiency has been found corresponding to higher values of temperature rise parameter. They suggested that it would be advantageous to use packed bed solar air heater when higher grade energy is required even when the insolation is relatively low. The effect of roughness and operating parameters on the thermal as well as the hydraulic performance of roughened solar air heaters was discussed and the thermohydraulic performance of roughened solar air heaters was compared with that of conventional smooth solar air heaters by Gupta et. al. [2]. Their study found that the systems operating in a specified range of Reynolds number shows better thermohydraulic performance depending upon the insolation. Thermohydraulic investigations on a packed bed solar air heater having its duct packed with blackened wire screen matrices of different geometrical parameters (wire diameter and pitch) were carried out by Mittal et. al. [3]. The thermohydraulic performance of a solar air heater was evaluated using a mathematical model and they reported that packed bed solar air heater is thermohydraulically

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