Contents lists available at SciVerse ScienceDirect







journal homepage: www.elsevier.com/locate/engfracmech

# Flow and fracture behaviour of FV535 steel at different triaxialities, strain rates and temperatures

### B. Erice, F. Gálvez\*, D.A. Cendón, V. Sánchez-Gálvez

Departamento de Ciencia de Materiales, Universidad Politécnica de Madrid (UPM), Calle del Profesor Aranguren s/n, 28040 Madrid, Spain Research Centre on Safety and Durability of Structures and Materials (CISDEM), UPM-CSIC, Calle del Profesor Aranguren s/n, 28040 Madrid, Spain

#### ARTICLE INFO

Article history: Received 3 December 2010 Received in revised form 7 June 2011 Accepted 29 August 2011

Keywords: Strain rate effects Constitutive modelling Finite element analysis Steel

#### ABSTRACT

The new generation jet engines operate at highly demanding working conditions. Such conditions need very precise design which implies an exhaustive study of the engine materials and behaviour in their extreme working conditions. With this purpose, this work intends to describe a numerically-based calibration of the widely-used Johnson-Cook fracture model, as well as its validation through high temperature ballistic impact tests. To do so, a widely-used turbine casing material is studied. This material is the Firth Vickers 535 martensitic stainless steel. Quasi-static tensile tests at various temperatures in a universal testing machine, as well as dynamic tests in a Split Hopkinson Pressure Bar, are carried out at different triaxialities. Using ABAQUS/Standard and LS-DYNA numerical codes, experimental data are matched. This method allows the researcher to obtain critical data of equivalent plastic strain and triaxility, which allows for more precise calibration of the Johnson-Cook fracture model. Such enhancement allows study of the fracture behaviour of the material across its usage temperature range.

© 2011 Elsevier Ltd. All rights reserved.

#### 1. Introduction

Jet engine certification involves assuring the manufacturer that in the case of an accidental blade-off event inside the turbine, any spoiled component as a consequence of this event, must be contained by the casing. This certification needs to pass an experimental procedure. This procedure is a real scale containment test, in which one turbine blade is intentionally manipulated to fail. These kinds of experimental procedures present financial difficulties. Many resources are focussed on improving and minimising the costs of such tests, so much that a future objective is to minimise costs by performing numerical simulations of these containment tests. Besides economic considerations, technical ones must also be taken into account. The aerospace industry requires lightweight materials with high strength: in other words, a high strength to weight ratio. The material used in a turbine casing, as well as the afore-mentioned characteristics, must have a high temperature resistance.

One of the most common materials used for jet engine turbine casings is 9–12% high chromium martensitic stainless steel, which has excellent mechanical properties at relatively high temperatures and good corrosion resistance. The exact material analysed in this study is the Firth-Vickers FV535 stainless steel. Unfortunately, the steel is not one of the most lightweight of materials. Numerical simulations of containment tests could help to optimise the thickness of these casings in order to reduce weight causing a great weight saving and thus reducing cost. In order to simulate with fidelity the real behaviour of the materials involved in the containment tests complete material model characterisation is mandatory.

<sup>\*</sup> Corresponding author at: Departamento de Ciencia de Materiales, Universidad Politécnica de Madrid (UPM), Calle del Profesor Aranguren s/n, 28040 Madrid, Spain.

E-mail addresses: borjaerice@mater.upm.es (B. Erice), fgalvez@mater.upm.es (F. Gálvez).

Nomenclature	
ā	aquivalent Von Missos stress
A	equivalent von wisses success
R	material constant of Johnson-Cook constitutive relation
D n	material constant of Johnson-Cook constitutive relation
n C	material constant of Johnson-Cook constitutive relation
m	material constant of Johnson-Cook constitutive relation
Ē	equivalent or Von Misses plastic strain
ē*	dimensionless plastic strain rate
ėp Ėo	user defined strain rate
ien ien	alastic strain rate
$T^*$	homologous temperature
T <sub>r</sub>	room temperature
T <sub>m</sub>	melting temperature
B	Taylor-Quinney coefficient
r 0	density
$C_n$	specific heat
D	damage parameter or indicator
$\bar{e}_n^f$	equivalent plastic strain to fracture
$\sigma^{F}$	stress triaxiality
$\sigma_{H}$	hydrostatic stress
$D_1$	material constant of Johnson–Cook fracture criterion
$D_2$	material constant of Johnson–Cook fracture criterion
$D_3$	material constant of Johnson–Cook fracture criterion
$D_4$	material constant of Johnson–Cook fracture criterion
$D_5$	material constant of Johnson–Cook fracture criterion
r	axisymmetric specimen initial radius
R	axisymmetric specimen notch radius
d	axisymmetric specimen diameter
$d_0$	axisymmetric specimen initial diameter
$d_f$	axisymmetric specimen final or fracture diameter
Α	specimen cross section area
$A_0$	specimen initial cross section area
$A_{f}$	specimen final or fracture cross section area
$\varepsilon_i$	incident strain
Е <sub>r</sub>	reflected strain
$\varepsilon_t$	transmitted strain
$\sigma_s$	specimen engineering stress
F <sub>s</sub>	force applied by the Split Hopkinson Pressure Bar over the specimen
$E_b$	SHPB input and output bar elastic modulus
A <sub>b</sub>	SHPB IIIput and output dar cross section area
es C	specifient engineering stidill abstic wave propagation velocity incide SUDP input and system bar
	clastic wave propagation venocity mistice SHPD imput and output Dai
l <sub>S</sub>	

Numerical simulations with a real jet engine model are carried out at the Department of Materials Science at the UPM. The non-linear explicit numerical code chosen for such a purpose is LS-DYNA in its 971 version. For the correct simulation of the complete impact phenomena produced inside the engine, it is necessary to include a material model that reproduces the blade-off event in the most accurate way possible. Previous works [1,2] have shown that the Johnson–Cook material model [3], already implemented in the LS-DYNA numerical code, works reasonably well. This work is focused on obtaining a valid Johnson–Cook model for the material proposed.

The accumulation of plastic strain is the basis of the majority of the fracture criteria. The Johnson–Cook (JC) failure criterion is also based on the same principle. The standard procedure to obtain the Johnson–Cook fracture model is detailed in [3] and has been used by Clausen et al. [4] and Børvik et al. [5], among others. This procedure is based on obtaining an equivalent plastic strain fracture envelope as a function of the stress triaxiality, strain rate and temperature. To obtain the JC fracture criterion constants, extensive experimental testing was carried out. This included the following:

• Quasi-static tensile tests of axisymmetric smooth and notched specimens which provided different values of the stress triaxiality.

Download English Version:

## https://daneshyari.com/en/article/767463

Download Persian Version:

https://daneshyari.com/article/767463

Daneshyari.com