Contents lists available at ScienceDirect



Engineering Fracture Mechanics

journal homepage: www.elsevier.com/locate/engfracmech

Crack path prediction in rolled aluminum plates with fracture toughness orthotropy and experimental validation



Paul O. Judt*, Andreas Ricoeur, Günter Linek

Institute of Mechanics, University of Kassel, 34125 Kassel, Germany

ARTICLE INFO

Article history: Received 15 September 2014 Received in revised form 23 January 2015 Accepted 2 March 2015 Available online 14 March 2015

Keywords: Crack path prediction Fracture toughness orthotropy J-integral Mixed-mode Crack growth

ABSTRACT

The paper presents a numerical procedure for the accurate calculation of crack paths in plane structures. The *J*-integral is used to determine crack tip loading quantities such as stress intensity factors or the energy release rate. Crack paths are predicted applying a modified maximum energy release rate approach accounting for the fracture toughness orthotropy in rolled plates of aluminum alloy Al-7075-T651 where the anisotropy of elastic constants is negligible. Experiments with CT-specimens are carried out to determine the fracture toughnesses in and perpendicular to the rolling direction. The numerically predicted crack paths for differently shaped specimens are in good agreement with those obtained from experiments.

© 2015 Elsevier Ltd. All rights reserved.

1. Introduction

Rolled sheets of aluminum are known to exhibit a texture inherently giving rise to anisotropic material behavior. Besides the elastic properties, only slightly depending on the orientation, the fracture toughnesses in and perpendicular to the rolling direction differ by approximately 10–15%. Neglecting this feature, numerically predicted and experimentally observed crack paths agree qualitatively, however not quantitatively.

Several papers [31,32,2,1] focus on the calculation of crack tip loading quantities in orthotropic structures with stationary cracks, however not regarding crack growth or crack paths. Established numerical techniques for crack path prediction as elastic or elastic–plastic boundary value problem are often based on the FE-method. Convenient tools for calculating crack paths are e.g. iterative procedures in connection with intelligent remeshing algorithms and integrated post processors. The accurateness of the predicted crack paths goes along with the precise calculation of crack tip loading quantities, e.g. the J_k -integral, or in the linear elastic fracture mechanics (LEFM) the energy release rate (ERR) *G* or stress intensity factors (SIF). These quantities, which are depending on the applied loads and the geometrical configuration, are provided numerically by post processing procedures such as the *J*-integral [15,43], the crack tip element (CTE) method [22,5], the interaction integral (I-integral) technique [51,55] or the modified crack closure integral (MCCI) method [44]. Here, path-independent integrals are beneficial as, in contrast to the CTE or MCCI method, no special requirements of the FE-meshes have to be considered and numerical input data may be taken far from the crack tip.

The *J*-integral is based on Eshelby's general theory on configurational forces acting at singularities and inclusions [18] and was introduced by Cherepanov [15] and Rice [43] who applied the formulation of this path-independent integral to strain concentration problems. The two-dimensional J_k -integral vector, introduced by Budiansky and Rice [9], is composed of the coordinate $J_1 = J$ and J_2 and provides an extended path-independent formulation of the classical *J*-integral for arbitrary

E-mail addresses: judt@uni-kassel.de (P.O. Judt), ricoeur@uni-kassel.de (A. Ricoeur), linek@uni-kassel.de (G. Linek).

^{*} Corresponding author. Tel.: +49 561 804 2852; fax: +49 561 804 2720.

Nomenclature		
ā	maan	

ā	mean crack length	
a_0	initial crack length	
Δa	increment of crack advance	
da/dN	crack growth rate	
a_{ij}	compliance tensor	
В	specimen thickness	
С	crack growth rate coefficient	
C_{ijkl}	elasticity tensor	
E J	Young's modulus	
\underline{e}_i	local coordinates	
e _i	global coordinates	
e_0	geometric parameter	
J _{ij}	complex angular function	
G	energy release rate	
G_c	ratio of operative release rate and crack registance	
G _R	threshold parameter for fatigue grack growth	
G _{th}	complex angular function	
Бі И	energy quantity indicating crack deflection	
I.	<i>L</i> -integral vector	
J_k ΛK	stress intensity factor range	
K,	mode I stress intensity factor	
$K_{\rm H}$	mode II stress intensity factor	
Kic	fracture toughness	
$K_{\rm I}^{\rm max}$	maximum stress intensity factor of pulsation load	
K _{Ith}	threshold value for fatigue crack growth	
m	crack growth rate exponent	
n _i	normal vector of the integration contour	
P _o	load value	
Q_{ki}	energy momentum tensor	
r	radius	
s _k	complex constants	
и	strain energy density	
u _i	displacement vector	
Δu_i	jump of the displacements across the crack faces	
W	geometric parameter	
ΔW^{c}	work required for crack closure	
Z_k	crack growth direction	
Greek let		
α	global crack deflection angle	
β	local crack deflection angle	
o _{ij}	infinitesimal distance	
e	strain tonsor	
c _{ij}	radial coordinate	
φ	integration contour	
I V	Poisson's ratio	
л	total notential energy	
	mixed-mode ratio	
φ σ::	stress tensor	
γ	ratio of orthotropic fracture toughness	
<i>.</i> .		
Special symbols		
n{}	real part of complex quantity in brackets	
J {}	imaginary part of complex quantity in brackets	
I	normal crack opening mode	

- plane shear crack opening mode specimen shapes Π
- A, B

Download English Version:

https://daneshyari.com/en/article/770249

Download Persian Version:

https://daneshyari.com/article/770249

Daneshyari.com