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## Application of hydrogen influenced cohesive laws in the prediction of hydrogen induced stress cracking in 25%Cr duplex stainless steel

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#### Abstract

Cohesive zone finite element modeling is applied in the simulation of hydrogen induced stress cracking in 25% Cr duplex stainless steel. Hydrogen influence is implemented in linear and polynomial cohesive laws. Suitability of the laws in prediction of hydrogen induced stress cracking is investigated by applying models of U and V-notched tensile specimens representing a 25% Cr duplex stainless steel component submerged in sea water under cathodic protection (CP). Fracture prediction is performed by a three step procedure; elastic plastic stress analysis, stress assisted hydrogen diffusion and cohesive stress analysis. Local cohesive stress fields as well as the time to fracture initiation are investigated as a function of the shape of the traction separation laws and the element size for three levels of tensile stress. Simulated results are also compared with results from laboratory tensile tests and discussed with respect to the suitability of describing fracture initiation and fracture mechanism of the steel. The results show that the polynomial law and a mesh size of 0.5  $\mu$ m gives the most accurate description of the local cohesive stress field. The simulated time to fracture is closest to laboratory test results for stresses of 0.85–0.9 times the yield strength.

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#### 1. Introduction

A challenging problem in the framework of finite element analysis is the prediction of failure in materials and structures. In later years the cohesive zone modeling (CZM) technique has become greatly facilitated and

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### Nomenclature

- bcc body centred cubic crystal lographic structure
- CP cathodic protection
- CZM cohesive zone modeling
- FE finite element
- HEDE hydrogen enhanced decohesion
- HELP hydrogen enhanced local plasticity
- HISC hydrogen induced stress cracking
- SCE saturated calomel electrode
- TSL traction separation law
- $C, C_E, C_{Ni}, c_0, c_s$  hydrogen concentration: general, average in FE element, in nodes, in bulk, sub-surface *D* diffusion coefficient
- *E* Young's modulus
- $\Delta g_h^0$  Gibbs free energy difference
- J hydrogen flux
- k<sub>IH</sub> local hydrogen induced stress intensity/fracture toughness
- $K_{\rm IC}$  limit stress intensity

 $K_{I_{th}}, K_{HISC}$  threshold stress intensity: general, HISC-induced

*p* hydrostatic stress

- R gas constant
- s solubility
- t time
- $T, T^{Z}$  temperature, absolute temperature
- $V_{\rm H}$  partial molar volume of hydrogen in iron
- α ferrite
- $\alpha'', \beta'$  fitting parameters

 $\delta, \delta_1, \delta_N, \delta_T$  separation of cohesive element: general, at critical stress of linear law, normal, transverse,

- $\delta_c, \delta_M$  critical separation in normal direction, maximum value for transverse separation
- $\Delta$  element mesh length
- $\phi$  normalized hydrogen concentration: in stressed state, in unstressed state  $\gamma$  austenite
- $\gamma(0), \gamma(\theta)$  surface energy: without hydrogen influence, with hydrogen influence
- $\Gamma, \Gamma_{c}, \Gamma_{HISC}$  cohesive energy: general, critical, HISC related
- $\kappa_{\rm p}$  stress factor in diffusion
- v Poisson's ratio
- $\sigma_{\rm v}$  yield stress

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\sigma, \sigma(\delta), \sigma_{\rm N}, \sigma_{\rm T}, \sigma_{\rm M} cohesive stress, general, normal, transverse, maximum value for transverse stress
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 $\sigma_{\rm c},\sigma_{\rm c}(0),\sigma_{\rm c}(\theta)$  critical cohesive stress: general, without hydrogen influence, with hydrogen influence

 $\theta$  hydrogen coverage

gained renewed interest in the field of fracture modeling. Fracture takes place at an interface of cohesive zone elements embedded in a finite element model; no continuum elements are damaged in a cohesive model. In this respect the method is effective in fracture modeling of large geometries. The cohesive elements can be pictured as two faces separated by a thickness, which is close to zero. The relative motion of the top and bottom faces in the thickness direction represents opening or closing of the interface. The relevant constitutive "material" response is a traction separation description; an evaluation which gives the amount of energy required to create new surfaces. A traction separation law (TSL) is a function described by the cohesive stress ( $\sigma$ ) and separation ( $\delta$ ). The area below the curve represents the cohesive energy,  $\Gamma_c$ . There are a variety of shapes of the TSL proposed by different authors. Two TSL's will be applied in the present paper, see Fig. 1. Nguyen and

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