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#### Note

# Elastic *T*-stress solutions for flat elliptical cracks under tension and bending

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#### Abstract

Exact solutions for elastic T-stress of a flat elliptical crack in an infinite body under tension and bending are obtained in this paper. Many papers have been devoted to the problems for elliptical cracks in an elastic medium, but all their attention has been concentrated on the determination of stress intensity factors. In the current paper, elastic T-stress solutions are derived by means of the potential method and a specific collection of harmonic functions. The formulas of the elastic T-stress for a penny-shaped crack [Wang X. Elastic T-stress solutions for penny-shaped cracks under tension and bending. Engng Fract Mech 2004;71:2283–98] follow from the present results as a special case. It is obtained that under tension loading, the elastic T-stress is always compressive along the elliptical crack front. In both tension and bending cases, T-stress essentially depends on the Poisson's ratio of the material, a parametric angle and semi-axes of the ellipse. © 2007 Elsevier Ltd. All rights reserved.

Keywords: Elastic T-stress; Constraint effects; Flat elliptical crack; Potential method; Stress intensity factors

#### 1. Introduction

Consider an isotropic linear elastic body which contains a three-dimensional crack under symmetric loading with respect to crack plane. The basic terms in a series expansion of the stress field near the crack front can be described as [1,2]:

$$\sigma_{nn} = \frac{K_I}{\sqrt{2\pi r}} \cos\frac{\alpha}{2} \left( 1 - \sin\frac{\alpha}{2} \sin\frac{3\alpha}{2} \right) + T, \quad \sigma_{zz} = \frac{K_I}{\sqrt{2\pi r}} \cos\frac{\alpha}{2} \left( 1 + \sin\frac{\alpha}{2} \sin\frac{3\alpha}{2} \right), \tag{1a}$$

$$\sigma_{tt} = \frac{K_I}{\sqrt{2\pi r}} 2\nu \cos \frac{\alpha}{2} + E\varepsilon_{tt} + \nu T, \quad \sigma_{nz} = \frac{K_I}{\sqrt{2\pi r}} \sin \frac{\alpha}{2} \cos \frac{\alpha}{2} \cos \frac{3\alpha}{2}, \quad \sigma_{zt} = \sigma_{nt} = 0,$$
 (1b)

where (n, t, z) is a local orthogonal coordinate system, which is connected to the crack front point (a local coordinate system formed by the plane normal to the crack front and the plane tangential to the crack front

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#### Nomenclature

a, bsemi-axes of the elliptical crack mode I stress intensity factor  $K_{\rm I}$ Poisson's ratio of the material shear modulus of the material μ (n,t,z)local orthogonal coordinate system local polar coordinates  $r, \alpha$ Tmagnitude of elastic T-stress  $(\xi, \eta, \zeta)$ ellipsoidal coordinates remote tension loading  $\sigma_0$ remote bending loads  $p_{1}, q_{1}$ parametric angle components of the normal vector in the crack plane  $n_x, n_y$ special integrals  $J_{ii}$ K(k), E(k) full elliptical integrals of the first and second kind magnitude of normalized elastic T-stress  $t(\varphi)$ 

point s); r and  $\alpha$  are the local polar coordinates (see Fig. 1); v is the Poisson's ratio and E is the Young's modulus;  $K_I$  is the mode I stress intensity factor. The symbol T in Eqs. (1a) and (1b) designates the elastic T-stress, corresponding to a tensile/compressive stress acting parallel to the crack plane.

The elastic T-stress is an important parameter, which describes stress states near the crack tip. As it was demonstrated in [3–5], the size and shape of the plastic zone of the plane strain crack-tip and the crack tip constraint depend on sign and magnitude of the T-stress. The T-stress, in combination with the stress intensity factors (SIFs), ensures a two-parameter characterization of linear elastic crack tip fields [6–8]. Such two-parameter approach in linear elastic fracture mechanics is becoming more and more recognized [9,10]. The influence of T-stress on the constraint of interface cracks was investigated in [11].

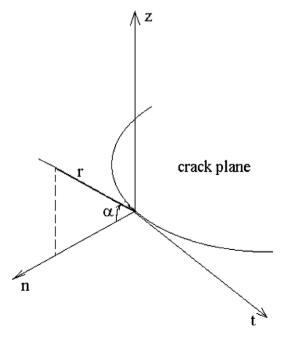


Fig. 1. Local coordinate system along the crack flat.

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