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# A case study of a hydride container performance applying non dimensional parameters

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## ABSTRACT

Many efforts have been done so far to understand sorption dynamics of hydride containers for hydrogen storage. Particularly, there are many articles in literature where experimental results for different hydride systems and container set-ups were successfully simulated using basically the same group of models. This fact is the base of a previous work where we defined a series of non dimensional parameters which may be used to estimate absorption time of hydride containers.

In this work we compare estimated absorption times with experimental outcomes for a prototype hydride container. We performed non dimensional analysis of our finned container prototype at two scales, i.e.: overall or macroscopic container scale and pore or microscopic scale. We discuss about this simplified model approach that allows estimating, with few parameters, the reaction time of a complex-geometry prototype.

The prototype container was designed according to the results of a numerical optimization that maximized the amount of hydrogen absorbed for a 3 min charging period. Experimental results indicate good agreement between estimated and experimental absorption time, making the non dimensional method a useful tool at preliminary stages of hydride container design.

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## Introduction

Hydrogen as energy carrier has some technical limitations that need to be addressed to promote its massive use. One major issue is hydrogen storage, owing to its low density and high chemical reactivity. Storage by means of hydrides is a feasible option, especially when considering stationary

applications. Hydride systems might be less expensive than high pressure or cryogenic storage that need a large amount of energy for compressing or liquefying the hydrogen. This results in hydride systems having lower operational cost [1].

Hydride containers are complex systems. Sorption reactions involve considerable reaction heat while the effective thermal conductivity of hydride powder is quite low. This causes important temperature changes that limit the sorption

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Nomenclature			
1D	one dimensional	$\tau$	characteristic decay time, s
$\hat{C}$	pressure drop parameter, bar	T	temperature, K
$C_{sg}$	hydride capacity, kg H <sub>2</sub> /kg hydride, –	V	volume, m <sup>3</sup>
$\Delta H$	molar enthalpy of reaction, J mol <sup>-1</sup>		
E	activation energy, J mol <sup>-1</sup>	Subindex	
$\epsilon$	hydride porosity, –	0	fitting parameter
F	heat conductive material fraction, –	1	fitting parameter
k	thermal conductivity, W m <sup>-1</sup> K <sup>-1</sup>	90%	at 90% of total capacity
$\hat{k}$	kinetics constant, s <sup>-1</sup>	abs	absorption
K	pressure drop coefficient	cont	container
L	characteristic length, m	d	heat conductive material
m	mass, kg	des	desired (reaction time)
$\dot{m}$	mass flow rate, kg s <sup>-1</sup>	e	equilibrium
n	pressure drop exponent, –	eff	effective
M	molecular weight, kg mol <sup>-1</sup>	ext	external
NDC	non dimensional conductance, –	g	hydrogen gas
NDFT	non dimensional fill time, –	kin	kinetics
NDK	non dimensional kinetics, –	line	hydrogen line
P	pressure, bar	max	maximum
R	ideal gas constant, 8.315 J mol <sup>-1</sup> K <sup>-1</sup>	MH	metal hydride and interstitial hydrogen mixture
SS	stainless steel	pore	pore
$\delta$	density, kg m <sup>-3</sup>	s	hydride or solid
t	time, s	supply	hydrogen supply to hydride container
		tank	hydrogen tank

reaction. When analyzing hydride containers both thermal and chemical issues have to be assessed simultaneously obtaining temperature and hydrogen concentration profiles, usually by numerical tools ([2–5] also see Table 1 in the work of Melnichuk et al. [6]). These profiles depend on the absorbing material, the container geometry and conductivity, pressure and temperature conditions and hydrogen flow through the metal hydride bulk [7]. Furthermore, in some cases the reaction kinetics of the absorbing material cannot be disregarded.

In addition to these phenomena, which were modeled and predicted by many authors, we observe an appreciable degree of uncertainty in some parameters such as porosity and thermal conductivity of the metal hydride. Both parameters also vary during sorption reaction, for reasons such as the volume change of the particles during hydration [8]. According to sensitivity analysis, thermal conductivity of the hydride could have a significant effect on the global reaction time [9].

Therefore, considering the complexity of the physical system and the uncertainties introduced by some parameters, a simplified model providing an estimated reaction time, could be useful and even desirable in comparison to more complex models.

In this work we analyze the reaction time of a prototype hydride container using non dimensional parameters that were presented in a previous work [6]. The objective of this work is to compare the estimated absorption time obtained by non dimensional analysis with experimental results, and to certain extent to validate these theoretical predictions. The container was designed based on the results of a numerical optimization that maximized the amount of hydrogen absorbed for a 3 min charging period [10]. Therefore it is expected that most of the absorption would occur during that time.

## Non dimensional parameter analysis

### Outline

In a previous work we developed a series of non dimensional parameters that provide an approximate measure of the relative importance of the different factors on the absorption process of a hydride container [6]. It is worth noting the same concepts can easily be applied to desorption dynamics. This work was based on the non dimensional conductance (NDC) defined by Visaria et al. [9], which can be regarded as the approximate ratio between the thermal evolution time and the desired charging time.

**Table 1 – Parameters for non dimensional calculations.**

Parameter	Value	Reference
$T_{max}$ (°C)	60.9 ( $P_g = 30$ bar)	This work
$\Delta H_{Abs}$ (J mol <sup>-1</sup> )	27,020	This work
$C_{sg}$ (kg <sub>g</sub> /kg <sub>MH</sub> )	$1.15 \times 10^{-2}$	This work
$k_d$ (W m <sup>-1</sup> K <sup>-1</sup> )	138	[12]
$\rho_s$ (kg m <sup>-3</sup> )	$8.3 \times 10^3$	[13]
$\epsilon$	0.5	[13]
$\kappa_{abs}$ (s <sup>-1</sup> )	59.2	[14]
$E_{abs}$ (J mol <sup>-1</sup> )	21,170	[14]
$P_e$ (bar)	3.4 ( $T_{ext} = 0$ °C)	This work
	7.7 ( $T_{ext} = 20$ °C)	This work

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