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Maximum power cold start mode of proton exchange membrane fuel cell

Qing Du ^a, Bin Jia ^{a,b}, Yueqi Luo ^a, Jixin Chen ^c, Yibo Zhou ^a, Kui Jiao ^{a,*}^a State Key Laboratory of Engines, Tianjin University, 92 Weijin Road, Tianjin 300072, China^b Internal Combustion Research Institute, Tianjin University, 92 Weijin Road, Tianjin 300072, China^c Department of Mechanical Engineering, University of Michigan, 2350 Hayward St., Ann Arbor, MI 48109, USA

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ABSTRACT

Successful and fast cold start is important for proton exchange membrane (PEM) fuel cell in vehicular applications in addition to the desired maximum power in any case. In this study, the maximum power cold start mode is investigated in details and compared with other cold start modes based on a multiphase stack model. It is found that for the maximum power cold start mode, the current density is generally kept at high levels, and the performance improvement caused by the membrane hydration and temperature increment may not be observable. Therefore, before the melting point, the performance drops continuously. The maximum power cold start mode could better balance the heat generation and ice formation, leading to improved cold start survivability than that in the constant voltage and constant current modes, with a fast start-up generally guaranteed. Once the survivability can be ensured, the initial water content needs to be higher for fast cold start, suggesting that over purging should be avoided. The maximum power mode is suggested to be optimal for PEM fuel cell cold start based on the modeling results.

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Introduction

Proton exchange membrane (PEM) fuel cell has been regarded as an ideal power source for vehicular applications due to its significant advantages, i.e., high efficiency, low emission, silence and simplicity [1]. The low operating temperature of PEM fuel cell facilitates the fast start-up/shutdown necessary for powering a vehicle but meanwhile introduces challenges for water management. Although certain amount of water is critical to maintain the membrane hydrated and thus a high ionic conductivity, too much water can hinder the reactant

transport from the channel toward the catalyst site and result in increased mass transport losses. Therefore an optimum water amount/distribution is generally pursued by control strategy [2] and material innovation [3] to achieve improved fuel cell performance, with phase-change being carefully considered. Such a problem becomes even more complicated when the realistic application of a PEM fuel cell comes into people's attention. Due to the environmental temperature, it is necessary to operate a PEM fuel cell in subzero conditions. The formation of ice during phase-change can block the reaction sites, reduce the performance, accelerate the degradation and lead to the failure of cold start. Thorough

* Corresponding author. Tel.: +86 22 27404460; fax: +86 22 27383362.

E-mail address: kjiao@tju.edu.cn (K. Jiao).

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Nomenclature		Subscripts and superscripts	
a	water activity	a	anode
A	cell geometric area, m^2	act	activation
ASR	area specific resistance, $\Omega\text{ cm}^2$	BP	bipolar plate
c	mole concentration, mol m^{-3}	c	cathode, capillary
C_p	specific heat, $\text{J kg}^{-1}\text{ K}^{-1}$	channel	flow channel
D	mass diffusivity, $\text{m}^2\text{ s}^{-1}$	CL	catalyst layer
EW	equivalent weight of membrane, 1.1 kg mol^{-1}	conc	concentration
F	Faraday's constant, $96,487\text{ C mol}^{-1}$	eff	effective
h	surrounding heat transfer coefficient, $\text{W m}^{-2}\text{ K}^{-1}$	env	environment
I	current density, A cm^{-2}	eq	equilibrium
j	exchange current density, A cm^{-2}	f	frozen
k	thermal conductivity, $\text{W m}^{-1}\text{ K}^{-1}$	fl	fluid phase
M	molecular weight, kg mol^{-1}	fmw	frozen membrane water
p	pressure, Pa	GDL	gas diffusion layer
\dot{Q}	heat transfer rate, W	H_2	hydrogen
R	universal gas constant, $\text{J mol}^{-1}\text{ K}^{-1}$	H_2O	water
s	volume fraction	i	the i th components
S	source terms	in	inlet
t	time, s	init	initial condition
Δt	time step size, s	lq	liquid water
T	temperature, K	mem	membrane
T^0	standard temperature, 298 K	N	cell number
V	voltage	nf	non-frozen
Greek letters		nmw	non-frozen membrane water
α	transfer coefficient	O_2	oxygen
ε	porosity	out	outlet, output
ζ	water transfer rate, s^{-1}	ref	reference
κ	electric conductivity, S m^{-1}	sat	saturation
λ	water content in ionomer	sl	solid phase
ξ	stoichiometry ratio	T	energy (for source term)
ρ	density, kg m^{-3}	vp	water vapour
ω	volume fraction of ionomer in catalyst layer	wall	surrounding wall of the stack
δ	thickness, m		

understanding of cold start characteristics and developing associated operating strategies are thus of top importance for state-of-art research.

In order to understand the cold start behaviors of PEM fuel cell, two categories of previous studies have been conducted. One approach is to optimize the structure and material design of PEM fuel cell so that the system can endure subzero conditions with more tolerance [4–9]. Hirakata et al. [10] studied the effect of pore diameter of gas diffusion layer (GDL) on cold start behavior and cell performance. They found that a GDL with smaller pore diameter exhibited favorable anti-flooding performance. Santamaria et al. [11] compared the cold start performance between parallel and interdigitated flow field PEM fuel cells at various current densities, concluding that an interdigitated flow field may provide better performance under less extreme cold start conditions than parallel flow fields. Ko et al. [12] presents a theoretical study on the effects of ionomer fraction and weight ratio of Pt to carbon support in the cathode catalyst layer (CL). Their calculations confirm that these two design parameters provide control of the ice storage capacity and water absorption potential of the cathode CL,

and consequently demonstrate a substantial influence on the PEM fuel cell cold start behavior. On the other hand, a few studies focused on modification of the operating conditions to achieve a successful cold start [13–20]. Jiao et al. [21] developed a three-dimensional multiphase model to simulate various operating and initial conditions as to their influences on cold start, which include cell voltage, initial water content and distribution, anode inlet relative humidity (RH), surrounding heat transfer coefficient, and start-up temperature. Experimental investigation has been also attempted through the simultaneous measurements of current and temperature distributions during the cold start [22].

A consensus from these prior studies is that start-up mode [13–18], initial temperature [23,24] and initial water content [25–30] in membrane and CL are three essential conditions which determine the failure/success of cold start. Particularly for the start-up mode, the constant current start-up mode has been widely used in experimental [31–33] and modeling studies [34–38] of PEM fuel cell cold start. For example, Jiang et al. [39] modeled the current ramping method and found that this method is beneficial for cold start due to the

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