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Gas diffusion layer deformation and its effect on the transport characteristics and performance of proton exchange membrane fuel cell



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ABSTRACT

Cell/stack assembly force can strongly affect the transport characteristics and performance of a proton exchange membrane fuel cell (PEMFC) through causing the structural deformation. In this study, a mathematical model has been developed to investigate the effect of the assembly force for different gas diffusion layers (GDL) and membranes. The results indicate that the predominant deformation of the cell structure occurs in the porous GDL due to its weak mechanical strength. Thicker GDLs result into lower water content in the GDL structure, and can sustain a larger assembly force without the risk of "electrode flooding"; while thinner GDLs have higher water content, can maintain the hydration required for the membrane, and yield a better cell performance with less sensitivity to the variations in the assembly force. Thinner membranes yield better cell performance, but the cell performance is more sensitive to the changes in the assembly force. A combination of thin GDL and membrane is beneficial for better cell performance with reasonable sensitivity to the assembly force. For thinner GDLs, an optimal assembly force exists beyond which the cell performance is reduced; and practical cell assembly force will limit the GDL thickness.

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1. Introduction

Proton exchange membrane fuel cell (PEMFC) has been widely considered as one of the most promising clean power sources because of its capability for zero-emission operation with high efficiency and power density. Over the past several decades, significant progress has been made in the drive towards commercialization [1]. Gas diffusion layer (GDL), a key component of PEMFC required for reactant supply to the catalyst layer (CL), product water removal and collection/ transport of electron, experiences significant deformation under the cell/stack assembly force. GDL deformation changes its structural characteristics, including its thickness and porosity, which in turns change the transport properties such as permeability, effective diffusivity and electrical conductivity, negatively impacting the transport process for reactant, water and charged species, consequently the efficiency and power density.

The effect of the cell/stack assembly force on the GDL in PEMFC has been investigated with various degrees of complexities. Experimental studies have been performed, for example, Lee et al. [2] showed that each type of GDL has a

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Nomenclature		ξ	stoichiometry ratio
a	wateractivity	ρ	density, kg m ⁻³
Δ	coll geometric area m^2	σ	surface tension, N m^{-1}
C C	molar concentration, mol m^{-3}	σ	₀ Assembly force, uniformly distributed, MPa
C	specific heat $1 ka^{-1} K^{-1}$	φ	electrical potential, V
Cp d	poro diamator m	ω	volume fraction of ionomer in catalyst layer
u D	pore diameter, in mass diffusivity $m^2 c^{-1}$	τ	shear stress, Pa
D F	Noung's modulus. Pa	δ	thickness, m
EW	equivalent weight of membrane, kg kmol $^{-1}$	ϕ	electronic potential or volume fraction
F	interfacial drag coefficient	Subscripts and superscripts	
F	faraday's constant, C mol $^{-1}$	a	anode
G	shear elastic modulus, Pa	BP	bipolar plate
Н	latent heat, J kg ⁻¹ , surrounding heat transfer	с	cathode
	coefficient, W m ⁻² K ⁻¹	cell	cell characteristic
Ι	current density, A cm ⁻²	CL	catalyst layer
J	reaction rate, $A m^{-3}$	Cond	condensation
jo	volumetric exchange current density, A m^{-3}	d	dissolved water
k	thermal conductivity, W $m^{-1} K^{-1}$	eff	effective
К	permeability, m ²	ele	electronic
'n	mass flow rate, kg s ⁻¹	EOD	electro-osmotic drag
М	molecular weight, kg kmol $^{-1}$	equil	equilibrium
n _d	electro-osmotic drag coefficient (H ₂ O per H ⁺)	evap	evaporation
р	pressure, Pa	fl	fluid phase
Ċ	heat transfer rate, W	g	gas phase
R	universal gas constant, J mol $^{-1}$ K $^{-1}$	GDL	gas diffusion layer
RH	relative humidity	H_2	hydrogen
S	volume fraction	i, j	the ith and jth components
S	source terms or entropy, J $ m kmol^{-1}$ $ m K^{-1}$	in	inlet
Т	temperature, K	ion	ionic
To	volume averaged cell temperature, K	1	liquid water
ù	velocity, m s $^{-1}$	m	mass (for source term)
V	electrical potential, V	mem	membrane
Х	mole fraction	O ₂	oxygen
Y	mass fraction	out	outlet
Greeb letters		ref	reference state
α	transfer coefficient	rev	reversible
v v	water phase change rate s^{-1}	Sat	saturation
I E	porosity or strain tensor	sl	solid phase
č	water transfer rate, s^{-1}	surr	surroundings
, n	over potential. V	Т	energy (for source term)
θ	contact angle, o	u	momentum (for source term)
к	electrical conductivity, S m^{-1}	v	water vapour
λ	water content in ionomer or lame constant	d-v	dissolved water to vapour
μ	poisson ration or dynamic viscosity, kg m^{-1} s ⁻¹	v-1	vapour to water liquid (vice versa)
1	1		

unique mechanical structure and property, hence a different optimal compression or assembly force. Ge et al. [3] designed a special test fixture to directly measure a range of compression ratio and studied the effect of the GDL compression and deformation on the PEMFC performance.

However, it is difficult to measure experimentally the changes in the physical properties caused by the assembly force. Therefore, numerical method has been frequently used to investigate the compression effect. In a half-cell model by Chu et al. [4], four different functions of position were chosen to describe the porosity variations in the in-plane direction of the GDL. A sine wave porosity distribution was considered by

Roshandel et al. [5] when assembly force was applied, although a constant permeability was still used in their study. Some studies have focused on the effect of assembly force on the temperature distribution and the contact resistance [6–11], while some others investigated the transport properties and performance of PEMFC under the assembly force [12,13]. Su et al. [14] focused on the impact on the gas transport in the GDL material for three different configurations. Lai et al. [15] studied the effect of GDL intrusion into the flow channel on the transport properties of PEMFC by using 2-dimensional finite element method. Xing et al. [16] used the simultaneous perturbation stochastic algorithm method to

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