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## H<sub>2</sub> effects on diesel combustion and emissions with an LPL-EGR system

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### ABSTRACT

In this study, we examined H<sub>2</sub> effects on the combustion and emissions of a diesel engine with low-pressure loop (LPL) exhaust gas recirculation (EGR). We converted a 2.2-L four-cylinder direct-injection diesel engine satisfying Euro5 for H<sub>2</sub> supply. An LPL-EGR system replaced the high-pressure loop (HPL) EGR system. For all tests, the brake mean effective pressure (BMEP) was kept at 4 bar and the EGR ratio was varied from 9 to 42%. The H<sub>2</sub> energy percentage was varied from 0 to 7.4% independently to evaluate the H<sub>2</sub> effects and EGR effects separately. The heat release rate was calculated from the measured cylinder pressure. We found that substitution of H<sub>2</sub> for diesel fuel made the premixed burn fraction larger, and reduced the nitrous oxide (NO<sub>x</sub>) and particulate matter (PM) emissions simultaneously. For example, the NO<sub>x</sub> emissions were reduced by 36% for an EGR of 42% and an H<sub>2</sub> percentage of 7.4%. PM emissions were reduced by 18% for an EGR of 35% and an H<sub>2</sub> percentage of 7.4% compared with diesel fuel only cases.

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## 1. Introduction

Due to stricter regulations and concerns over global warming and human health problems, many researchers have focused on the development of various eco-friendly technologies to reduce CO<sub>2</sub>, particulate matter (PM), and nitrous oxide (NO<sub>x</sub>) emissions from vehicles. Recently, there has been greater interest among consumers for diesel vehicles since their lower pumping losses and higher compression ratios provide better fuel efficiency. However, due to their lean operation conditions and diffusion combustion, diesel vehicles emit more NO<sub>x</sub> and PM than gasoline vehicles.

Many studies have attempted to reduce NO<sub>x</sub> and PM emissions. Several technologies are available to reduce PM and meet current regulations, including diesel particulate filters (DPFs), catalyzed DPFs (CDPFs), and diesel oxidation catalysts (DOCs). Lean NO<sub>x</sub> traps (LNTs), hydrocarbon selective catalytic reduction (HC-SCR), and urea-SCR have been developed to

reduce NO<sub>x</sub>. To satisfy Euro6 legislation, heavy duty diesel vehicles use urea-SCR; LNTs are used on light duty diesel vehicles. These after-treatment technologies efficiently reduce PM and NO<sub>x</sub> emissions; however, they significantly increase the cost of the vehicle due to equipment expenses.

Unlike after-treatment technologies that reduce PM and NO<sub>x</sub> in the exhaust pipe after the combustion process, various advanced combustion technologies and pre-treatment technologies have been developed to reduce PM and NO<sub>x</sub> emissions without supplementary equipment such as DPFs, LNTs, or SCRs. Exhaust gas recirculation (EGR) is one of the pre-treatment technologies for reducing NO<sub>x</sub>. EGR lowers the temperature of the cylinder, taking advantage of the difference in the specific heats of the exhaust emissions and fresh air [1].

Advanced combustion technologies have been developed to reduce PM and NO<sub>x</sub> during the combustion process in a cylinder. A representative of advanced combustion technologies is homogeneous charge compression ignition (HCCI).

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### Nomenclature

EGR:	exhaust gas recirculation	DOC:	diesel oxidation catalyst
HPL:	high pressure loop	sLPM:	standard liters per minute
IMEP:	indicated mean effective pressure	BMEP:	brake mean effective pressure
LPL:	low pressure loop	FMEP:	friction mean effective pressure
HCCI:	homogeneous charge compression ignition	CA:	crank angle
LTC:	low temperature combustion	DPF:	diesel particulate filter
ECU:	engine control unit	LNT:	lean NOx trap
H <sub>2</sub> :	hydrogen	SCR:	selective catalytic reduction
O <sub>2</sub> :	oxygen	TDC:	top dead center
NOx:	nitrogen oxide	ATDC:	after top dead center
PM:	particulate matter	MB:	mass burn fraction
		MB10:	10% mass burn fraction
		$\theta_{MB10}$ :	crank angle of MB10

There is a trade-off between PM and NOx emissions for conventional diesel engines. However, HCCI can reduce PM and NOx simultaneously because the air–fuel mixture is homogeneous, and the combustion temperature is lower than that of conventional diesel engines [2,3]. To realize low-temperature combustion (LTC), such as HCCI, various technologies such as PREDIC, UNIBUS, and MK have been developed [4–6]. However, serious problems remain for HCCI, including combustion phasing and limited operating range [7,8]. First, HCCI cannot control the start of combustion in the traditional manner, such as by initiating fuel injection or firing a spark plug, because the chemical properties of the reactants dominate the reaction at low temperatures. Second, there is a limited operating range because engine failure could occur due to the high rate of pressure rise during the combustion process. Therefore, HCCI technologies cannot be applied over the entire operating range of engines.

Many studies have been performed to optimize internal combustion engines using H<sub>2</sub>, due to its low ignition energy, high diffusivity, and fast flame-propagation speeds. Researchers have studied the effects of an H<sub>2</sub> additive on the combustion and emissions of gasoline engines. Andrea et al. [9] reported that H<sub>2</sub> improved the coefficient of variation (COV) of the indicated mean effective pressure (IMEP), and decreased the burn duration under lean conditions ( $\phi < 0.85$ ). Ji et al. [10–12] reported that the H<sub>2</sub> effects on the combustion and emissions as the load conditions varied. The addition of H<sub>2</sub> to a gasoline engine increased the thermal efficiency under lean and low load conditions and reduced HC and CO emissions under lean conditions.

Fuel and H<sub>2</sub> are distributed homogeneously in a cylinder of a gasoline engine; the combustible mixture in the cylinder ignites instantaneously and forcibly by spark-plug ignition. H<sub>2</sub> additive can increase the flame speed of a gasoline engine because the gasoline fuel and H<sub>2</sub> are ignited simultaneously by the spark plug. However, in a diesel engine, the diesel fuel is injected into a cylinder along with air and H<sub>2</sub>, which are distributed homogeneously throughout the engine. The diesel engine ignites spontaneously without ignition equipment. Thus, the effects of H<sub>2</sub> on diesel engines can differ significantly from those on gasoline engines. Despite this, there have been very few studies that discuss the effects of H<sub>2</sub> on the combustion and emissions of diesel engines [13–15].

Shin et al. [16,17] studied the effects of H<sub>2</sub> additive on the combustion and NOx emissions of a diesel engine under constant fuel injection. They held the amount of diesel fuel constant while increasing the amount of H<sub>2</sub> additive. The engine power increased with the amount of the H<sub>2</sub> additive. Thus, the thermal efficiency of the diesel engine improved due to the higher IMEP with a similar friction mean effective pressure (FMEP). The NOx emissions decreased under these conditions, because the main combustion duration increased. However, Shin's studies did not deal with the independent effects of H<sub>2</sub> on diesel engine combustion and NOx emissions, because the brake mean effective pressure (BMEP) and surrounding temperature of the cylinder also changed with the addition of H<sub>2</sub>. The temperature elevation, in particular, affected not only the combustion, but also NOx formation [18].

In this study, we investigated the effects of H<sub>2</sub> on the combustion and emissions of diesel engines under constant BMEP conditions. The engine power was kept constant with respect to the H<sub>2</sub> supplied to the engine by adjusting the quantity of injected diesel fuel. This allowed investigation of the effects of H<sub>2</sub> without influencing the engine power or temperature. We also investigated the effects of H<sub>2</sub> on the PM that was emitted from the diesel engine. In this case, a four-cylinder 2.2-L direct-injection diesel engine, satisfying Euro5 legislation, was converted for H<sub>2</sub> feed and with low-pressure loop (LPL) exhaust gas recirculation (EGR). The cylinder pressure and emissions were measured to evaluate the H<sub>2</sub> effects on the combustion, and on the NOx and PM emissions, as the H<sub>2</sub> energy ratio changed for various EGR ratios.

## 2. Experiment

### 2.1. Experiment setup

Fig. 1 shows a schematic diagram of the experimental setup, which consisted of a diesel engine, a dynamometer, an LPL-EGR system, a thermodenuder, a scanning mobility particle sizer (SMPS), and equipment that measured the pressure, temperature, air flow rate, H<sub>2</sub> flow rate, and exhaust/intake gas composition.

A four-cylinder 2.2-L R-engine made by Hyundai Motor Company was used in this study. This engine satisfied Euro5

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