

# A novel tubular oxygen-permeable membrane reactor for partial oxidation of  $CH<sub>4</sub>$  in coke oven gas to syngas

## Yuwen Zhang\*, Kun Su, Fanlin Zeng, Weizhong Ding, Xionggang Lu

Shanghai Key Laboratory of Modern Metallurgy and Materials Processing, Shanghai University, Shanghai 200072, China

## article info

Article history: Received 13 February 2013 Received in revised form 2 May 2013 Accepted 4 May 2013 Available online 6 June 2013

Keywords: Tubular oxygen-permeable membrane reactor Catalytic partial oxidation Coke oven gas Syngas production

## **ABSTRACT**

Dense BaCo<sub>0.7</sub>Fe<sub>0.2</sub>Nb<sub>0.1</sub>O<sub>3- $\delta$ </sub> (BCFNO) membrane tubes were prepared by slip casting and readily brazed to 310S stainless steel supports using a silver-based alloy. A novel tubular membrane reactor was constructed by placing a cylindrical Ni-based monolithic catalyst coaxially around the tubular membrane and a conventional Ni-based catalyst-bed apart from the membrane tube. The novel membrane reactor was successfully applied to partial oxidation of CH<sub>4</sub> in coke oven gas (COG). At 850 °C, 94% of CH<sub>4</sub> conversion, 93% of H<sub>2</sub> and as high as 11.3  $\text{cm}^3 \text{ cm}^{-2} \text{ min}^{-1}$  of oxygen permeation flux were obtained. The experimental  $H_2$  and CO selectivity and CH<sub>4</sub> conversion were close to the thermodynamically predicated ones. There was a good match in the coefficient of thermal expansion (CTE) among BCFNO membrane, Ag-based alloy and 310S metal support. Long-term operation test results indicate that the novel tubular BCFNO membrane reactor exhibited not only high activity but also good stability for the partial oxidation of  $CH<sub>4</sub>$  in COG to syngas.

Copyright © 2013, Hydrogen Energy Publications, LLC. Published by Elsevier Ltd. All rights reserved.

## 1. Introduction

Coke oven gas (referred as COG), a by-product generated in the process of producing coke, is gaining increasing attention as one of the most attractive sources of syngas or hydrogen production  $[1-3]$  $[1-3]$ . The main components of COG are 54-59%  $H_2$ , 24-31% CH<sub>4</sub> and 5.5-7% CO [\[4\].](#page--1-0) As a potential source for syngas or hydrogen production from  $CH<sub>4</sub>$  by catalytic partial oxidation (CPO), COG can be as competitive as natural gas in the terms of energy consumption and amount of net carbon dioxide emis-sion [\[5\]](#page--1-0). However, the partial oxidation of  $CH<sub>4</sub>$  in COG requires high-cost pure oxygen. Recently, our group has used mixed ionic-electronic conducting (MIEC) membrane reactor to produce syngas by reforming of  $CH_4$  in COG [\[6](#page--1-0)–[8\].](#page--1-0) The technologies based on MIEC membranes make it possible to integrate oxygen separation and catalytic partial oxidation in a single

reactor and can significantly reduce the energy and cost for syngas production from methane [\[9,10\].](#page--1-0) The detailed performance and stability of the disc-shaped BaCo<sub>0.7</sub>Fe<sub>0.2</sub>Nb<sub>0.1</sub>O<sub>3- $\delta$ </sub> (BCFNO) membrane reactor under the condition of COG were investigated and the possible reaction pathways of partial oxidation of  $CH_4$  in COG in the membrane reactor were deduced  $[11-13]$  $[11-13]$ .

CrossMark

To develop a commercial process for syngas production from COG by a membrane reactor, high temperature and large area modules with gas-tight seals must be constructed. In all pervious studies, disc-shaped membranes with only a limited membranes area were employed for membrane reactors as they are easily fabricated  $[11-13]$  $[11-13]$  $[11-13]$ . Although the membrane area can be enlarged by employing a multiple planar stack, many problems such as sealing and pressure resistance have to be faced. In recent, tubular membranes have been

 $*$  Corresponding author. Tel./fax:  $+86$  21 56338244.

E-mail address: [springzyw@shu.edu.cn](mailto:springzyw@shu.edu.cn) (Y. Zhang).

0360-3199/\$ - see front matter Copyright © 2013, Hydrogen Energy Publications, LLC. Published by Elsevier Ltd. All rights reserved. <http://dx.doi.org/10.1016/j.ijhydene.2013.05.019>

developed to reduce the engineering difficulties, especially the problems associated with the high temperature seal  $[14-17]$  $[14-17]$ .

In this article, the closed-one-ended BCFNO membrane tubes were fabricated and readily brazed to a stainless steel supports using a silver-based alloy. A novel tubular membrane reactor was constructed by placing a quartz tube coaxially around the membrane. The shell was filled with a cylindrical Ni-based monolithic catalyst and a conventional Ni-based catalyst-bed was packed apart from the membrane tube. The performance of the novel tubular BCFNO membrane reactor was evaluated under the condition of COG.

## 2. Experimental

## 2.1. Powder and membrane preparation

The BCFNO powder was prepared by solid state reaction. Details of the preparation procedure of the BCFNO powder has been given elsewhere [\[6\].](#page--1-0) The closed-one-ended membrane tubes were fabricated by slip casting [\[18\].](#page--1-0) Pouring aqueous slurry of ceramic powders into plaster mold could get closedone-end tubular membranes. The green tubes were heated at a rate of 20 °C h<sup>-1</sup> in the temperature range of 100–350 °C to facilitate the removal of the gaseous species formed during decomposition of the organic additives, then the tubes were sintered between 1000 and 1150 °C for 20 h. The final tubes had an outer diameter of about 16 mm and a wall thickness of 1 mm. In present study, a short membrane tube with a length of 110 mm was used.

#### 2.2. Membrane reactor set-up

A high temperature membrane reactor system for assessing oxygen permeation flux and the conversion of  $CH<sub>4</sub>$  in COG was used, schematically shown in Fig. 1. The closed-one-ended membrane tube was sealed on the stainless steel support by a silver-based RAB (reactive-air-brazing)-alloy [\[19\]](#page--1-0). Then the membrane tube on the steel support was placed inside a larger quartz tube. A cylindrical Ni-based monolithic catalyst (Catalyst A shown in Fig. 1) was placed in the annulus region. The catalyst LiLaNiO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was prepared via the impregnation



according to report [\[6\]](#page--1-0) and used as the catalysts A. A porous cylindrical  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was used as a catalyst support. The annulus distance between the membrane and the monolithic catalyst was about 1 mm. At the same time, a conventional Ni-based catalyst-bed (Catalyst B shown in Fig. 1) was packed a few centimeters apart from the membrane tube along the downstream. The catalysts B was a commercial Z111 series reforming catalyst supplied by the southwest research and design institute of chemical industry in China. Helium or COG was passed through the annulus between the larger quartz and membrane/stainless steel tube. The model COG was a typical mixture expected in a commercial recycle feed that contained 57.09%H<sub>2</sub>, 28.18%CH<sub>4</sub>, 7.06%CO, 3.16%CO<sub>2</sub> and 4.51%Ar. Membrane gas leak free conditions were ensured by monitoring nitrogen concentration on the permeation side.  $N_2$  in the model COG was substituted with Ar in order to ensure the reliability of monitoring nitrogen concentration. In present experiments, no nitrogen leakage was detected. Inside the stainless steel support tube was a smaller tube through which air was introduced to the dead-end side of the membrane tube. The membrane module was heated by a temperature programmable tubular furnace. The temperature was measured by a K-type thermocouple encased near the membrane tube. The flow rates of the feed gas were controlled by mass flow controllers. On the outside of the membrane, the effluent compositions were measured by a gas chromatograph (VARIAN, CP3800) equipped with a thermal conductivity detector. When the model COG was fed, the oxygen permeation flux was determined from the content of CO and  $CO<sub>2</sub>$  in the reacted gas and the yield of  $H<sub>2</sub>O$ evaluated from the balance of hydrogen before and after the reaction. The conversion of  $CH<sub>4</sub>$  in the model COG, the selectivities of CO and  $H_2$  were defined as reference [\[11\]](#page--1-0).

The phase and crystal structures of the sintered membranes and the samples after experiments were characterized with an X-ray diffractometer (XRD, Rigaku D-Max/RB). The surface morphology of the membranes was observed using a scanning electron microscope (SEM, JSM-6700F). Measurements of the coefficient of thermal expansion (CTE) as a function of temperature were conducted on 25 mm  $\log x$  3 mm diameter bars of BCFNO membrane, silver-based alloy and metal support using a Netzsch dilatometer DIL 402C.

## 3. Results and discussion

### 3.1. Morphology of the tubular membranes

The plasters mold and tubular membranes are shown in [Fig. 2](#page--1-0). The surfaces and cross-section of the fresh tubular BCFNO membrane were characterized by SEM and the results are presented in [Fig. 3.](#page--1-0) As shown in [Fig. 3\(](#page--1-0)a) and (b), it can be seen that the ceramic grains exhibit clear grain boundaries with size of several microns. [Fig. 3\(c\)](#page--1-0) shows that there exist some pores that are visible in the cross-section but do not communicate with either membrane surface. The nitrogen permeation measurements confirmed that the BCFNO tubular membrane is gastight and no open pores exists. The relative densities of the sintered tubular membranes determined by Archimedes method were higher than 93%, which showed Fig. 1 - Diagram of tubular ceramic membrane reactor. That the tubular membranes were dense. A regular circular

Download English Version:

<https://daneshyari.com/en/article/7722574>

Download Persian Version:

<https://daneshyari.com/article/7722574>

[Daneshyari.com](https://daneshyari.com)