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Experimental modal analysis of lithium-ion pouch cells

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HIGHLIGHTS

• Experimental assessment of the frequency response of a Li-ion pouch cell.

• Assessment of the mode shapes for a Li-ion pouch cell using impulse excitation.

• Quantifying cell stiffness as a function of state of charge.

• Quantifying cell damping as a function of state of charge.

• Correlation of the cell's frequency response with road-induced vibration profiles.

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ABSTRACT

If future electric and hybrid electric vehicle batteries are to be designed such that the impact of vibration induced resonance is minimized, engineers tasked with the design of the vehicle's energy storage system must have a rigorous understanding of key system attributes such as the natural frequencies of the cell, the level of damping present and the mode shapes induced within the battery under mechanical load. This paper describes the underpinning theory and experimental method employed when using the impulse excitation technique to quantify the natural frequencies and mode shapes of a commercially available 25 Ah Nickel Manganese Cobalt Oxide (NMC) Laminate Pouch Cell. Experimental results are presented for fifteen cells at five different values of state of charge (SOC). The results indicate that irrespective of the energy content within the cell, the same four modes of vibration (torsion and bending) exist within a frequency range of 191 Hz–360 Hz. This is above the frequency range (0–150 Hz) typically associated with road-induced vibration. The results also indicate that the cell's natural frequencies of vibration and damping do not vary with changing values of SOC.

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1. Introduction

Within the automotive and road transport sector, one of the main drivers for technological development and innovation is the need to reduce the vehicle's fuel consumption and the emissions of carbon dioxide (CO₂). Legislative requirements are motivating vehicle manufacturers and subsystem suppliers to develop new and innovative electric vehicle (EV) and hybrid electric vehicle (HEV) concepts. Within this field, a key enabling technology is the design and integration of the high voltage (HV) battery system.

The impact of mechanical vibration on the vehicle's electrical and electronic components and subsystems is known to be a major cause of in-market durability failure [1]. If excessive warranty

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chnology is the terry system. hicle's electrical in to be a major essive warranty essive warranty is not support of a system. To ensure vehicle durability it is necessary to determine, at the design stage, the natural vibration characteristics

determine, at the design stage, the natural vibration characteristics of components, both in isolation and when they are aggregated into larger vehicle sub-systems. Recent studies [2] have highlighted that if a system was allowed to vibrate at one of its modal frequencies

claims are to be avoided, it is important that engineers tasked with the design of the HV battery system, properly understand the magnitude and frequency of the vibration inputs that the energy

storage system will be exposed too during the vehicle's predicted

life. If future vehicle battery systems are to be designed such that the impact of vibration induced resonance is minimized, engineers

must have a rigorous understanding of key system attributes such

as the natural frequencies of the cell, the level of damping for each

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Nomenclature		k_p	tip stiffness Nm^{-1}
		<i>K</i> _C	
_		m_H	nammer mass kg
Terms and abbreviations		m_c	cell mass kg
BMS	battery management system	Q	quality-factor -
dB	decibels	Т	time s
EMS	electromagnetic shaker	ω	frequency rads ⁻¹
EV	electric vehicle	ω_n	natural frequency rads ⁻¹
FRF	frequency response function	ς	damping ratio -
HEV	hybrid electric vehicle	$G_{xy}(f)$	cross-spectral density
HV	high voltage	$G_{xx}(f)$	auto-spectral density (x)
Li-ion	lithium ion	$G_{yy}(f)$	auto-spectral density (y)
NMC	nickel manganese cobalt	x(t)	system input (time domain)
NVH	noise vibration and harshness	y(t)	system output (time domain)
PSD	power spectral density	X(s)	system input (laplace domain)
SISO	single input single output	Y(s)	system output (laplace domain)
SOC	state of charge	H(s)	system transfer function (laplace domain)
		$H(j\omega)$	system transfer function (frequency domain)
Mathematical notation – symbols and units			
f_{max}	maximum frequency Hz		

with excessive, sustained, oscillatory motion permanent deformation or structural damage may occur. One example of an automotive component that failed through sustained excitation at one of its natural frequencies is presented within [1]. The research discusses the complete mechanical failure of the component after only 7000 km of driving [1]. The failure mode was identified using modal analysis techniques. The study found that the first natural frequency of the component occurred at 52.2 Hz and the road-load profile induced an accelerated fatigue condition within the device. Modal analysis is not limited to small components or systems. The methodology is also widely employed within the civil engineering domain, for example when assessing the structural integrity of bridges [3]. A recent study from the UK [3] highlights the application of modal analysis for understanding the undesirable swaving motion experienced when the Millennium Bridge was opened in London during the year 2000. It was identified that the 1st and 2nd natural modes of vibration for the bridge occurred between 0.5 and 1 Hz respectively and pedestrians excited these modes when they traversed the bridge [3]. Due to excessive motion of the structure and the subsequent fears for public safety, the bridge was closed until 2002, while engineer's integrated additional dampers within the bridge to reduce the amplification associated with the natural frequencies.

This paper describes the underpinning theory and experimental method employed when using the impulse excitation technique to quantify the natural frequencies and mode shapes of a commercially available 25 Ah Nickel Manganese Cobalt Oxide (NMC) Laminate Pouch Cell. From the experimental results obtained, values for cell damping and stiffness are estimated. Through the evaluation of different cells at the same SOC and at different values of state of charge (SOC), this research has been able to quantify the variability in the mechanical frequency response of the cells due to cell-to-cell manufacturing variations and stored energy.

This paper is structured as follows; Section 2 discusses the concept of mechanical testing for Li-ion cells and Section 3 introduces the experimental theory that underpins modal analysis. Section 4 describes the experimental set-up and method employed when undertaking modal analysis with a Li-ion pouch cell. Key results and discussions are presented in Section 5, with conclusions and further work presented in Sections 6 and 7 respectively.

2. Related research

Research undertaken into the mechanical testing and characterization of Li-ion cells, particularly within the context of designing and testing the vehicle's HV battery system can broadly be classified as being based on either static or dynamic test methods [2]. Irrespective of the exact methodology employed, the primary motivation for performing such experiments is often the generation of data to either parameterize or validate high fidelity finite element models of the battery system to better understand the impact of mechanical loading [2]. Research that aims to quantify pertinent material properties under a combination of different environmental conditions with varying mechanical and electrical loads includes, but is not constrained too: assessments of mechanical stress and strain within the numerous different components that comprise the cell (outer casing, electrodes, separators and current collector) [2,4–6], quantifying the creep within a representative sample of conductive material at different temperatures [6] and measuring the volume expansion of a pouch-cell during charge-discharge conditions [8].

In addition to the performance evaluation of different cell chemistries and formats, there is also a significant body of research that attempts to quantify the mechanical robustness (crashworthiness) of the cell or complete battery system. Examples of recent publications include the mechanical crushing of the cell [4,7,9], the effect of cell penetration [2,10], assessing the durability of the cell against impact [4,9] and mechanical shock [4] and understanding the fatigue conditions and possible failure modes of the battery system due to extreme variations in temperature and pressure [11,12]. The need to conduct such tests is often driven by the requirement to satisfy whole vehicle crash homologation Standards [13,14] and legislation, such as UN38.3, that governs the transportation of dangerous goods [15–17].

In recent years, there has been comparatively less research addressing the mechanical durability and vibration response of individual cells or the complete battery system. Research has been published [18] that correlates mechanical fatigue within the cell to the use of repetitive deep-discharge cycles. However, as discussed within Section 1, another of source of mechanical fatigue within the battery may well be the vibration-induced resonance resulting Download English Version:

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