



# A critical assessment of methods for the determination of the shear stress amplitude in multiaxial fatigue criteria belonging to critical plane class



Giovanni Petrucci\*

Università degli Studi di Palermo, Dipartimento di Ingegneria Chimica, Gestionale, Informatica, Meccanica, Viale delle Scienze, 90128 Palermo, Italy

## ARTICLE INFO

### Article history:

Received 3 October 2014  
Received in revised form 17 December 2014  
Accepted 4 January 2015  
Available online 10 January 2015

### Keywords:

Multiaxial fatigue  
Shear stress amplitude  
Critical plane  
Circumscribed circle  
Rectangular hull

## ABSTRACT

Multiaxial high cycle fatigue criteria based on the critical plane approach necessitate unambiguous definitions of the amplitude and mean value of the shear stress ( $\tau_a$  and  $\tau_m$ ) acting on the material planes. Four of the existing definitions relate the values of  $\tau_a$  and  $\tau_m$  to a geometrical element of the curve described by the tip of the shear stress vector (curve  $\Psi$ ), respectively, the radius of the Minimum Circumscribed Circle, the Longest Chord, the Longest Projection, the diagonal of the Maximum Rectangular Hull (MRH).

In this paper a critical assessment of the above definitions is proposed, focusing on that based on the concept of MRH, which is the most recently developed. The main issues of the comparison are the uniqueness of the solution in the determination of  $\tau_a$  and  $\tau_m$ , the ability to differentiate proportional and non-proportional stresses, the differences of the values of  $\tau_a$  obtained by each of the 4 methods for differently shaped curves  $\Psi$ .

© 2015 Elsevier Ltd. All rights reserved.

## 1. Introduction

Multiaxial high cycle fatigue criteria based on the critical plane approach require the determination of the shear stress amplitude  $\tau_a$  acting onto the planes passing through the analyzed material point [1–7]. The shear stress amplitude  $\tau_a$  relative to a plane  $\Delta$ , identified by its unit normal vector  $\mathbf{n}=[n_x, n_y, n_z]^T$ , has to be evaluated by processing the values of the components of the shear stress vector acting onto the plane,  $\tau_n(t)$  (Fig. 1a). The critical plane is determined as that experiencing the maximum shear stress amplitude  $\tau_{a_{\max}}$  [2,4–6], or the maximum value of a parameter involving  $\tau_a$  and the normal stress  $\sigma_n(t)$  acting onto the plane (Fig. 1a) [1,3].

In many cases, multiaxial fatigue criteria are used for cyclic states of stress, for which the components of the stress tensor assume the same values after a time period  $T$ . In the case of proportional stresses, the  $\tau_n$  vector maintains a constant direction and its tip describes a straight line segment (Fig. 1b); in this case, the determination of  $\tau_a$  and of the mean component of the shear stress,  $\tau_m$ , can be obtained directly from the maximum and minimum values of the modulus of  $\tau_n(t)$ . In the more general case of non-proportional stresses, both direction and magnitude of  $\tau_n(t)$  vary with time, so that, in the time period  $T$ , the tip of the shear stress vector

draws an imaginary closed curve  $\Psi$ , as in the example of Fig. 1 [4,5,8]. In this case the identification and the consequent evaluation of  $\tau_a$  and  $\tau_m$  is far from trivial and various definitions have been proposed [4,5,8–10,12–21].

In the comparison carried out in this paper four definitions of  $\tau_a$  and  $\tau_m$  have been mainly considered; each of them relates the value of  $\tau_a$  and  $\tau_m$  to a geometrical element of the curve  $\Psi$ , in particular the Minimum Circumscribed Circle (MCC), the Longest Chord (LC), the Longest Projection (LP), the Maximum Rectangular Hull (MRH). Some considerations about the definitions related to the Minimum Circumscribed Ellipse (MCE) and the Minimum Circumscribed Rectangle (MCR) in comparison to that of the MRH are also reported.

In all the definitions, the value of  $\tau_a$  is related to a parameter representative of the extent of the geometrical element, while  $\tau_m$  is related to a particular point in the  $u$ - $v$  plane, whose position depends on the position and the shape of the curve  $\Psi$ .

The Minimum Circumscribed Circle (MCC) to a curve is the smallest circle that contains all the points of the curve, as shown in Fig. 2a, where  $R$  is the radius of the MCC and  $C$  its center. According to the MCC method [4,5,8,9,12–15],  $\tau_a$  is equal to  $R$  and  $\tau_m$  is equal to the modulus of the vector joining point  $O$  to point  $C$ .

The Longest Chord of a curve is the segment joining the two farthest points one to the other among all the possible pairs of points of the curve, as shown in Fig. 2b where  $A$ ,  $B$  and  $C_c$  are the extremes

\* Tel.: +39 09123897279.

E-mail address: [giovanni.petrucci@unipa.it](mailto:giovanni.petrucci@unipa.it)

### Nomenclature

$t$	time	$R_a$	length of the major semi-axis of the MCE
$T$	time period	$R_b$	length of the minor semi-axis of the MCE
$N$	number of instants	$C$	center of the MCC
$\Delta$	generic material plane	$A, B$	endpoints of the LC
$\mathbf{n}$	unit normal vector of the plane $\Delta$	$C_C$	midpoint of the LC
$\sigma_n(t)$	normal component of the stress vector acting onto a generic plane	$C_P$	midpoint of the LP
$\tau_n(t)$	shear component of the stress vector acting onto a generic plane	$C_H$	center of the MRH
$\tau_a$	shear stress amplitude	$U, V$	coordinates of $C$
$\tau_m$	mean values of shear stress	$U_g, V_g$	coordinates of a generic point of the plane $\Delta$
$\tau_{a,c}$	shear stress amplitude in the critical plane	$r_i$	distances of the points of the curve from $C$
$\tau_{a_{\max}}$	maximum shear stress amplitude in a material point	$d_{ij}$	distance between the $i$ -th and the $j$ -th point of the curve $\Psi$
$\Psi$	curve described by the tip of the $\tau_n(t)$ vector	$d_{A,B}$	distance between points $A$ and $B$ (length of the LC)
$\tau_u, \tau_v$	coordinates of the points of the continuous curve $\Psi$	$\gamma$	angle between the $x$ and $u$ axes
$\tau_{u_i}, \tau_{v_i}$	coordinates of the points of the curve $\Psi$ at the time instants $t_i$	$L_x(\gamma)$	half-length of the projection of the curve $\Psi$ along $x$ direction
MCC	Minimum Circumscribed Circle	$L_y(\gamma)$	half-length of the projection of the curve $\Psi$ along $y$ direction
LC	Longest Chord	$L_H(\gamma)$	half-lengths of the diagonals of the circumscribed hulls of the curve $\Psi$
LP	Longest Projection	$\tau_{zx,a}(\gamma)$	amplitude of the shear stress acting in the $x$ direction, coincident with $L_x(\gamma)$
MRH	Maximum Rectangular Hull	$\tau_{zy,a}(\gamma)$	amplitude of the shear stress acting in the $y$ direction, coincident with $L_y(\gamma)$
OP	Orthogonal Projection (projection of the curve $\Psi$ along a line orthogonal to the LP)	$\tau_{z,a}(\gamma)$	amplitude of the equivalent shear stress, coincident with $L_H(\gamma)$
LSRH	Longest Size Rectangular Hull	$\Gamma_{LP}$	angle of the maximum value of the function $L_x(\gamma) = \tau_{zx,a}(\gamma)$
MCE	Maximum Circumscribed Ellipse	$\Gamma_{LH}$	angle of the maximum value of the function $L_H(\gamma) = \tau_{z,a}(\gamma)$
MCR	Minimum Circumscribed Rectangle		
$R$	radius of the MCC		
$L_C$	half-length of the LC		
$L_P$	half-length of the LP		
$L_H$	half-length of the diagonal MRH		
$L_O$	half-length of the OP		

and the midpoint of the LC,  $d_{A,B}$  and  $L_C = d_{A,B}/2$  are the length and the half-length of the LC,  $P_O$  and  $L_O = P_O/2$  are the length and the half-length of the Projection of the curve along a line orthogonal to the direction of the LC segment (OP). According to the LC method [9,10]  $\tau_a$  is equal to  $L_C$ , and  $\tau_m$  is equal to the modulus of the vector joining point  $O$  to point  $C$ .

The Longest Projections (LP) is the longest of the line segment obtained by projecting the curve  $\Psi$  on every line of the plane  $\Delta$ , emanating from the origin  $O$  [9,11], as shown in Fig. 2c, where  $P_L$  and  $L_P = P_L/2$  are respectively the length and the half-length of the LP. According to the LP method  $\tau_a$  is equal to  $L_P$  and  $\tau_m$  is equal to the modulus of the vector joining point  $O$  to point  $C_P$ .

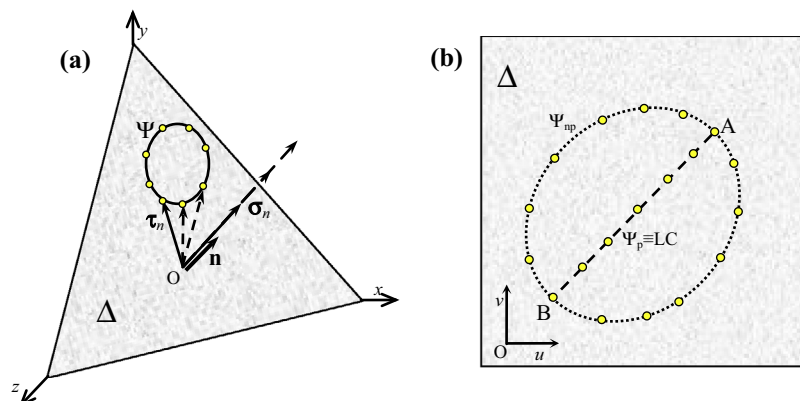


Fig. 1. Components of the stress vector acting onto a generic material plane  $\Delta$ : (a)  $\sigma_n$  and  $\tau_n$  components; (b) the curves  $\Psi$  described by the tip of  $\tau_n$  in the case of proportional (straight line segment  $\Psi_p$ ) and non-proportional ( $\Psi_{np}$ ) stress.

The Maximum Rectangular Hull (MRH) to a curve is the rectangle with the longest diagonal among all those containing all the points of the curve and whose four sides are in contact with the curve itself, at least in one point, as shown in Fig. 2d, where  $L_H$  is the half-length of the diagonal of the MRH and  $C_H$  is its center. According to the MRH method [16]  $\tau_a$  is equal to  $L_H$ , while no definition has been provided for  $\tau_m$  [16,17].

In the MCE approach [18–20] the smallest ellipse that circumscribes the curve  $\Psi$  is properly determined, then  $\tau_a$  is evaluated as the square root of the sum of the squares of the lengths of its major and minor semi-axis,  $R_a$  and  $R_b$ . The method based on the MCR [21] is similar to that of the MRH, being the minimum rectangular hull considered rather than the maximum one.

Download English Version:

<https://daneshyari.com/en/article/776667>

Download Persian Version:

<https://daneshyari.com/article/776667>

[Daneshyari.com](https://daneshyari.com)