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Full Length Article

Change of Cu⁺ species and synergistic effect of copper and cerium during reduction-oxidation treatment for preferential CO oxidation



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ABSTRACT

The CuO-CeO₂@SiO₂ catalyst with flower-sphere morphology was prepared by the impregnation method and then experienced the reduction-oxidation treatment at different temperatures. The multi-technique characterization shows that the reduction-oxidation treatment can remodel CuO, improve textural and surface properties and change Cu⁺ content and synergistic effect of copper and cerium. The importance of this work lies in the fact that the decrease of Cu⁺ content and synergistic effect of copper and cerium that occurs in the reduction-oxidation process results in the decrease of catalytic activity over the CuO-CeO₂@SiO₂ catalyst for preferential CO oxidation. The process of reaction in rich-hydrogen streams is equivalent to a reduction procedure which decreases Cu⁺ content and synergistic effect of copper and cerium.

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1. Introduction

Many researches have focused on producing and delivering of clean hydrogen as the interest in proton-exchange membrane fuel cells (PEMFCs) increases [1–3]. Hydrogen for PEMFCs is usually generated by a multistage process including catalytic reforming of hydrocarbons and water-gas shift reaction. The resulting rich-hydrogen streams contain 0.5–2.0 vol% CO, which poisons Pt anode and must be removed to a trace level below 100 ppm [4–6]. Preferential oxidation of CO (CO-PROX) has been recognized as the most simple and cost-effective method to reduce CO from rich-hydrogen streams [4,7,8].

CuO-CeO₂ bimetal oxides are alternative catalysts to noble metals due to low cost and high catalytic performance in PROX reaction [9–16]. Catalytic performance is related to synergistic interaction of CuO-CeO₂ interfacial sites since activity of CO oxidation has been attributed to redox cycles of Ce⁴⁺/Ce³⁺ and Cu²⁺/Cu⁺, which are abundant in contact interface of copper and cerium [8,9,17–20]. The interfacial CuO is easily reduced to form Cu⁺ species that is generally considered as CO adsorption sites. Meanwhile, oxygen vacancies at contact interface can capture gas-phase oxygen molecules which are driven into active oxygen species. CO molecules adsorbed onto Cu⁺ would be quickly oxidized by adjacent active oxygen species [12,20]. Oxygen vacancies are reactivated and continuously capture gas-phase oxygen molecules to produce new active species around interface after desorbing oxygen [21,22]. However, CuO/CeO₂ catalyst usually decreases catalytic activity above 150 °C, which restricts the application of CuO/ CeO₂ catalyst [23]. To solve this problem, the inverse CeO₂/CuO catalyst is developed since 2010 [12,14,23]. The inverse CeO₂/CuO catalyst will experience the decrease of catalytic activity above 180 °C although it has better high-temperature activity than the CuO/CeO₂ catalyst. Therefore, it is essential to explore the cause of the decrease of catalytic activity in hydrogen-rich streams.

The process of reaction in rich-hydrogen streams for CO-PROX is equivalent to a reduction procedure. It is reported that reshaping CuO on silica generates highly active Cu/SiO₂ catalyst via a reduction-oxidation treatment [24]. There is a memory effect of the shape of CuO to metal copper on silica during the reduction process [24]. Therefore, we hope to acquire the information about the change of copper species or synergistic interaction of copper and cerium by the reduction-oxidation treatment.

In this work, the CeO₂@SiO₂ support with flower-sphere morphology was prepared by the hydrothermal method, and the thin SiO₂ layer was incompletely coated on the surface in order to ensure contact between CuO and CeO₂. The CuO-CeO₂@SiO₂ catalyst was prepared by the impregnation method and then experienced reduction-oxidation treatment at different temperatures aiming to remodel CuO on silica. The multi-technique characterization was employed to correlate change of properties with catalytic



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performance. The goal is to gain a further insight into the essential of the decrease of catalytic activity during CO-PROX reaction.

2. Experimental

2.1. Catalyst preparation

The CeO₂@SiO₂ support with flower-sphere morphology was prepared by the two-step hydrothermal method [25]. The C₆H₁₂O₆·H₂O was dissolved in 60 mL distilled water. The solution was stirred vigorously and sealed into the Teflon-lined autoclave, and then the solution was heated at 180 °C for 4 h. After cooling to room temperature, the Ce(C₂H₃O₂)₃·1.5H₂O were added in the above solution and kept at 180 °C for 12 h. The obtained solid was washed and dried overnight at 80 °C. It was denoted as CeO₂@C.

The absolute ethyl alcohol, $NH_3 \cdot H_2O$ and CTAB were added into a three-necked flask containing the CeO₂@C aqueous solution, respectively. The mixture was stirred and treated by ultrasonic wave for 30 min. Then, the TEOS was added dropwise into the mixture and stirred for 8 h. The mixture was washed by distilled water and absolute ethanol and dried overnight at 80 °C. Further, the solid was heated with a heating rate of 2 °C min⁻¹ and calcined at 600 °C for 6 h. The sample was named as CeO₂@SiO₂.

The CuO-CeO₂@SiO₂ catalysts were prepared by incipient wetness impregnation method. The as-prepared support was impregnated in the Cu(COOH)₂·3H₂O aqueous solution. Then, it was aged for 24 h and dried at 80 °C for 12 h. Finally, the solid was calcined at 600 °C for 6 h. The products were denoted as XCuO-CeO₂@SiO₂ catalysts. X before the symbol of CuO indicated quantity of CuO in the catalysts.

The 30CuO-CeO₂@SiO₂ catalyst was chosen as experimental sample and experienced the reduction-oxidation treatment in a tubular furnace as the following steps: (i) The sample was heated from room temperature to 200 °C, 250 °C or 300 °C with a ramp rate of 3 °C min⁻¹ and kept for 6 h in 10% H₂/Ar. (ii) The sample after reduction treatment was divided into two parts. One part was re-oxidized at 300 °C and another part was oxidized at 600 °C for 6 h in air. The obtained catalysts were marked as CuO-CeO₂@SiO₂-R_YO_Z. Y indicated the temperature of reduction (300 or 600 °C) after reduction treatment.

2.2. Catalyst characterization

X-ray powder diffraction was carried on a PANalytical Empyream X'pert PRO diffractometer by using Cu K α source (λ = 0.15406 nm). The range of scan was between 10 °C and 80 °C. The average crystallite size was estimated according to Scherrer's equation.

Scanning electron microscopy images of the samples were obtained by a Hitachi S-4800 scanning electron microscope with an accelerating voltage of 15 kV. The samples were coated with a thin layer of gold and platinum before scanning.

Transmission electron microscopy images of the samples were taken on a FEI Tecnai G^2 F20 transmission electron microscope. The samples were dispersed into ethanol with ultrasonic treatment for 10 min, and a drop of the suspension was placed on a copper grid for TEM observation.

 N_2 adsorption-desorption isotherms were achieved via a Quantachrome Autosorb-IQ adsorption analyzer at 77 K. Before each measurement, the sample was outgassed in vacuum at 200 °C for 12 h. The surface area was estimated by the Brunauer-Emmett-T eller method and the pore size distribution was calculated from the desorption branch using the Barrett-Joyner-Halenda method. $\rm H_2$ temperature-programmed reduction was conducted on a Micromeritics AutoChemII2920 equipped with a thermal conductivity detector. The samples were pretreated in a helium flow at 200 °C for 1 h and cooled to room temperature. The reduction profiles were collected in the 5% H₂/Ar mixture with a flow rate of 35 mL/min from room temperature to 800 °C.

X-ray photoelectron spectra were collected on a Perkin Elmer PHI 5000 ESCT System spectrometer with monochromatic Al K α radiation source (1486.6 eV) for the analyses of the core level signals of Cu 2*p* and Ce 3*d*. During data processing of XPS spectra, binding energy values were referenced to C 1*s* peak (284.8 eV) from adventitious contamination layer.

2.3. Catalytic performance test

Catalytic performance tests were carried on a fixed-bed reactor at atmospheric pressure. A mixture gas containing 1.0 vol% CO, 1.0 vol% O₂, 50.0 vol% H₂ and N₂ balance was passed through the reactor filled with 100 mg catalyst. The space velocity was 40,000 mL h⁻¹ g⁻¹ and the reaction was operated from 35 to 235 °C. The inlet and outlet streams were measured using an online GC-2014C gas chromatograph equipped with a thermal conductivity detector. CO, O₂ and N₂ were separated by a 5A molecular sieve column, and CO₂ and CH₄ were separated by a TDX column. The conversion of CO (C_{CO}) and O₂ (C_{O2}) as well as selectivity of CO₂ (S_{CO2}) were calculated according to the following Eqs. (1), (2) and (3), respectively.

$$C_{CO} \ (\%) = ([CO]_{in} - [CO]_{out}) / [CO]_{in} \times 100$$
(1)

$$C_{02} \ (\%) = ([O_2]_{in} - [O_2]_{out}) / [O_2]_{in} \times 100$$
(2)

$$S_{CO2} \ (\%) = C_{CO} / \lambda_{O2} \times 100$$
 (3)

In all the catalytic tests, $\lambda = 2$ was used, because this value was optimal for preferential oxidation of CO [26].

3. Results

3.1. Catalyst selection

3.1.1. X-ray power diffraction

Fig. 1 shows XRD patterns of the CuO-CeO₂@SiO₂ catalysts with different CuO content. The diffraction peaks at 28.55° , 33.08° , 47.49° and 56.53° were indexed to cubic fluorite CeO₂ [27,28].



Fig. 1. XRD patterns of the CuO-CeO₂@SiO₂ catalysts.

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