



# Analytical modeling and experimental validation of micro end-milling cutting forces considering edge radius and material strengthening effects



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## ABSTRACT

This paper presents a novel micro end-milling cutting forces prediction methodology including the edge radius, material strengthening, varying sliding friction coefficient and run-out together. A new iterative algorithm is proposed to evaluate the effective rake angle, shear angle and friction angle, which takes into account the effects of edge radius as well as varying sliding friction coefficient. A modified Johnson–Cook constitutive model is introduced to estimate the shear flow stress. This model considers not only the strain-hardening, strain-rate and temperature but also the material strengthening. Furthermore, a generalized algorithm is presented to calculate uncut chip thickness considering run-out. The cutting forces model is calibrated and validated by NAK80 steel, and the relevant micro slot end-milling experiments are carried out on a 3-axis ultra-precision micro-milling machine. The comparison of the predicted and measured cutting forces shows that the proposed model can provide very accurate predicted results. Finally, the effects of material strengthening, edge radius and cutting speed on the cutting forces are investigated by the proposed model and some conclusions are given as follows: (1) the material strengthening behavior has significant effect on micro end-milling process at the micron level. (2) Cutting forces predicted increase with the increase of edge radius. (3) Considering varying sliding friction coefficient can enhance the sensitivity of the predicted cutting forces to cutting speed.

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## 1. Introduction

In recent years, demands of micro products and components are growing in the fields such as electronics optics, aerospace and biotechnology. The miniature components usually have complex millimeter-level three-dimension geometries which require micron level accuracy. As an effective way to produce micro products, the micro end-milling can create more complex three-dimension geometries in a wide range of workpiece materials compared with the conventional fabrication methods such as photolithography and laser beam etching. Therefore, understanding and modeling of the micro end-milling process is desirable.

It is reported [1–7, 9–13] that in micromachining process, the specific cutting energy for removing unit volume of material

increases nonlinearly with the chip thickness decreasing from a few hundred microns to a few microns. In early years, many researchers have attempted to explain and predict this scaling phenomenon. Most of studies attribute it to the edge radius effect [1–7]. Waldorf et al. [1] proposed a slip-line model to predict the plowing component of cutting forces caused by the edge radius, and a series of experiments were performed on 6061-T6 aluminum using tools with different edge radius. Vogler et al. [2] presented a new cutting forces prediction model for micro end-milling based on the slip-line model which considering the minimum chip thickness and material microstructure, and the microstructure level finite element simulations were performed to determine the model parameters. Woon et al. [3] investigated the effects of tool edge radius on the frictional contact and flow stagnation phenomenon with the finite element approach. Bisacco et al. [4] presented a theoretical model for cutting forces prediction in micro end-milling based on the oblique cutting model which including the uncut chip thickness to edge radius ratio, and the shearing and plowing force coefficients were determined by the orthogonal cutting experiments. Fang [5]

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## Nomenclature

$A, B, C, m, n$	coefficients of Johnson–Cook model	$T_r$	room temperature (°C)
$b$	magnitude of the Burgers vector (nm)	$u$	exponential factor
$C_1, C_2$	constant	$V$	cutting speed (m/min)
$C_p$	specific heat (J/kg K)	$\alpha$	nominal rake angle (°)
$d_a$	axial depth of cut ( $\mu\text{m}$ )	$\alpha_e$	effective rake angle (°)
$F_{x(amp)}, F_{y(amp)}$	cutting forces amplitudes in X- and Y-direction (N)	$\alpha_n$	normal rake angle (°)
$f_t$	feed per tooth ( $\mu\text{m}/\text{tooth}$ )	$\alpha_t$	empirical coefficient
$G$	shear modulus (GPa)	$\alpha_r$	angle between feed rate and Y-direction (°)
$h$	uncut chip thickness ( $\mu\text{m}$ )	$\beta_n$	normal friction angle (°)
$h_0$	primary shear zone thickness ( $\mu\text{m}$ )	$\beta_T$	percentage of the total shear deformation energy
$i$	inclination angle (°)	$\gamma$	run-out angle (°)
$K$	number of flutes	$\delta$	engagement angle (°)
$K_{tc}, K_{rc}, K_{ac}$	shearing force coefficient in tangential, radial, axial direction ( $\text{N}/\text{mm}^2$ )	$\varepsilon$	equivalent plastic strain
$K_{te}, K_{re}, K_{ae}$	plowing force coefficient in tangential, radial, axial direction ( $\text{N}/\text{mm}^2$ )	$\dot{\varepsilon}$	equivalent plastic strain rate ( $\text{s}^{-1}$ )
$K_0$	preset value	$\dot{\varepsilon}_0$	reference plastic strain rate ( $\text{s}^{-1}$ )
$L$	length of the primary shear zone ( $\mu\text{m}$ )	$\zeta$	constant
$M$	Taylor factor	$\eta$	strain gradient ( $\mu\text{m}$ )
$N$	rotation speed of the spindle (rpm)	$\eta_0, \gamma_0, \alpha_0, \rho_0$	angle variables in slip-line model [1]
$R$	length variable in slip-line model [1]	$\eta_c$	chip velocity angle (°)
$r$	radius of the tool (mm)	$\theta$	angular position of cutter (°)
$re$	edge radius ( $\mu\text{m}$ )	$\theta_f$	separation angle (°)
$\bar{r}$	nye factor	$\theta_s, \theta_e$	Integrating start angle and integrating end angle (°)
$T$	material temperature (°C)	$\lambda$	helix angle (°)
$T_m$	material melting temperature (°C)	$\mu$	sliding friction coefficient
		$\xi$	exponential constant
		$\rho$	radial run-out length ( $\mu\text{m}$ )
		$\rho_m$	material density ( $\text{kg}/\text{m}^3$ )
		$\tau$	shear flow stress (MPa)
		$\phi_n$	normal shear angle (°)

proposed a generalized slip-line model with a round edge tool to predict the shearing and plowing forces. Jin et al. [6,7] presented a slip-line model for micro orthogonal cutting process considering the tool edge radius effect, and the Johnson–Cook constitutive model was adopted to estimate the shear flow stress and hydrostatic pressure.

Material strengthening effect is one of the significant characteristics of the micro machining process. However, to date, very meager efforts have been dedicated to analytical modeling of cutting forces in micro end-milling process considering the effect of material strengthening. Dinesh et al. [8] linked the material strengthening behaviors observed in micro-/nano-indentation to that in micro machining and suggested that the material strengthening effect in micro machining could also be explained by the strain gradient plasticity theory. Based on the work in [8], Joshi et al. [9] presented a modified Johnson–Cook constitutive model by introducing the material length scale and effective strain gradient. Liu et al. [10] adopted this modified Johnson–Cook constitutive model to the finite element based micro orthogonal cutting simulations, and the results showed that the strain gradient strengthening effect is prominent especially at small uncut chip thickness. Lai et al. [11] also introduced this model to finite element simulations of micro orthogonal cutting. Rao and Srinivasa [12,13] developed a new strain gradient equation and introduced it to the modified Johnson–Cook constitutive model. The results showed that the predicted shear stress enhanced about three times compared to the model proposed by Joshi et al. [9] at uncut chip thickness of 10  $\mu\text{m}$ .

The run-out have significant influence on the micro end-milling process. Some efforts have been devoted to modeling the effects. Bao et al. [14] proposed an analytical model to calculate the uncut chip thickness. Li et al. [15] developed a new uncut chip thickness computation algorithm for micro end-milling

accounting for the combination of exact trochoidal trajectory of tool tip and run-out. The similar algorithms were adopted to calculate uncut chip thickness in [16,17]. Bissacco et al. [4] presented a simplified method to estimate the uncut chip thickness considering run-out and discussed the effect of run-out on cutting forces.

As mentioned above, a large number of models have been developed to predict the cutting forces in micro end-milling, but these models did not consider the effects of edge radius, material strengthening and run-out together, which could affect the prediction accuracy of the cutting forces. The objective of this paper is to develop a novel analytical micro end-milling cutting forces model by using the fundamental metal cutting principles and material physical properties, which incorporates the effects of edge radius, material strengthening, varying sliding friction coefficient and run-out. Development of such a new analytical model is contributed to further improve prediction accuracy for the cutting forces in micro end-milling. Besides, investigation of the effects of the material strengthening, edge radius and varying sliding friction coefficient affected by cutting speed on the cutting forces is also conducive to provide better understanding and monitoring for the micro end-milling process.

The organization of the paper is as follows: in Section 2, a novel analytical micro end-milling cutting forces model is developed which considers the edge radius, material strengthening, varying sliding friction coefficient and run-out. Section 3 presents the experimental set-up and compares the predicted results with the experimental measurements. In Section 4, the effects of the material strengthening, edge radius and cutting speed on the cutting forces are further investigated by using the proposed model. The modeling characteristics and some conclusions are given in Section 5.

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