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recycling system

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ABSTRACT

In the technology of liquid ammonia modification, the ammonia is recycled by compression and condensation. To minimize the energy-consumption of ammonia recycling system, compression ratio and fan speed are optimized. Thermodynamic models for the compressor and evaporative condenser are developed respectively. Mathematical equations are given to determine the optimal compression ratio and the corresponding fan speed ratio. To solve the equations, a numerical algorithm is proposed. By controlling the fan speed, the matching of ammonia mass flow rate and air flow rate can be optimized, which brings about the minimal energy-consumption. When the wet-bulb temperature is 22 °C, the system energyconsumption could be saved by 10.8-12.9% under optimal compression ratio and fan speed. © 2016 Elsevier Ltd and IIR. All rights reserved.

Vitesse optimale de ventilateur et taux de compression d'un système à compression de vapeur à l'ammoniac à condensation par air

Mots clés : Condensation par air ; Compression de vapeur ; Taux de compression ; Vitesse de ventilateur ; Système de recyclage d'ammoniac ; Consommation énergétique

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Nomenclature

- A correction coefficient affected by water film temperature
- $\begin{array}{ll} A_{1e} & \mbox{ overall mass transfer coefficient of evaporative} \\ & \mbox{ condenser if operating at rated fan speed [kg s^{-1}]} \\ C & \mbox{ coefficient [0.35]} \end{array}$
- c_{pwa} specific heat capacity of air $[1.02 \times 10^3 \text{ J kg}^{-1} \text{ K}^{-1}]$
- d₀ external diameter of tubes in the evaporative condenser [m]
- F_o external surface area of tubes of evaporative condenser $[m^2]$
- F_{ω} contact area between water film and air $[m^2]$
- specific enthalpy of the superheated ammonia at the compressor suction [J kg⁻¹]
- h_2 specific enthalpy of the superheated ammonia at the compressor discharge [J kg⁻¹]
- h_3 specific enthalpy of ammonia at saturated state [J kg⁻¹]
- h₄ specific enthalpy of liquid ammonia at saturated state [J kg⁻¹]
- $h_{air,in}$ enthalpy of air at the inlet of evaporative condenser [J kg⁻¹]
- $h_{air,out}$ enthalpy of air at the outlet of evaporative condenser [J kg⁻¹]
- h_{ave} average enthalpy of air [J kg⁻¹]
- h_{sat} enthalpy of saturated air at condensing temperature [J kg⁻¹]
- i number of compressor cylinder
- J cost function [J kg⁻¹]
- k isentropic index of compression, for ammonia [1.3]
- M molar mass of ammonia $[17 \times 10^{-3} \text{ kg mol}^{-1}]$
- \dot{m}_a ammonia mass flow rate [kg s⁻¹]
- \dot{m}_{air} actual air mass flow rate [kg s⁻¹]
- \dot{m}_{aire} air mass flow rate if operating at rated fan speed [kg s⁻¹]
- m' polytropic index of compression, for ammonia [1.28]
- n_1 speed of compressor [r s⁻¹]
- n_2 actual speed of fan [r s⁻¹]
- n_{2e} rated speed of fan [r s⁻¹]
- P_f actual power of condenser fan [W]
- P_{fe} rated power of condenser fan [W]
- P_p rated power of condenser pump [W]
- Pr_f Prandtl number of air [0.721]
- P_t actual power input of compressor [W]
- p_{dk} discharge pressure of compressor [Pa]
- p_{int} suction pressure of compressor [Pa]
- Q heat rejection of evaporative condenser [W]

1. Introduction

Liquid ammonia modification is a novel process for dyeing, printing and finishing. Liquid ammonia medium is used to modify cotton and linen, which could improve the perfor-

- q_{va} airflow provided by evaporative condenser fan if operating at rated fan speed [m³ s⁻¹]
- R ideal gas constant [8.314 J mol⁻¹ K⁻¹]
- Re_f Reynolds number of air
- T_1 suction temperature of compressor [K]
- T₂ condensing temperature of ammonia [K]
- T_{db} dry-bulb temperature of the inlet air in the condenser [°C]
- T_{wb} wet-bulb temperature of the inlet air in the condenser [°C]
- u_2 fan speed ratio $u_2 \in [0, 1]$
- v_{int} specific volume of ammonia at compressor suction [m³ kg⁻¹]
- $\label{eq:null_states} \begin{array}{ll} \upsilon_m & \mbox{ coefficient of kinematic viscosity of air} \\ [15.8 \times 10^{-6} \ m^2 \ s^{-1}] \end{array}$
- v_p cylinder volume of compressor [m³]
- $\dot{\nu}$ theoretical volumetric displacement of compressor $[m^3 \ s^{-1}]$
- $\label{eq:Wts} W_{ts} \quad \text{isentropic compressor work per unit mass of} \\ ammonia \begin{bmatrix} J \ kg^{-1} \end{bmatrix}$
- w_{max} actual air velocity at the narrowest section in the evaporative condenser [m s⁻¹]
- w_{maxe} air velocity at the narrowest section in the evaporative condenser if operating at rated fan speed [m s⁻¹]
- $\label{eq:lambda} \begin{array}{ll} \Delta h & \mbox{heat rejection per unit mass of ammonia during} \\ & \mbox{condensing process } [J \mbox{ kg}^{-1}] \end{array}$
- Δh_{air} increment enthalpy of air in the evaporative condenser [J kg⁻¹]

Abbreviations

- COP coefficient of performance
- CTC condensing temperature control
- HPC head pressure control
- RH relative humidity

Greek symbols

- $lpha_{
 m c}$ sensible heat transfer coefficient [W m⁻² K⁻¹]
- β_{w} correction coefficient of contact area between water film and air affected by water splashing and waving [1.5]
- η overall electrical efficiency of compressor
- $\eta_{\scriptscriptstyle{isen}}$ is entropic efficiency of compressor
- η_m combined motor and transmission efficiency of compressor
- η_v volumetric efficiency of compressor
- ε compression ratio
- $\begin{array}{ll} \lambda_f & \mbox{ heat conductivity of air under average temperature} \\ & [2.61 \times 10^{-2} \ \mbox{W} \ \mbox{m}^{-1} \ \mbox{K}^{-1}] \end{array}$
- ho_a average density of air [1.16 kg m⁻³]

mance of cotton and linen. As liquid ammonia is easy to volatilize and ammonia gas is a toxic gas, liquid ammonia and ammonia gas must be recycled in the technology of liquid ammonia modification.

Ammonia gas is recycled by compression and condensation. The recycling process leads to considerable energyDownload English Version:

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