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## ABSTRACT

Si3N4 fibers prepared from polycarbosliane are exposed in dry and wet air respectively from 800 to 1300 °C for up to 1 h. After dry air oxidation, an uniform  $SiO<sub>2</sub>$  coating doped with nitrogen is formed on fiber surface. However, the coating obtained in wet air is much thicker with more complex microstructure containing sublayers of N-doped SiO<sub>2</sub>, near stoichiometric Si<sub>3</sub>N<sub>4</sub> and graphite-like nanoribbons. Activation energy for oxidation in wet and dry air is determined as 108 and 152 kJ mol−<sup>1</sup> , respectively. Both of the values are lower than the known Si<sub>3</sub>N<sub>4</sub> materials with  $E_a$  of 259–485 kJ mol<sup>-1</sup>.

## 1. Introduction

Continuous silicon nitride  $(Si<sub>3</sub>N<sub>4</sub>)$  thin fiber is a family of polymerderived ceramic fibers composed of Si and N, and is commonly doped with different amount of C and O according to the precursor structures  $[1–4]$  $[1–4]$  and preparation techniques  $[5–7]$  $[5–7]$ . The non-stoichiometric nature of the precursor results in uniformly disordered structures in the fiber after pyrolysis. Consequently, most of the polymer derived  $Si<sub>3</sub>N<sub>4</sub>$  fibers are amorphous up to 1400 °C and retain high tensile strength [8–[11](#page--1-2)]. With additional characters of high electrical resistivity, low thermal conductivity and low dielectric constant, the continuous  $Si<sub>3</sub>N<sub>4</sub>$  fibers are promising reinforcements for thermal insulation and microwavetransparent composites [12–[14\]](#page--1-3). In recent years, one of the expected applications of  $Si<sub>3</sub>N<sub>4</sub>$  fibers has been indicated as reinforcement in the high temperature microwave-transparent composites as replacement of the  $SiO<sub>2</sub>$  fiber, which losses most of its original strength when serving at above 900 °C, owing to the severe grain coarsening [\[15](#page--1-4)–17]. Nevertheless, also the  $Si<sub>3</sub>N<sub>4</sub>$  fibers face challenges during service in air, because of passive oxidation of the fiber surface and microcracking at the fiber/oxidation coating interface.

To date, studies on the oxidation behavior of  $Si<sub>3</sub>N<sub>4</sub>$  were conducted mainly on powders and bulks [\[18](#page--1-5)–25]. Results indicated that the oxidation rates of  $Si<sub>3</sub>N<sub>4</sub>$  depended upon the purity of the material. The lowest oxidation rates were observed for high-purity chemical vapor deposited (CVD)  $Si<sub>3</sub>N<sub>4</sub>$  [[25\]](#page--1-6). However, these works contributed little to knowing the oxidation behavior of the continuous  $Si<sub>3</sub>N<sub>4</sub>$  fibers, which was not only because of the variations in composition between bulks

and fibers, but also due to the particularity of the fibers with respected to heat transfer process and the resultant structural characters. Studies regarding the  $Si<sub>3</sub>N<sub>4</sub>$  fibers mainly dealt with the crystalline behavior of the fibers at high temperatures in inert atmospheres. Matsuo et al. studied the structural evolution of perhydropolysilazane (PHPS)-derived Si<sub>3</sub>N<sub>4</sub> fiber after heating at 1400–1500 °C in N<sub>2</sub>. α-Si<sub>3</sub>N<sub>4</sub> particles were only detected on the fiber surface, which seemed to be proceeded by a vapor phase growth mechanism [[26\]](#page--1-7). Gilkes et al. explored the microstructure of hydridopolysilazane (HPZ)-derived  $Si<sub>3</sub>N<sub>4</sub>$  fibers by using neutron scattering and nuclear magnetic resonance [[27\]](#page--1-8). The HPZ-Si3N4 fibers were found to contain excess crystalline silicon and disordered carbon, and the fibers annealed in  $N_2$  at 1400 °C for 100 h contained a cristobalite phase. Similar results evidenced that these polymer-derived  $Si<sub>3</sub>N<sub>4</sub>$  fibers had excellent thermal stability [[28\]](#page--1-9). Cinibulk et al. investigated the oxidized microstructure of a Si-B-C-Nbased fiber derived from an N-methylpolyborosilazane precursor. With presence of B, complicated coating structure formed on the fiber surface upon heating in stagnant laboratory air at 1500 °C for 2 h. Although the fiber core retained its amorphous nature, the fiber suffered significant strength degradation after oxidation [[29](#page--1-10)].

In the present work,  $Si<sub>3</sub>N<sub>4</sub>$  fiber derived from polycarbosilane (PCS) are exposed to wet and dry air respectively in a temperature range from 800 to 1300 °C for up to 1 h. Microstructure, mechanical property and oxidation kinetics of the oxidized  $Si<sub>3</sub>N<sub>4</sub>$  fiber are explored. The effect of reactive gas species on oxidation behavior of the  $Si<sub>3</sub>N<sub>4</sub>$  fiber is here discussed.

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#### <span id="page-1-0"></span>Table 1

Chemical composition of the as prepared  $Si<sub>3</sub>N<sub>4</sub>$  fibers.



#### 2. Experimental procedure

The PCS precursor is synthesized following the Yajima's route [[30,31](#page--1-11)]. The average molecular weight (M) is 1190, and the softening point is 189 °C. The obtained PCS is used as precursor of the  $Si<sub>3</sub>N<sub>4</sub>$  fiber and treated through the route developed by Japan atomic energy research institute [\[7\]](#page--1-12). [Table 1](#page-1-0) shows the chemical composition of the asprepared  $Si<sub>3</sub>N<sub>4</sub>$  fibers. Average tensile strength of the fiber is 936 ± 87 MPa.

For oxidation experiment, green fibers are placed in alumina crucible and pushed into alumina tube furnace with  $MoSi<sub>2</sub>$  as heating element. Wet air is obtained by blowing compressed dry air (Linde Gas, 99.99%, China) into deionized water in an airtight container, which was connected directly to the furnace tube. Partial pressure of the water vapor can be controlled by changing the dry air pressure as well as the water temperature according to Ideal Gas Law. In this work, the partial pressure of water vapor is 2.4 KPa. The heating rate of the oxidation is 5 °C min<sup>-1</sup>. The holding times at each target temperature, 800, 1000 and 1300 °C, are 0.5 h and 1 h respectively. Tensile strength of the single fiber is tested at room temperature using an electronic single fiber strength tester (SLBL-10N, SHIMADZU, Japan). 25 specimens are used in each test. The gauge length is 25 mm and the loading rate is  $1$  mm min<sup>-1</sup>.

The phases of the fibers are identified using an X-ray diffractometer (D8 Advance, Bruker-AXS, Germany). The microstructure is characterized using SEM of 30 keV (SU-70, Hitachi, Japan) and by TEM of 200keV(JEM 2100, JEOL, Japan and Talos F200S, FEI, USA). The TEM specimens are prepared by a special embedding method reported elsewhere [[32\]](#page--1-13). The embedded specimens are thinned by cutting, mechanical grinding, dimpling and ion milling.

### 3. Result and discussion

#### 3.1. Microstructural evolution of the  $Si<sub>3</sub>N<sub>4</sub>$  fiber after oxidation

[Fig. 1](#page-1-1) shows the weight changes of the  $Si<sub>3</sub>N<sub>4</sub>$  fibers after oxidation. All of the treated fibers gain weight. The weight gain in wet air is significantly higher than that in dry air, indicating that the oxidation reaction is promoted by wet air condition. Similar results were also obtained in the oxidation of crystalline  $Si<sub>3</sub>N<sub>4</sub>$  and SiC materials

<span id="page-1-1"></span>

Fig. 1. Weight gain of  $Si<sub>3</sub>N<sub>4</sub>$  fibers after oxidized in (a) wet air and (b) dry air.

<span id="page-1-2"></span>

Fig. 2. X-ray diffraction patterns of the  $Si<sub>3</sub>N<sub>4</sub>$  fibers after oxidized in (a) wet air and (b) dry air.

[33–[35\]](#page--1-14). Whether in wet or dry air, the weight of the oxidized fibers increases with increasing temperature. As the  $Si<sub>3</sub>N<sub>4</sub>$  fibers are oxidized at 800 °C, the weight gain in isothermal processes changes almost linearly with the soaking time, indicating the oxidation process is controlled by surface reaction. However, above 1000 °C, the weight gain in last half hour becomes lower than that in first half hour. This indicates that the oxidation is retarded at high temperatures, since the inward diffusion of oxidizing gases is restricted and becomes a rate-controlling process as the thickness of the oxidated coating increases.

[Fig. 2](#page-1-2) shows the XRD pattern of the treated  $Si<sub>3</sub>N<sub>4</sub>$  fibers. All the Si3N4 fibers remain amorphous even after oxidation at 1300 °C for 1 h. The sharp peak at 21.8° after heating at 1300 °C belongs to lattice plane (004) of tridymite, which results from the crystallization of the silica coating. Based on the Scherrer formula, grain size of the tridymite coatings obtained after different treatments can be estimiated by the change of the FWHM (Full width at half maximum of peak intensity). As compared with the dry air oxidation, the  $Si<sub>3</sub>N<sub>4</sub>$  fiber oxidized in wet air at 1300 °C/1 h has a (004) peak of higher intensity with narrower FWHM (∼70% width of the FWHM obtained in dry air), indicating a larger grain size of the tridymite and a higher crytallinity degree of the coating. Results suggest that water vapor promotes not only the oxidation reaction, but also grain growth of  $SiO<sub>2</sub>$ .

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