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# Comprehensive analytic solutions for the geometry of symmetric constant-wall-thickness scroll machines



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## ARTICLE INFO

### Article history:

Received 17 March 2014

Received in revised form

2 May 2014

Accepted 31 May 2014

Available online 11 June 2014

### Keywords:

Scroll compressor

Scroll expander

Geometry

## ABSTRACT

In this work, a comprehensive framework and geometric solutions are presented for the most common type of scroll machine, the symmetric constant-wall-thickness scroll compressor based on the involute of a circle. This analytic treatment comprises solutions for the volume, derivative of volume, centroid, normalized force and moment parameters, and leakage areas for all chambers in the machine. The representations for the centroid and area are based on Green's Theorem analysis which allows for general solutions that can then also be applied to other machines. Analytic solutions are also presented for the discharge geometry corresponding to arc-line-arc, perfect-meshing-profile, one-arc, and two-arc discharge geometries. Each of the derived parameters is validated against numerical solutions based on polygons. Source code in the Python programming language is provided for the analytic derivations as well as the implementation of each of the analytic outputs.

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## Solutions analytiques générales pour la géométrie des machines à spirale à épaisseur de paroi constante

Mots clés : Compresseur à spirale ; Détendeur à spirale ; Géométrie

### 1. Introduction

The scroll machine was first proposed by [Léon Creux \(1905\)](#) in 1905, but it would be many decades before scroll compressors

would see practical application due to the manufacturing challenges posed by the involutes.

A significant amount of literature exists which deals with the geometric modeling of scroll compressors. [Morishita and Sugihara \(1984\)](#) produced one of the first complete

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<http://dx.doi.org/10.1016/j.ijrefrig.2014.05.029>

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Nomenclature		Subscripts	
<b>Variables</b>		<i>a</i>	Axial
<i>A</i>	Area (m <sup>2</sup> )	<i>a1</i>	Discharge arc 1
$\bar{A}$	Area contribution (m <sup>2</sup> )	<i>a1,1</i>	Discharge arc 1 point 1
<i>b<sub>l</sub></i>	Intercept of line	<i>a1,2</i>	Discharge arc 1 point 2
<i>d</i>	Distance (m)	<i>a2</i>	Discharge arc 2
<i>f</i>	Anti-derivative for force	<i>a2,1</i>	Discharge arc 2 point 1
<b>F</b>	Force vector (N)	<i>a2,2</i>	Discharge arc 2 point 2
<i>h</i>	Height of scroll (m)	<i>a2,max</i>	Maximum for discharge arc 2
<b>Gr</b>	Anti-derivative for area (m <sup>2</sup> )	<i>b</i>	Base (generating)
$\hat{i}$	Unit vector in +x direction	<i>disp</i>	Displacement
$\hat{j}$	Unit vector in +y direction	<i>D</i>	Downstream
<i>L</i>	Length (m)	<i>o</i>	Orbiting
<i>L</i>	Green's theorem function	<i>0</i>	Initial
<i>M</i>	Green's theorem function	<i>s</i>	Starting
<i>m<sub>l</sub></i>	Slope of line	<i>e</i>	Ending
<b>M</b>	Moment (N m)	<i>f</i>	Fixed scroll
<b>n</b>	Unit normal vector	<i>f–o</i>	From fixed to orbiting scroll
<i>N<sub>c1</sub></i>	Number of <i>c<sub>1</sub></i> chambers	<i>is</i>	Inner involute starting
<i>N<sub>c2</sub></i>	Number of <i>c<sub>2</sub></i> chambers	<i>os</i>	Outer involute starting
<i>N<sub>c,max</sub></i>	Number of pairs of compression chambers	<i>ssa</i>	Suction separation
<i>p</i>	Pressure (Pa)	<i>fi0</i>	Fixed scroll inner involute initial
<i>r</i>	Radius (m)	<i>fis</i>	Fixed scroll inner involute starting
<i>t</i>	Parameter for parameterization	<i>fie</i>	Fixed scroll inner involute ending
<i>t<sub>s</sub></i>	Scroll thickness (m)	<i>fo0</i>	Fixed scroll outer involute initial
<i>u</i>	Solution value for $\phi_{ssa}$ (rad)	<i>fos</i>	Fixed scroll outer involute starting
$\Delta x$	Difference in x coordinate (m)	<i>foe</i>	Fixed scroll outer involute ending
$\Delta y$	Difference in y coordinate (m)	<i>I</i>	Inner for chamber
<i>x</i>	Cartesian coordinate (m)	<i>k,fi</i>	Conj. pts. fixed scroll inner involute
$\bar{x}$	Centroid coordinate (m)	<i>k,fo</i>	Conj. pts. fixed scroll outer involute
<i>y</i>	Cartesian coordinate (m)	<i>k,oi</i>	Conj. pts. orb. scroll inner involute
$\bar{y}$	Centroid coordinate (m)	<i>k,oo</i>	Conj. pts. orb. scroll outer involute
$\alpha$	Angle in discharge curve calculation (rad)	<i>max</i>	Maximum
$\alpha$	Index of compression chamber pair	<i>min</i>	Minimum
$\beta$	Angle in discharge curve calculation (rad)	<i>om</i>	Overturning moment
$\delta$	Solution value for $\phi_{ssa}$ (rad)	<i>o1</i>	Arc 1 on orbiting scroll
$\phi$	Involute angle (rad)	<i>o2</i>	Arc 2 on orbiting scroll
$\theta$	Crank angle (rad)	<i>o–f</i>	From orbiting to fixed scroll
$\theta_a$	Discharge angle (rad)	<i>oi0</i>	Orbit. scroll inner involute initial
$\Theta$	Shifted orbiting angle ( $\Theta = \phi_{fie} - \theta - \pi/2$ ) (rad)	<i>ois</i>	Orbit. scroll inner involute starting
$\varpi_a$	Parameter for $r_{a2,max}$	<i>oie</i>	Orbit. scroll inner involute ending
<i>V</i>	Volume (m <sup>3</sup> )	<i>oo0</i>	Orbit. scroll outer involute initial
<i>V<sub>ratio</sub></i>	Built-in volume ratio	<i>oos</i>	Orbit. scroll outer involute starting
$\delta_{radial}$	Radial gap width (m)	<i>ooe</i>	Orbit. scroll outer involute ending
<b>Superscripts</b>		<i>o</i>	Orbiting scroll
/	Line segment	<i>O</i>	Outer for chamber
⌋	Arc of circle	<i>r</i>	Radial
⊃	Involute	<i>t</i>	Tangential
		<i>U</i>	Upstream
		<i>x</i>	x-component
		<i>y</i>	y-component
		○	Spinning

analyses of the scroll compressor including geometry and dynamics. Yanagisawa et al. (1990) constructed a full geometric model based on the foundation set by Morishita. More treatment of the scroll geometry is available from

Halm (1997). One of the major shortcomings of Halm's model is that the derivation is based on particular values for the initial angles of involute. Wang et al. (2005) noted this problem and carried out derivations for the scroll chamber

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