



# Breakaway oxidation of $\text{Ti}_3\text{AlC}_2$ during long-term exposure in air at 1100 °C



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## ABSTRACT

Catastrophic breakaway oxidation of  $\text{Ti}_3\text{AlC}_2$  occurs during long-term oxidation at 1100 °C in air up to 4000 h. Correspondingly, the oxidation kinetics transforms from cubic law to linear law. The transition time is about 3171 h, and the corresponding critical Al content is about 5.99% lower than the initial content. Afterwards, Ti and C start to be oxidized instead of selective oxidation of Al, and  $\text{Al}_2\text{O}_3$  scale loses its protectiveness. Meanwhile, voids generated at the  $\text{Al}_2\text{O}_3/\text{Ti}_3\text{AlC}_2$  interface reduce the oxide scale adhesion. After 3250 h oxidation,  $\text{Ti}_3\text{AlC}_2$  still maintains its crystal structure, indicating the capability of bearing great Al lack.

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## 1. Introduction

The layered ternary ceramics, named MAX phases, where M is an early transition metal, A is an A group element, and X is C and/or N [1–3], have attracted increasing attention due to their unique combination of the properties of both ceramics and metals [4], such as high modulus and strength, good thermal shock resistance, high electrical and thermal conductivity, good machinability, high damage tolerance [5–11]. Among the reported MAX phases,  $\text{Ti}_3\text{AlC}_2$  [12],  $\text{Ti}_2\text{AlC}$  [13] and  $\text{Cr}_2\text{AlC}$  [14] exhibit the most excellent high temperature oxidation resistance, which endow them potential applications as high-temperature materials. Therefore, the oxidation behaviors of these MAX phases, especially  $\text{Ti}_3\text{AlC}_2$ , have been investigated widely.

Wang and Zhou [12] reported that  $\text{Ti}_3\text{AlC}_2$  exhibited good oxidation resistance at 1000–1300 °C for 20 h in air due to the formation of a continuous and adherent  $\text{Al}_2\text{O}_3$  scale, indicating that the preferential oxidation of Al in  $\text{Ti}_3\text{AlC}_2$  happened. The oxidation kinetics followed parabolic law, and the inward diffusion of oxygen through the oxide scale was dominant step. Song et al. [15] presented that at the early oxidation stage of  $\text{Ti}_3\text{AlC}_2$  at 1100 °C in air for short

time ( $\leq 900$  s), predominantly  $\alpha\text{-Al}_2\text{O}_3$  nuclei generated and grew to form a thin  $\text{Al}_2\text{O}_3$  layer firstly. Various, during the oxidation of  $\text{Ti}_3\text{SiC}_2$ , one of most typical MAX phases, both Ti and Si were oxidized to form duplex oxide scale of  $\text{TiO}_2$  outer layer and  $\text{TiO}_2 + \text{SiO}_2$  mix inner layer [16]. That is to say, although  $\text{Ti}_3\text{SiC}_2$  has the identical crystal structure and components except Si replacing Al, its selective oxidation could not happen. Lin et al. [17] investigated Al distribution in  $\text{Ti}_3\text{AlC}_2$  adjacent to the  $\text{Al}_2\text{O}_3/\text{Ti}_3\text{AlC}_2$  interface by utilizing STEM, found that the oxidation induced Al depletion only existed in the narrow range of about 50 nm, which indicates that the outward diffusion of Al in  $\text{Ti}_3\text{AlC}_2$  was quite rapid. Li et al. [18] proposed that the selective oxidation of  $\text{Ti}_3\text{AlC}_2$  based materials was attributed to high oxygen affinity and diffusion coefficient of Al in  $\text{Ti}_3\text{AlC}_2$ .

Based on Wagner's theory about selective oxidation of alloys (such as Fe–Cr–Al alloys [19]), it is well known that there is a critical content  $C_{\text{Al}}'$  of Al, only when the content of Al in the alloys is higher than the critical value, can the initial selective oxidation of alloys and sustainable growing of protective  $\text{Al}_2\text{O}_3$  happen. With increasing oxidation time, Al in the alloys is consumed constantly by the growth of  $\text{Al}_2\text{O}_3$  scale. When the oxidation time is long enough, the alloys suffer from breakaway oxidation in two main failure modes [20]: mechanically induced chemical failure (MICF), involving in scale cracking and spallation; intrinsic chemical failure (InCF), resulting from depletion of aluminum content within the substrate below  $C_{\text{Al}}'$  [21–23].

For  $\text{Ti}_3\text{AlC}_2$ , it is necessary to conduct long-term oxidation of  $\text{Ti}_3\text{AlC}_2$ , in order to determine the critical content of Al needed for

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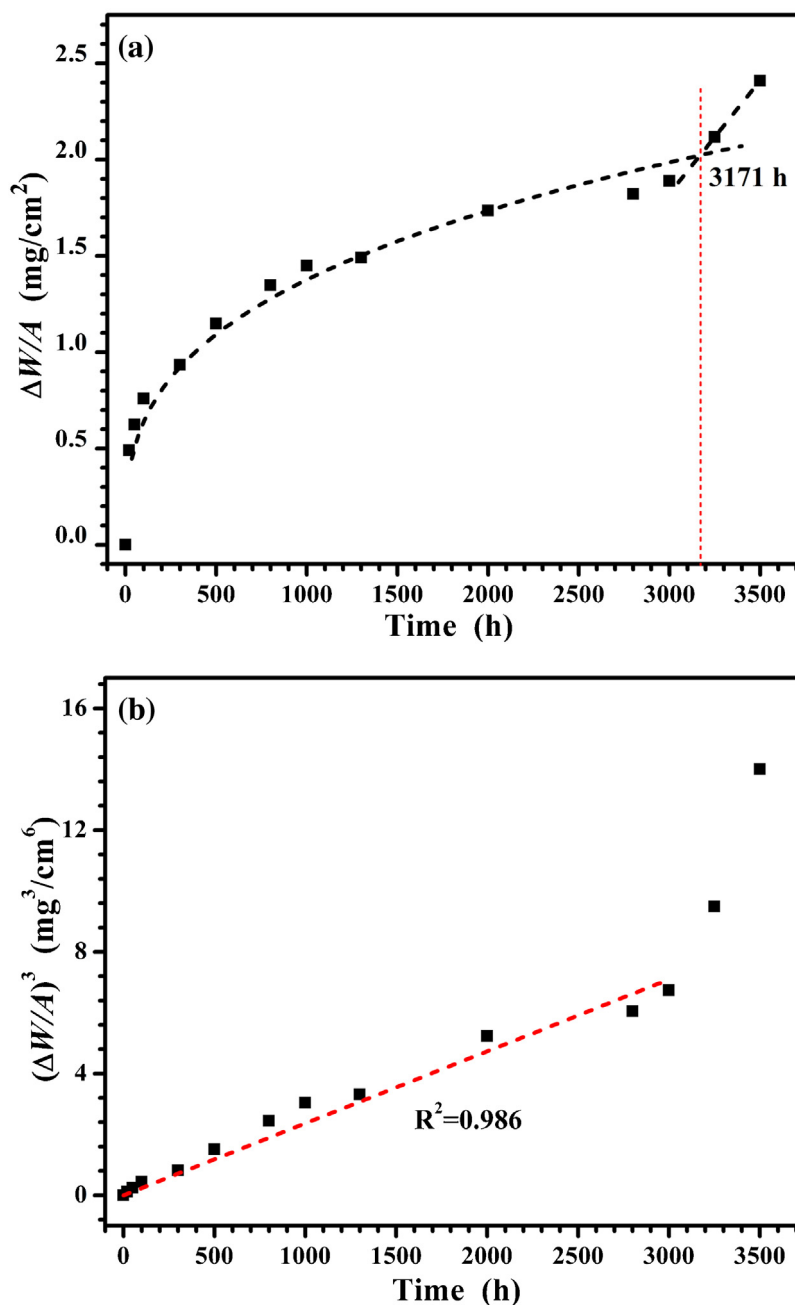


Fig. 1. Oxidation kinetics of  $\text{Ti}_3\text{AlC}_2$  at  $1100^\circ\text{C}$  in air up to 3500 h, (a)  $\Delta W/A$  vs.  $t$ , (b)  $(\Delta W/A)^3$  vs.  $t$ .

sustaining the protectiveness of  $\text{Al}_2\text{O}_3$  scale. On the other hand, severe consumption of Al may result in phase transformation of  $\text{Ti}_3\text{AlC}_2$  to more stable Ti–C binary carbides [24,25]. In fact,  $\text{Cr}_2\text{AlC}$  also exhibited good oxidation resistance up to  $1300^\circ\text{C}$  in air for 20 h due to the formation of protective  $\text{Al}_2\text{O}_3$  scale [14]. However, differing from  $\text{Ti}_3\text{AlC}_2$ ,  $\text{Cr}_2\text{AlC}$  transformed to Cr–C carbides (Such as  $\text{Cr}_7\text{C}_3$ ,  $\text{Cr}_3\text{C}_2$ ) easily due to the depletion of Al within  $\text{Cr}_2\text{AlC}$  in the areas adjacent to the  $\text{Al}_2\text{O}_3$ /substrate interface [14]. When the oxidation time was prolonged,  $\text{Cr}_2\text{O}_3$  nodules formed on the oxide layer [26], even voids generated in the  $\text{Cr}_7\text{C}_3$  layer destroyed the subscale area and deteriorated the scale adherence under the oxidation condition at  $1300^\circ\text{C}$  in air up to 336 h [27].

It is believed that  $\text{Ti}_3\text{AlC}_2$  would also lose its good oxidation resistance at some time due to the scale cracking and spallation without healing or depletion of Al in the substrate. Unfortunately, it is difficult to determine the lifetime of  $\text{Ti}_3\text{AlC}_2$  and failure mode

by previous work. Firstly, nothing about the critical Al content for selective oxidation of  $\text{Ti}_3\text{AlC}_2$  or its breakaway oxidation has been reported up to now. Secondly, although there is no Al depletion zone found beneath the protective  $\text{Al}_2\text{O}_3$  scales for short-time oxidation [28], the distribution of Al in the  $\text{Ti}_3\text{AlC}_2$  substrate after long-term oxidation has not been determined. Thirdly, cracking, spallation and crack-healing ability of  $\text{Al}_2\text{O}_3$  scale on  $\text{Ti}_3\text{AlC}_2$  after long-term oxidation ( $>1000$  h) are unclear. Therefore, it is imperative to study the long-term oxidation behaviors of  $\text{Ti}_3\text{AlC}_2$  as well as to determine critical content of Al for sustaining protection of  $\text{Al}_2\text{O}_3$  scale or phase stability of  $\text{Ti}_3\text{AlC}_2$ .

In the present work, a long-term oxidation of  $\text{Ti}_3\text{AlC}_2$  up to 4000 h at  $1100^\circ\text{C}$  in static air has been conducted to study the evolution of oxidation kinetics and oxidation products of  $\text{Ti}_3\text{AlC}_2$ . Meanwhile, the critical Al content within  $\text{Ti}_3\text{AlC}_2$  below which breakaway oxidation occurred is determined. Oxide adhesions

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