

Assessment of boiling heat transfer correlations in the modelling of fin and tube heat exchangers

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Received 4 September 2006; received in revised form 7 November 2006; accepted 9 January 2007

Available online 18 January 2007

Abstract

A new way to assess the performance of refrigeration system models is presented in this paper, based on the estimation of cycle parameters, such as the evaporation temperature which will determine the validity of the method. This paper is the first of a series which will also study the influence of the heat transfer coefficient models on the estimation of the refrigeration cycle parameters. It focuses on fin and tube evaporators and includes the dehumidification process of humid air. The flow through the heat exchanger is considered to be steady and the refrigerant flow inside the tubes is considered one-dimensional. The evaporator model is discretised in cells where 1D mass, momentum and energy conservation equations are solved by using an iterative procedure called SEWTLE. This procedure is based on decoupling the calculation of the fluid flows from each other assuming that the tube temperature field is known at each fluid iteration. Special attention is paid to the correlations utilised for the evaluation of heat transfer coefficients as well as the friction factor on the air and on the refrigerant side. A comparison between calculated values and measured results is made on the basis of the evaporation temperature. The experimental results used in this work correspond to an air-to-water heat pump and have been obtained by using *R-22* and *R-290* as refrigerants.

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Keywords: Refrigeration; Air conditioning; Heat exchanger; Finned tube; Survey; Correlation; Boiling; Heat transfer; Comparison; Experiment

Evaluation des corrélations de transfert de chaleur lors de l'ébullition dans la modélisation des échangeurs de chaleur du type tube aileté

Mots clés : Réfrigération ; Conditionnement d'air ; Échangeur de chaleur ; Tube aileté ; Enquête ; Corrélation ; Ébullition ; Transfert de chaleur ; Comparaison ; Expérimentation

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Nomenclature

A	cross section area (m ²)	W	humidity (kg vap/kg dry air)
A_o	total surface area	x	vapour quality
$A_{p,o}$	outer surface area of tubes	z, y	spatial co-ordinates (m)
$A_{T_{ji}}$	extended surface area		
b_w	slope of i vs. T curve	<i>Greeks</i>	
C_p	specific heat (J/kg K)	α	heat transfer coefficient (W/m ² K)
C_F	function of the molar weight	α_c	convection heat transfer coefficient (W/m ² K)
CV	$G[(x^2/\rho_g\alpha) + ((1-x)^2/\rho_f(1-\alpha))]$	α_D	convection mass transfer coefficient (W/m ² K)
D	diameter (m)	δ	film thickness
D_c	fin collar outside diameter ($D_o + 2\delta_f$)	δ_f	fin thickness
D_h	hydraulic diameter (m)	Δ	Increment
D_o	tube outside diameter	ϵ	void fraction
e	wall thickness (m)	η	dynamic viscosity (Ns/m ²)
$f()$	set of equations	η_T	extended surface efficiency
f	friction factor	∇^2	Laplacian operator
f_1, f_2, f_3, f_4	friction factor coefficient in air side correlation	Φ_f^2	2-phase fric. multiplier
$F()$	general function	ϕ, φ	generic variable
F_1, F_2, F_3	friction factor coefficient in air side correlation	ϕ	friction multiplier
F_p	fin pitch	ρ	density (kg/m ³)
g	gravity (m/s ²)	σ	surface tension
G	mass velocity (kg/s m ²)	θ	angle characterising the volume occupied by the vapour phase
i	enthalpy (J/kg)		
j	Colburn factor	<i>Subscripts and superscripts</i>	
k	thermal conductivity (W/m K)	a	air
\dot{m}	mass flow rate (kg/s)	cb	convective boiling
N	number of tube rows	cri	critical
Nu	Nusselt number	eq	equivalent
p	pressure (Pa)	f	saturated liquid (liquid phase)
P	perimeter (m)	g	saturated vapour (vapour phase)
$P_1, P_2, P_3, P_4, P_5, P_6$	Colburn factor coefficients	GO	vapour only
P_1	longitudinal pitch	i	inlet, cell index
P_t	transverse tube pitch	j	cell index
Pr	Prandtl number	LO	liquid only
q	heat flux (W/m ²)	mom	momentum
Q	heat (W)	nb	nucleate boiling
R	thermal resistance	o	outlet, cell index
Re	Reynolds number	PB	pool boiling
S	slip ratio	r	refrigerant
T	temperature (K)	s	saturation
u	velocity (m/s)	tp	two-phase flow
		VO	vapour only
		w, W	wall
		wat	water
		0	reference value
		*	reduced parameter

1. Introduction

In this paper, a new way to assess the goodness of published boiling heat transfer correlations for horizontal tubes in fin and tube evaporators calculations is presented.

Normally when a model for fin and tube evaporators is based on cell discretisation, the uncertainties associated with the heat transfer coefficients in both sides overcome those associated with the modelling assumptions. It is also usual to find that the modeller doubts about the application

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