

Single-effect absorption refrigeration cycle boosted with an ejector-adiabatic absorber using a single solution pump



C. Vereda*, R. Ventas, A. Lecuona, R. López

Departamento de Ingeniería Térmica y de Fluidos, Universidad Carlos III de Madrid, Avda. Universidad 30, 28911 Leganés, Madrid, Spain

ARTICLE INFO

Article history: Received 25 July 2013 Received in revised form 1 October 2013 Accepted 27 October 2013 Available online 5 November 2013

Keywords:

Absorption hybrid cycles Ammonia-lithium nitrate Cooling Two-phase ejector Adiabatic absorber Solar cooling

ABSTRACT

This paper presents a numerical model of a single-effect absorption refrigeration cycle incorporating a triple purpose liquid–vapor ejector acting as pressure booster for refrigerant vapor, adiabatic absorber and controlled solution expansion valve. The promising ammonia-lithium nitrate solution is selected as working pair, being able to produce cold at subzero temperatures, thus valid either for air conditioning or industrial refrigeration. With the use of the liquid–gas ejector, the absorption pressure becomes higher than the evaporation pressure, besides recovering part of the solution pump energy. Results of the simulation show that this innovation behaves like a compressor boosted hybrid cycle without carrying its complexity. It allows decreasing the activation temperature (about 15 °C for a recirculation ratio of 3) and increasing the cooling capacity (reaching a gain of about 100% for a generation temperature of 80 °C).

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Cycle frigorifique à simple effet à absorption augmenté par un absorbeur à éjecteur adiabatique utilisant une pompe à solution unique

Mots clés : Cycles hybrides à absorption ; Nitrate de lithium-ammoniac ; Refroidissement ; Ejecteur diphasique ; Absorbeur adiabatique ; Refroidissement solaire

* Corresponding author. Tel.: +34 91 624 6224; fax: +34 91 624 9430. E-mail address: cvereda@ing.uc3m.es (C. Vereda).

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Nomenclature		$\eta_{ m M}$	ejector mixing efficiency
A d COP_T COP_E h \dot{m} P_1 P_4 P_{abs} pr \dot{Q} Q rr T T_c T_e U V	area, m^2 diameter, m thermal coefficient of performance electrical coefficient of performance specific enthalpy, J kg ⁻¹ mass flow rate, kg s ⁻¹ condenser-generator pressure, Pa evaporator pressure, Pa absorber pressure, Pa ejector pressure ratio: P ₅ /P ₄ thermal power, W volumetric flow, m ³ s ⁻¹ recirculation ratio temperature, °C condensation temperature, °C global heat transfer coefficient, W m ⁻² K ⁻¹ velocity, m s ⁻¹	η _{emec} η _N ω φ Subscrip	electro-mechanical pump motor efficiency ejector nozzle efficiency ejector mass flow ratio: \dot{m}_r/\dot{m}_{10} ejector volumetric flow ratio: Q_r/Q_{10} d_r/Q_{10}
V	velocity, m s ⁻¹		outlet
Ŵ _p X	pump power, W ammonia mass fraction		refrigerant recirculation ratio
Greek: α ρ η _D η _{hyd}	ratio of ammonia absorbed in the mixing tube density, kg m ⁻³ ejector diffuser efficiency pump hydraulic efficiency	she sol sub sup tp	solution heat exchanger solution sub-cooling super-heating two-phase

1. Introduction

The diabatic absorber is currently the largest size element of absorption single-effect machines due to transferring heat and mass at the same time, using a two-phase flow configuration, Herold et al. (1996). In contrast, the adiabatic absorber separates the processes of heat and mass transfer, Ryan (1993). The absorption heat evacuation occurs in a conventional single-phase heat exchanger (sub-cooler), which allows reducing its size and cost as well, as it can be a commercial standard model. Therefore, the plate heat exchanger technology with adiabatic absorber seems to be an enabling factor for reducing the size and cost of the absorber, Flamensbeck et al. (1998).

In the adiabatic absorber, as the absorption heat is not evacuated, the usual diabatic equilibrium cannot be reached inside this single-pass absorber, Ventas et al. (2010a, b); instead, the equilibrium is at a higher temperature, thus with less refrigerant absorbed. Hence, externally recirculating and sub-cooling the poor in refrigerant solution more refrigerant vapor can be absorbed in successive passes. A second lowhead pump, in addition to the main solution pump, can provide this recirculation. In small capacity chillers, this could in

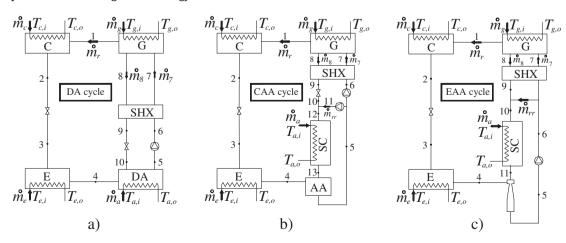


Fig. 1 — Layout of single-effect absorption cycles: a) with diabatic absorber (DA), b) with conventional adiabatic absorber (CAA) and c) with ejector-adiabatic absorber (EAA). Components legend: evaporator (E), condenser (C), generator (G), solution heat exchanger (SHX), sub-cooler (SC), diabatic absorber (DA) and adiabatic absorber (AA).

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