

## Modeling of a semi-hermetic CO<sub>2</sub> reciprocating compressor including lubrication submodels for piston rings and bearings



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#### ABSTRACT

A comprehensive model for a semi-hermetic  $CO_2$  reciprocating compressor is presented. This comprehensive model is composed of three main sub-models simulating the geometry and kinematics, the compression process, and frictional power loss. Valve and leakage sub-models are included in the compression process model. The frictional power loss model includes the friction at the bearings and between the piston ring and cylinder wall. The predicted results of the comprehensive model are validated using external compressor performance measurements of compressor input power and mass flow rate. The mass flow rate and compressor input power are predicted to within 4.03% and 6.43% mean absolute error, respectively, compared to the experimental datum. Additionally, a parametric study is presented which investigates compressor performance as a function of the stroke-to-bore ratio.

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# Modélisation d'un compresseur à piston semi-hermétique au CO2, y compris des sous-modèles pour la lubrification des segments de piston et des paliers

Mots clés : Compresseur à piston ; Modèle ; CO2 ; Optimisation ; Frottement

### 1. Introduction

Since the rediscovery of carbon dioxide ( $CO_2$  or R744) as a suitable refrigerant by Lorentzen and Pettersen (1992), many studies have been conducted on  $CO_2$  compressors and systems. The operating temperatures of typical refrigeration or air-conditioning systems dictate that a cycle using  $CO_2$  as a working fluid would need to operate as a trans-critical cycle. In these systems, the  $CO_2$  reciprocating compressor runs with a relatively high operating

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Nomeno	clature	μ	dynamic viscosity [Pa S] or friction coefficient [–]
А	area [m <sup>2</sup> ]	$v_{1,oil}, v_{2,o}$	$_{ m sil}$ kinematic viscosity at 37.8 °C and 93.3 °C
C	discharge coefficient [_]		respectively [cS]
	integration constant [_]	$\nu_1, \nu_2$	Poisson's ratio [—]
С <sub>1</sub> , С <sub>2</sub>	diameter [m]	$v_{r1}$	the surface roughness variance ratio [–]
	Vound's modulus for ring and guinder well (Cool	ρ	density [kg m <sup>-3</sup> ]
E <sub>1</sub> , E <sub>2</sub>	found s modulus for ring and cylinder wall [Gpa]	σ	composite surface roughness
F	iorce [N]	$\sigma_1, \sigma_2$	surface roughness for ring and cylinder liner
G	gravity [N]	τ	thermal conductivity of refrigerant in control
Р	power [W]		volume $[W m^{-1}K^{-1}]$
$H_{pc}$	instant frictional loss between the top piston ring	$\phi_{f}, \phi_{fc}$	shear stress factors, dimensionless
	and cylinder wall [W]	φ <sub>x</sub> , φ <sub>c</sub>	Pressure flow factor and shear flow factor
L	axial length of the bearing [m]	τ A) τ S	angular speed of the crankshaft (rad $s^{-1}$ )
Nj	rotational speed of the journal [rps]		angalar speca of the cramonale frag of j
Ν	the number of asperities per unit contact area	Subscript	S
Q	quantity of heat transferred to control volume	0	clearance volume
	through boundary from its ambient [J]	А	asperity
R	gas constant of carbon dioxide [J $kg^{-1} K^{-1}$ ], or	b	ring back
	radius [m]	bearing	crankshaft bearing and crank journal bearing
S	piston stroke [m]	bush	bearing bush
Т	temperature [K]	с	refrigerant in control volume
U	velocity [m s <sup>-1</sup> ]	case	compressor case
V	volume [m <sup>3</sup> ]	cir	circumferential
W	work [J], power [W] or force [N]	contact	asperity contact
W*	Dimensionless load capacity [-]	CS	crankshaft
Z	compact factor of carbon dioxide [-]	cvl	cylinder
_ a	niston acceleration $[m s^{-2}]$	d	downstream
h	niston ring thickness [m]	die	discharge
	clearance [m]	f	friction
	c c crankshaft dimensions [m]	I GOD	niston ring con
$L_1, L_2, L_3, L_4$	$L_4, L_5$ Clarkshart differences [11]	gap	piston mig gap
n h	unit entitalpy j kg j of on min thickness [m]	gas	gas in the un-indicated region of piston mig
n <sub>valve</sub>		п 1.1.1.	
m	mass [kg]	nign	nigh pressure side
m	mass flow rate of refrigerant of the compressor	ind	actual indicated power
	[kg s <sup>-1</sup> ]	input	compressor input
n	compressor rotational speed [rpm]	journal	crankshaft journal
р	pressure [Pa]	1	connecting rod
$p_1, p_2$	inlet and outlet pressure of piston ring lubrication	li, lo	leak in and out
	region [Pa]	loc	local
и	unit internal energy [J kg <sup>-1</sup> ]	low	low pressure side
υ	specific volume [m³ kg <sup>-1</sup> ]	М	electric motor
х	piston displacement [m]	mean	mean velocity of piston
x <sub>C</sub>	cavitation point [m]	oil	lubricating oil
Crach lat	toro	р	piston
GIEEK LEL	Polotico algoran es volume [ ]	radius	radius
α	Relative clearance volume [–]	ring	piston ring
β	angle between the axis of connecting rod and	shaft	crankshaft
o'	center line of cylinder [rad]	suc	suction
β	asperity radius of curvature	sup	oil supply
η	efficiency	т	ring tension
$\theta$	crank angle [rad]	t	total
К	specific heat ratio [–]	u	upstream
λ	ratio of crank radius to the length of the	valve	valve
	connecting rod	, and	

pressure compared to other reciprocating compressors using conventional refrigerants, which presents practical challenges. Thus, the unique operating cycle and practical challenges for  $CO_2$  compressors necessitate the need for careful

modeling of a  $CO_2$  reciprocating compressor as presented in this work.

Many steady-state simulation models for reciprocating compressors are presented in the literature. Navarro et al. (2007)

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