

# Modeling and performance analyses of evaporators in frozen-food supermarket display cabinets at low temperatures

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## Abstract

This paper presents modeling and experimental analyses of evaporators in “in situ” frozen-food display cabinets at low temperatures in the supermarket industry. Extensive experiments were conducted to measure store and display cabinet relative humidities and temperatures, and pressures, temperatures and mass flow rates of the refrigerant. The mathematical model adopts various empirical correlations of heat transfer coefficients and frost properties in a fin-tube heat exchanger in order to investigate the influence of indoor conditions on the performance of the display cabinets. The model is validated with the experimental data of “in situ” cabinets. The model would be a good guide tool to the design engineers to evaluate the performance of supermarket display cabinet heat exchangers under various store conditions.

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*Keywords:* Frozen product; Display cabinet; Evaporator; Modelling; Simulation; Flow; Refrigerant; Temperature; Relative humidity; Pressure; Frost

## Modélisation et analyse de la performance des évaporateurs utilisés dans les meubles de vente de supermarché employés pour les surgelés

*Mots clés :* Produit congelé ; Meuble de vente ; Évaporateur ; Modélisation ; Simulation ; Débit ; Frigorigène ; Température ; Humidité relative ; Pression ; Givrage

### 1. Introduction

Supermarket refrigeration systems, mainly refrigerated display cases, consume roughly 20% of the total energy use of the store (Getu [1]). The field (defrosting, anti-sweat

resistance heaters, display cabinet lights and fans) energy consumption contributes to an additional 14%. The energy consumption due to the air-conditioning system of the building is as much as 17% of the entire energy use of the supermarket. The rest of the supermarket energy use, which is around 49% attributes to water heating and lighting systems of the establishment. Supermarkets often use multi-compressor systems/racks, which are situated in remote machine rooms. The compressors operate in parallel at the same saturated suction temperature, and are piped with

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**Nomenclature**

$A_f$	fin surface area [m <sup>2</sup> ]	$N_t$	total number of tubes
$A_{\text{reg,tube}}$	bare tube surface area of superheated/ two-phase region [m <sup>2</sup> ]	NTU	number of transfer units [dimensionless]
$A_{\text{reg,i}}$	internal tube surface area of superheated/ two-phase region [m <sup>2</sup> ]	$Nu$	Nusselt number [dimensionless]
$A_{\text{reg,o}}$	overall surface area of superheated/two-phase region [m <sup>2</sup> ]	$P$	pressure [Pa]
$A_{\text{sp}}$	air-side total surface area in superheated region [m <sup>2</sup> ]	$Pr_D$	Prandtl number based on tube inside diameter [–]
$A_{\text{tp}}$	air-side total surface area in two-phase region [m <sup>2</sup> ]	$Pr_{\text{DH}}$	Prandtl number based on frosted surface [–]
$A_{\text{total}}$	air-side total surface area [m <sup>2</sup> ]	$\dot{Q}$	rate of heat transfer [W]
$C$	ratio of minimum to maximum capacity rate of heat exchanging fluids [–]	$r_f$	fin tip radius [m]
$C_a$	capacity rate of air [W K <sup>-1</sup> ]	$r_o$	tube outer radius [m]
$C_{\text{max}}$	maximum heat capacity rate [W K <sup>-1</sup> ]	$Re$	Reynolds number [dimensionless]
$C_{\text{min}}$	minimum heat capacity rate [W K <sup>-1</sup> ]	$Re_D$	Reynolds number based on tube inside diameter
$C_r$	capacity rate of refrigerant [W K <sup>-1</sup> ]	$Re_{\text{DH}}$	Reynolds number based on frosted surface [–]
$C_p$	specific heat at constant pressure [kJ kg <sup>-1</sup> K <sup>-1</sup> ]	RH	relative humidity [%]
$D$	diameter [m]	$S_F$	fin spacing [fin m <sup>-1</sup> ]
$D_H$	frosted hydraulic diameter [m]	$S_L$	longitudinal tube spacing [m]
$f$	friction factor [dimensionless]	$S_T$	transverse tube spacing [m]
$f_f$	friction factor due to fins	$t$	time [s]/thickness [m]
$f_t$	friction factor due to tubes	$T$	temperature [°C]
$Fo_{\text{DH}}$	Fourier number based on frosted surface [–]	$T_i$	the temperature difference between triple point and coil surface [K]
GFF	glass-door-frozen-food	TFF	through-frozen-food
$G$	mass flux [kg s <sup>-1</sup> m <sup>-2</sup> ]	$U$	overall heat transfer coefficient [W/m <sup>2</sup> k <sup>-1</sup> ]
$h$	enthalpy [J kg <sup>-1</sup> ]/heat transfer coefficient [W m <sup>-2</sup> K <sup>-1</sup> ]	$x$	quality [dimensionless]
$h_c$	fin-tube contact conductance [W m <sup>-2</sup> K <sup>-1</sup> ]	<i>Greek letters</i>	
$h_{f,a}$	air-side fouling conductance [W m <sup>-2</sup> K <sup>-1</sup> ]	$\Delta$	change [–]
$h_{f,\text{ref}}$	refrigerant-side fouling conductance [W m <sup>-2</sup> K <sup>-1</sup> ]	$\varepsilon$	heat exchanger effectiveness [–]
$h_{\text{sg}}$	sublimation latent heat [J kg <sup>-1</sup> ]	$\varphi$	efficiency [–]
$I_0$	modified zero-order Bessel function of the first kind [–]	$\omega$	humidity ratio [kg moisture/kg dry air]
$K_0$	modified zero-order Bessel function of the second kind [–]	$\omega_\infty$	free air stream humidity ratio [kg/kg]
$I_1$	modified first-order Bessel function of the first kind [–]	$\rho$	density [kg m <sup>-3</sup> ]
$K_1$	modified first-order Bessel function of the second kind [–]	$\zeta$	constant [dimensionless]
$j$	colburn factor	$\mu$	viscosity [kg s <sup>-1</sup> m <sup>-1</sup> ]
$k$	conductivity [W m <sup>-1</sup> K <sup>-1</sup> ]	<i>Subscripts</i>	
$L$	length [m]	a	air
$L_D$	frost length in the direction of air flow [m]	ave	average
$L_{\text{reg}}$	tube length in superheated/two-phase region [m]	ain	air inlet
Lewis	Lewis number [–]	aout	air outlet
$m$	mass [kg]/constant [–]	case	display cabinet
$\dot{m}$	mass flow rate [kg s <sup>-1</sup> ]	D	tube diameter
$m_{\text{fst}}$	frost mass accumulation [kg m <sup>-2</sup> ]	e	evaporator
		ein	evaporator inlet
		eout	evaporator outlet
		exvin	expansion valve inlet
		f	liquid refrigerant/fin
		fst	frost
		i	inner
		ice	ice
		in	inlet
		lat	latent

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